

Research Article

Adsorption of Hexavalent Chromium from Aqueous Solution Using Chemically Activated Carbon Prepared from Locally Available Waste of Bamboo (*Oxytenanthera abyssinica*)

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This study reports on the adsorption of Hexavalent Chromium from aqueous solutions using activated carbon prepared from bamboo (*Oxytenanthera abyssinica*) waste by KOH activation heating in an electrical furnace at 1073 K for 3 hrs. Batch adsorption experiments were also carried out as a function of pH, contact time, initial concentration of the adsorbate, adsorbent dosage, and temperature of the solution. Kinetic studies of the data showed that the adsorption follows the pseudo-second-order kinetic model. Thermodynamic parameters showed that adsorption on the surface of BWAC was feasible, spontaneous in nature, and exothermic between temperatures of 298 and 318 K. The equilibrium data better fitted the Freundlich isotherm model for studying the adsorption behavior of Hexavalent Chromium by BWAC. IR spectrum for loaded and unloaded BWAC was obtained using FT-IR spectrophotometer. Adsorption efficiency and capacity of Hexavalent Chromium were found to be 98.28% at pH 2 and 59.23 mg/g at 300 K.

1. Introduction

Out of the various toxic pollutants chromium and its compounds are considered as the most dangerous inorganic water pollutants. Chromium compounds present in the effluents as a result of electroplating, metal finishing, magnetic tapes, wood preservation, leather tanning, pigments, and chemical manufacturing industries [1, 2]. They can also present in rocks, soils, plants, and animals. This heavy metal occurs in the environment in two oxidation states: trivalent Cr(III) and hexavalent Cr(VI). Cr(III) is considered as an essential trace nutrient for human, while Cr(VI), in turn, is highly toxic [3, 4]. Because of its mutagenic and carcinogenic properties, it includes skin irritation to lung cancer, as well as kidney, liver, and gastric damage [5].

Owing to the different toxicities of Cr(VI), there is a great interest in the speciation and determination of chromium species in environment. A number of treatment methods

for the removal of chromium ions from aqueous solutions have been reported, mainly reduction, ion exchange, electrodialysis, electrochemical precipitation, evaporation, solvent extraction, reverse osmosis, chemical precipitation, and adsorption. Most of these methods suffer from drawbacks such as high operational costs and incomplete removal or the disposal of the residual metal sludge [6].

Adsorption by activated carbon is one of the effective techniques for Cr(VI) ion removal from wastewater because of the high surface area, highly porous character, and relatively low cost of the adsorbent [7, 8]. Activated carbon is especially known for the effective removal of organic chemicals, inorganic and heavy metal ion pollutants from wastewater in the laboratory as well as in various industries [9, 10]. Activated carbon can be synthesized by physical treatment, in which the surface of the carbonaceous material is exposed to a stream of gases at high temperature or chemical one where the carbonaceous material is exposed to

activation agents such as acids, hydroxides, and zinc chloride at low temperature. The major raw materials for production of activated carbon are wood [11], coal [12], nutshells [13–15], and fruit stones [16, 17]. The main disadvantage of activated carbon is the weak mechanical properties of its surface and that it is easily burned at high operation temperature [18].

Some low cost activated carbons used for removing of Hexavalent Chromium ions such as groundnut husk [19], agrowaste [20], neem leaves [21], sawdust [22], wheat bran [23], rice bran [24], sago waste [25], green coconut shell [26], hazelnut shell [27], olive stone [28], gingelly oil cake [29], and peanut shell [30, 31] have all been reported as useful for preparing adsorbents.

Activated carbons derived bamboo wastes have shown great potential for the removal of organic and inorganic waste from the aqueous solution. In present research we have used bamboo waste to develop activated carbon by chemical activation method using KOH for the removal of Hexavalent Chromium ion.

