Research Article

Studying the Effects of Adding Silica Sand Nanoparticles on Epoxy Based Composites

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Received 10 December 2012; Accepted 24 December 2012

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The research about the preparation of submicron inorganic particles, once conducted in the past decade, is now leading to prepare polymer matrix composite (PMC) reinforced with nanofillers. The objective of present research is to study the modified effects of reinforcement dispersion of nanoparticle silica in epoxy resin on the physical properties, mechanical and thermal behaviour, and the microstructure of resultant composites. Stirrer mixing associated with manual mixing of silica sand nanoparticles (developed in our earlier research) (Ahmad and Mamat, 2012) into epoxy was followed by curing being the adopted technique to develop the subject nanocomposites. Experimental values showed that 15 wt.% addition of silica sand nanoparticles improves Young's modulus of the composites; however, a reduction in tensile strength was also observed. Number of holes and cavities produced due to improper mixing turn out to be the main cause of effected mechanical properties. Addition of silica sand nanoparticles causes a reduction in degree of crystallinity of the nanocomposites as being observed in differential scanning calorimetry (DSC) analysis.

1. Introduction

Nowadays industrial and academic research laboratories are focusing much of their efforts to develop and improve physical, mechanical, and electrical properties of polymer nanocomposites. Their interest to develop such composites is mainly because of the fact that nanoparticles present a high surface-to-volume ratio which may induct unique properties to these nanocomposites as compared to macro-scale composites [1]. Andritsch et al. [2] prepared nanocomposites filled with SiO₂, Al₂O₃, and AlN with an average particles size from 22 nm to 10 nm and studied the nanoparticles dispersion and DC breakdown strength. They observed the highest DC breakdown strength for 0.5 wt.% for two component system. It was also noticed that the DC breakdown strength increased with 10 wt.% as compared to 2 and 5 wt.% and again decreased with 15 wt.% nano-fillers. Yasmin et al. [3] studied the dispersion of clay nanoparticles in epoxy-based composites using a three roll mill with the concentration of 1–10 wt.%. This technique was found highly efficient and environmentally friendly due to excellent dispersion of nanoparticles within a short time. Elastic modulus was improved up to 80% with 10 wt.% addition of clay nanoparticles in epoxy. Absence of any improvement in tensile strength of the nanocomposites over pure epoxy was due to the clustering of nanoparticles and/or to the occasional occurrence of nano- to microsize voids in the microstructure. Li et al. [4] prepared the Epoxy nanocomposites with exfoliated nanoclay and a novel ultrafine full-vulcanized powdered rubber. The morphology of the epoxy/rubber/clay nanocomposites has been studied using X-ray diffraction (XRD) and transmission electron microscopy (TEM). Their study showed that the unmodified clay was fully exfoliated and uniformly dispersed in the resulting nanocomposite and found that the impact strength of this special epoxy/rubber/clay nanocomposite increased up 107% over the neat epoxy resin. Thermal analyses showed that thermal stability of the nanocomposite was much better than that of epoxy nanocomposite based on organically modified clay. Damian et al. [5] synthesized epoxy-based nanocomposites reinforced with multiwalled...
carbon nano-tubes (MWNT). They functionalized MWNTs in order to increase the dispersion in the polymer matrix and thus to ensure good adhesion between the two components. Their study showed that the structure of amine MWNT-B100 exhibit compatibility with the epoxy matrix. However, the higher thermostability was achieved by the composite based on MWNT- COOH as observed from TGA. Frache et al. [6] prepared the epoxy based nanocomposites reinforced with home-made hydrotalcites (HTlcs) and montmorillonite-(MMT-)type layered silicates and studied the morphology, dispersion and thermal analysis of the nanocomposites. Their research showed possibility to obtain nano-structured materials, characterized by the resin intercalation into HTlc galleries, by using a proper exchange of the pristine hydro-talcite with stearate anions. The thermal analysis indicated that nanocomposites based on HTlcs were prone to decompose, both in air and nitrogen, while in the case of the nanocomposite based on the organophilic MMT a slight improvement was found in air. Jordan et al. [7] studied the effect of addition of micron and nanosized silica inclusions on polyurethane matrix and found it as an increment in density as the filler content increased. He investigated that the composite density further can be increased with micron-sized inclusions as compared to the density for the nanosized inclusions. In above studies, no body tried to utilize silica sand nanoparticles as reinforcement agents in epoxy based composites. Exclusively, the objective of present research is to fill this gap and study the effect of addition of silica sand nanoparticles on epoxy based composites.