2. Materials and Method

2.1. Preparation of Bamboo Waste Activated Carbon (BWAC). Bamboo (*Oxytenanthera abyssinica*) waste was collected from Hosanna furniture manufacturing house, which is 230 Km from Addis Ababa (Ethiopia). The waste was air-dried for one month before use. Then it was cut into pieces approximately $1 \times 1 \text{ cm}^2$ in size. It was washed with distilled water and dried at 378 K for 12 hrs. This bamboo precursor was immersed in a potassium hydroxide solution (25% by weight/volume). The mixture was dried in an oven overnight at 378 K. The dried bamboo/KOH mixture then was put on a crucible placed in an electrical furnace (Model Nabertherm (R)) for carbonization. The heating rate of carbonization was $10^\circ \text{C}/\text{min}$ and continues until the final temperature of 1078 K was reached and it was kept at this temperature for 3 hrs. The produced activated carbon was then cooled down to room temperature. To remove remaining impurities such as ash, the synthesized BWAC was washed with 5% aqueous solution of HCl, followed by washing with distilled water several times until the pH of the washing solution was neutral. Prior to adsorption study HCl-treated activated carbon then was dried at 378 K for 12 hrs and ground into fine particle of $150 \mu\text{m}$ (sieve size) [32].

2.2. Preparation of Stock Solution. All chemicals used in this study were of analytical reagent grade and were used without further purification. Salt of $\text{K}_2\text{Cr}_2\text{O}_7$ was used for the preparation of the standard solutions for the study. The working solutions with different concentrations of the metal ions were prepared by appropriate dilutions of the stock solution with distilled water before use. The initial pH of the solution was adjusted accordingly with a pH meter. Thermostated water bath (Model Grant GLS400, England) was used as the medium for the process. The concentrations before and after adsorption of each metal ion were determined using atomic

absorption spectroscopy (AAS) (Model Analytik Jena Nov AA 300).

2.3. Characterization of the Adsorbent. Fourier transform infrared (FT-IR) spectra of dried unloaded BWAC and Hexavalent Chromium loaded BWAC were recorded at $400\text{--}4000 \text{ cm}^{-1}$ using Spectrum 65, Perkin Elmer model FT-IR spectrophotometer, to determine the surface functional groups. Proximate analysis of total ash content, moisture content, volatile matter, and fixed carbon was also performed.

2.4. Adsorption Study. The adsorption study was carried out by contacting 0.25 g of the activated carbon with 25 mL of the metal ion solution under different conditions for a period of time in a boiling tube. The adsorption studies are conducted at 300 K using thermostated water bath to determine the effect of pH, contact time, and initial metal ion concentration on the adsorption. The residual metal ion was analyzed using atomic absorption spectrophotometer. All experiments were carried out in triplicate, and the concentrations given are average values. The initial metal ion concentration in the test solution and the adsorbent dosage were varied to investigate their effect on the adsorption kinetics. The adsorption studies were carried out at different temperatures. This is used to determine the effect of temperature on the thermodynamic parameters. The amount of adsorption at time t , q_t (mg/g), was calculated using the following relation [33]:

$$q_t = \frac{(C_0 - C_t)V}{W}, \quad (1)$$

where C_t (mgL^{-1}) is the liquid phase concentrations of metal ion at any time and C_0 (mgL^{-1}) is the initial concentration of the metal ion in solution. V is the volume of the solution (L) and W is the mass of dry adsorbent (g).

The percentage removal of Hexavalent Chromium solution was calculated by using the following equation:

$$\% \text{Adsorption} = \frac{(C_0 - C_e)}{C_0} \times 100, \quad (2)$$

where C_0 and C_e (mgL^{-1}) are the initial and equilibrium concentrations of Hexavalent Chromium ion in solutions.

3. Result and Discussion

3.1. Characterization of the Adsorbent. Activated carbons are widely used as adsorbents due to their high adsorption capacity, high surface area, microporous structure, and a high degree of surface. Some important physicochemical characteristics of BWAC are given in Table 1. Moisture content of the carbon has no effect on its adsorptive power; it dilutes the carbon which is necessary for the use of additional weight of carbon during the treatment process. The BWAC samples were determined using standard test method for moisture in AC [38]. The lower ash content and volatile matter are attributed to lower inorganic content and higher fixed carbon. Higher value of fixed carbon shows that the adsorbent is having more efficiency and stability [39, 40].

TABLE I: Physiochemical characteristics of BWAC.

| Parameter | Value |
|---------------------------------|-------|
| Moisture content (%) | 9.56 |
| Volatile matter (%) | 4.66 |
| Ash content (%) | 21.66 |
| Fixed carbon (%) | 73.68 |
| Particle size (μm) | 150 |
| pH | 7.00 |

FT-IR spectrum is an essential tool to identify the surface functional groups which can contribute significantly to enhance adsorption efficiency of the activated carbon by surface complexation. The spectra show that the activated carbon spectrum was closely identical to bamboo charcoal. A broad peak around 3458 cm^{-1} was attributed to O-H stretching vibration of the hydroxyl group. A peak around 2923 cm^{-1} was attributed to aliphatic methyl asymmetric C-H stretching. The peak observed around 1577 cm^{-1} was because of CH_2 bending. The peak observed around 1457 cm^{-1} can be attributed to the CH_3 bending. The bands around 1196 cm^{-1} region were alcoholic C-O stretching, which produce strong bands. The very weak absorption which was observed at 850 and 603 cm^{-1} was attributed to the long chain band of aliphatic alkane.

Figure 1 shows the FT-IR spectra of activated carbon before and after adsorption of chromium onto BWAC. It clearly shows that after the adsorption of Hexavalent Chromium on BWAC there is a small shift in frequency values and some of the frequency regions were absent. This observation indicated the participation of adsorption of Hexavalent Chromium on bamboo waste activated carbon (BWAC).

3.2. Effect of pH on Adsorption. The effect of pH on the adsorption of the metal ions was carried out within the range that was not influenced by the metal precipitation. The procedure used is similar to those earlier reported [33].

It can be seen in Figure 2 that the maximum of Hexavalent Chromium adsorption (98.28%) occurs at the lowest pH value. This finding has been reported by several investigators [41, 42], who have found that Hexavalent Chromium removal by activated carbon is enhanced in the acidic range of pH. The favorable effect of low pH can be attributed to the neutralization of negative charges on the surface of the adsorption by excess hydrogen ions, thereby facilitating the diffusion of hydrogen chromate ions (HCrO_4^-) and their subsequent adsorption. According to Muhammad et al. [43], (HCrO_4^-) is the dominant and ionic form of Hexavalent Chromium between pH 2.0 and 4.0. This ionic form was found to be preferentially adsorbed on the surface of carbon. The negative charges could result from oxygenated functional groups of basic character such as lactones or hydroxyl groups, physically adsorbed at the surface of the pores of activated

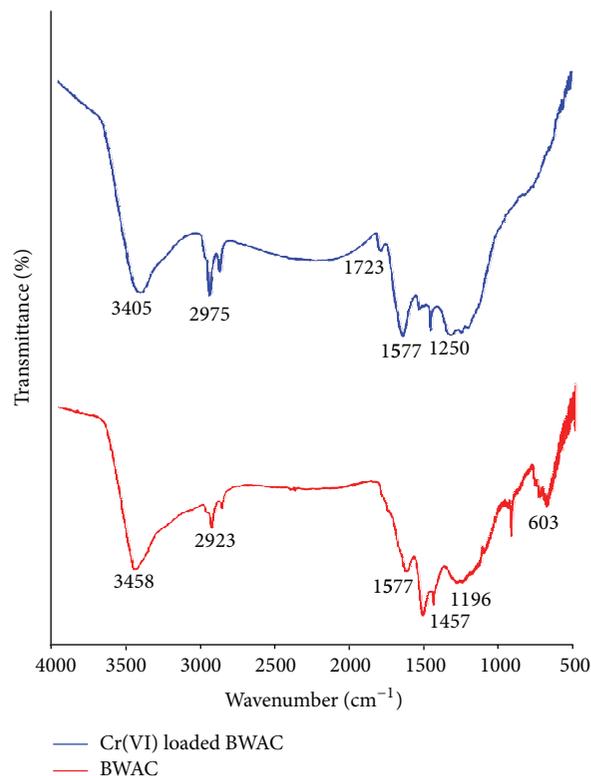


FIGURE 1: FT-IR spectra of BWAC before and after adsorption of Hexavalent Chromium.