2. Experimental Work

The processing and characterization of silica sand nanoparticles have already been discussed in our earlier papers [8]. Before mixing with epoxy resin (E-51), silica sand nanoparticles were dried at 120°C to remove any moisture for 5 hours. The silica sand nanoparticles were mixed with epoxy using stirrer and manual mixing for several hours. The resultant mixture was degassed and cured in steel mould at 120°C to form dog-bone-shaped samples (ASTM D638-97). ASTM D790-03 standard was used to develop flexural test specimens. The Universal Tensile Testing machine (5 KN) LLOYD Instruments, LR 5 K was engaged to determine the tensional and flexural properties of the composites with a cross-head speed of 50 mm/min. ASTM D 792-08 standard was used to determine the densities of epoxy based composites. Differential scanning calorimeter (DSC) in nitrogen atmosphere was incorporated to analyse the thermal properties of the epoxy based composites. A 5 mg weight sample was prepared to obtain the scans between 40 to 210°C wit a heating rate of 10°C/min.

3. Results and Discussion

3.1. Processing of Tronoh Silica Sand. The silica sand originated naturally from Tronoh Perak, Malaysia was washed with water to remove any clay particles followed by drying it in an oven at 120°C. The dried silica sand was meshed about <600 μm using sieve analysis. The <600 μm size of natural silica sand was ground to nanoparticles using dry ball milling with zirconia balls as grinding media with different steps of sieve analysis. This high-energy milling was known as one of the “top-down” nanoparticles type approach, which generally relies on physical methods for their production. Different particles sizes went through a precise sieve analysis (Sieve Shaker (EFL2000)). The analysis of silica sand nanoparticles had been verified using the ZetaSizer, Nano ZS (ZEN 3600) (MALVERN) analyzer. The nanoparticles results were also checked microscopically through FESEM.
The chemical composition of silica sand nanoparticles was analyzed adopting XRF technique [8].

3.2. Characterization of the Epoxy-Silica Sand Nanoparticles Composites

3.2.1. Density and Specific Gravity Determination of Epoxy-Silica Nanoparticles Composites. The silica sand being denser as compared to epoxy may cause an enhancement in density of epoxy when added as reinforcement as shown in Figure 1. For every 5 wt.% increase in weight of silica sand nanoparticles, the density of epoxy raised with an average incremental value of 1.8%. Temperature recorded during testing procedure remained as 22.6°C. The inclusions of silica nanoparticles when added to polymer tended to create a linkage of bonding between SiO$_2$ and polymer which some time results in higher density of the composites.

Results obtained above may actually be expanded to get specific gravity values for each sample. The density and specific gravity were determined using D 792-08 ASTM standard. Specific gravity, or relative density, increases in accordance to sample density as well as wt% increment of silica sand nanoparticles. An increase between 2%–6% can be seen by comparing silica sand nanoparticles added epoxy with its pure form as control element. For every 5% increase in weight of silica sand nanoparticles, it can be found that specific gravity increased by an average value of 1.8%, which is the same compared to density measurement. The results of specific gravities are shown in Figure 2.

3.2.2. Mechanical Properties of the Epoxy-Silica Sand Nanoparticles Composites. The properties of the composites depend upon the method of dispersion of particles, aggregation of particles, and interaction between particles and polymers. The thickness and density of the interphase developed between two constituents depend on the interaction between particles and polymer [7]. Interparticle distance also plays an important role in the interphase behaviour and properties of the composites. Tensile properties of the composites are mostly affected by the materials, method, specimen condition and preparation, and also by percentage of the reinforcement [9]. For the comparative testing of materials, the preparation of samples and adopted method are very important to get relatively same properties of the composites. Silica nanoparticles, if not properly mixed with the epoxy, cause voids and increase level of porosity inside the system. This is the reason why pure epoxy exhibited highest value of tensile strength and Young’s modulus, and why this strength got reduced when silica nanoparticles between 15 wt.% and 20 wt.% dispersed in it. The mechanical properties of the epoxy-silica sand nanoparticles composites are shown in Figure 3. As wt.% of silica sand nanoparticles increases, tensile strength as well as Young’s modulus also rises. These numbers conversely drop when 20 wt.% of silica sand nanoparticles is introduced to system. Nature of interface is important in producing high-performance epoxy-nanosilica composites [10]. Better tensile properties are achieved when the samples have good interface between matrix and filler because the applied load mostly transferred through the filler via interface.

3.2.3. Thermal Analysis of the Epoxy-Silica Sand Nanoparticles Composites. The thermal analysis of epoxy-SiO$_2$ nanocomposites was performed using DSC technique as shown in Table 1. Neat epoxy showed the values of crystallization temperature between 111.12 and 110.32°C; however, for 20 wt.% of silica sand nanoparticles addition to epoxy, the values remain between 121.59 and 119.97. The increase in weight percentage of silica sand nanoparticles to epoxy increases the crystallization temperature; however, it reduces the percentage crystallinity of the nanocomposites as shown in Figure 4 DSC curves. Melting endotherms showed a slight difference for all samples as observed in DSC thermograms and the same results were also found by other researcher using different kinds of nanoparticles [10]. Built-in software
Table 1: DSC analysis of epoxy-silica sand nanoparticles composites.