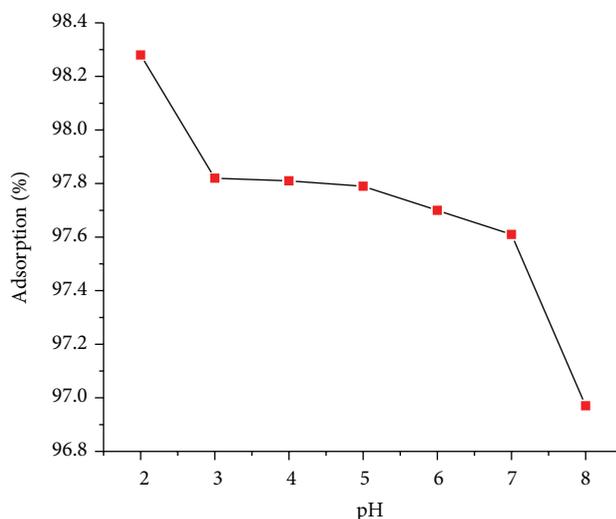


FIGURE 2: Effect of pH for adsorption of Hexavalent Chromium.

carbon. In view of this observation the optimum pH for Hexavalent Chromium adsorption is taken to be 2.

3.3. Effect of Contact Time on Adsorption. The adsorptions of the metal ions by activated carbon were studied at various time intervals (3–120 min) and at a concentration of 100 mg/L. Figure 3 shows that chromium uptake is fast for the first 3–20 min, respectively, and, thereafter, they proceed

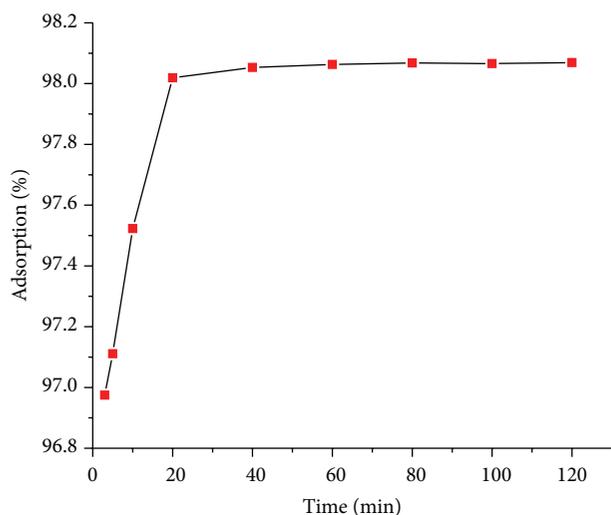


FIGURE 3: Effect of contact time for adsorption of Hexavalent Chromium.

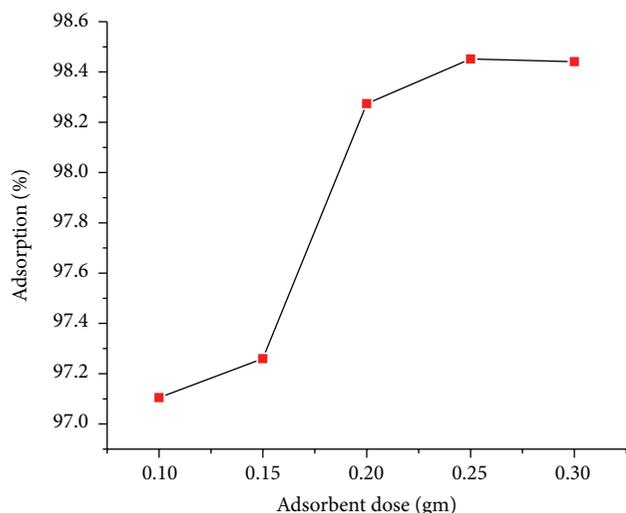


FIGURE 4: Effect of adsorbent dosage for adsorption of Hexavalent Chromium.