<table>
<thead>
<tr>
<th>Composites</th>
<th>Crystallization $T_c$ (onset) ($^\circ$C)</th>
<th>Crystallization $T_c$ (peak) ($^\circ$C)</th>
<th>Melting $T_m$ (onset) ($^\circ$C)</th>
<th>Melting $T_m$ (peak) ($^\circ$C)</th>
<th>$\Delta H$ (J/g)</th>
<th>Crystallinity (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Pure epoxy</td>
<td>110.32</td>
<td>111.12</td>
<td>160.20</td>
<td>161.14</td>
<td>250.774</td>
<td>86.8</td>
</tr>
<tr>
<td>5 wt.% silica sand + epoxy</td>
<td>112.34</td>
<td>113.40</td>
<td>160.33</td>
<td>161.40</td>
<td>240.523</td>
<td>83.5</td>
</tr>
<tr>
<td>10 wt.% silica sand + epoxy</td>
<td>115.44</td>
<td>116.20</td>
<td>160.45</td>
<td>161.21</td>
<td>239.804</td>
<td>80.3</td>
</tr>
<tr>
<td>15 wt.% silica sand + epoxy</td>
<td>117.95</td>
<td>118.60</td>
<td>179.64</td>
<td>161.46</td>
<td>237.495</td>
<td>79.5</td>
</tr>
<tr>
<td>20 wt.% silica sand + epoxy</td>
<td>119.97</td>
<td>121.59</td>
<td>138.30</td>
<td>145.55</td>
<td>230.444</td>
<td>77.6</td>
</tr>
</tbody>
</table>

Figure 5: Fracture surface analysis of pure epoxy, epoxy-SiO$_2$ nanoparticles composites with (a) pure, (b) 5 wt.% SiO$_2$, (c) 10 wt.% SiO$_2$, (d) 15 wt.% SiO$_2$, (e) 20 wt.% SiO$_2$. 
as shown in (1) below was used to determine the heat of fusion ($\Delta H$) from the scans as follows:

$$X_{DSC} = \frac{\Delta H_{sample}}{293}. \quad (1)$$

The reduction in degree of crystallinity was mainly due to reducing trend of heat of fusion from 5 wt.% to 20 wt.% of silica sand nanoparticles in epoxy. The same results were also discussed by some other researchers [11, 12].

### 3.2.4. Fracture Surfaces SEM Analysis of Tensile Samples of Epoxy-$\text{SiO}_2$ Composites

For pure epoxy, Figure 5(a) shows a brittle fracture which is due to quite surface roughness, and river line pattern in fracture surface [10]. A lot of holes and cavities can be seen in Figure 5(b), which could be due to other small molecular chemical compounds adhered to the silica nanoparticles. This behaviour confirms the reason, as discussed earlier, why tensile strength drops drastically with increasing trend of silicas and nanoparticles addition in crystallinity in epoxy based nanocomposites was observed geneously dispersed in epoxy. A reduction in degree of crystallinity was mainly due to improper mixing of the nanoparticles. SEM micrograph showed white and agglomerate zones on fracture surfaces which indicate that silica sand nanoparticles are not homogeneously dispersed in epoxy. A reduction in degree of crystallinity in epoxy based nanocomposites was observed with increasing trend of silica sand nanoparticles addition in epoxy as shown by DSC analysis.

### 4. Conclusion

Epoxy-$\text{SiO}_2$ nanocomposites were successfully produced using Tronoh silica sand nanoparticles as reinforcement. The density of the epoxy-$\text{SiO}_2$ nanocomposites was increased from 1.157 g/cm$^3$ to 1.244 g/cm$^3$ with an average increment of 1.796%. The mechanical properties of the nanocomposites decrease with the addition of silica sand nanoparticles due to improper mixing of the nanoparticles. SEM micrograph showed white and agglomerate zones on fracture surfaces which indicate that silica sand nanoparticles are not homogeneously dispersed in epoxy. A reduction in degree of crystallinity in epoxy based nanocomposites was observed with increasing trend of silica sand nanoparticles addition in epoxy as shown by DSC analysis.

### Acknowledgments

The authors would like to thank the Universiti Teknologi PETRONAS Perak, Malaysia and University of the Punjab Lahore Pakistan for providing the necessary support to complete this research.

### References