at a slower rate and finally attain saturation. The initial fast reaction may be due to the increased number of vacant sites available at the initial stage; as a result there exists increased concentration gradient between adsorbate in solution and adsorbate in the adsorbent. Generally, by the time adsorption involves a surface reaction process, the initial adsorption is fast. Then, a slower adsorption would follow as the available adsorption site which is gradually decreased. This is due to the fact that a large number of vacant surface sites are available for adsorption during the initial stage, and after a lapse of time the remaining vacant surface sites are difficult to be occupied due to repulsive forces between the solute molecules on the solid and bulk phases [44]. Maximum percentage of adsorption (98.019% in 100 mg/L of solution) occurs at 20 min; after that the percentage adsorption remains uniform.

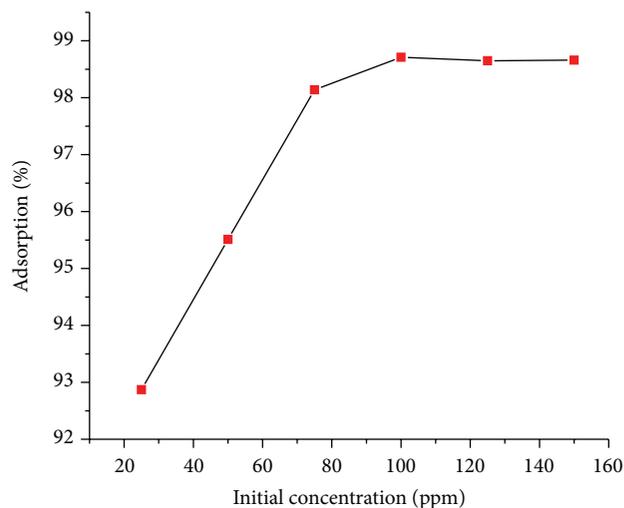


FIGURE 5: Effect of initial metal ion concentration for adsorption efficiency of Hexavalent Chromium.

3.4. Effect of Adsorbent Dosage. Figure 4 depicts effect of adsorbent dosage on the adsorption of chromium on the BWAC. It can be seen that the percent adsorption increases from 97.105 to 98.45% with an increase in the dose of BWAC from 0.1 to 0.25 g and remained nearly constant at adsorbent quantities higher than 0.25 g. This is due to the greater availability of adsorption sites of adsorbent and thus making easier penetration of Cr(VI) to the adsorption sites [44]. Since the quantity of metal ion is constant, an increase in the amount of adsorbent above a quantity that can completely adsorb the available Cr(VI) had no apparent effect on further increase of percent adsorption. The adsorption capacity decreases from 24.28 to 8.2 for Hexavalent Chromium as dosage increased.

3.5. Effect of Initial Concentration on Adsorption. The effect of initial Hexavalent Chromium concentration on the adsorption efficiency of BWAC under optimum conditions of pH and contact time is shown in Figure 5. The adsorption efficiency increased from 92.87 to 98.71% for Hexavalent Chromium with increasing initial concentration from 25 to 150 mg/L but the solution reached equilibrium at 100 mg/L and after that no significant change occurred in adsorption.

The adsorption capacity increases from 9.87 to 59.23 mg/g for Hexavalent Chromium as the initial metal ion concentration increased from 25 to 150 mg/L. This is because a higher initial concentration enhanced the driving force between the aqueous and solid phases and increased the number of collisions between metal ions and adsorbents [45]. However, the actual percentage adsorption of the metal ions from solution increased with the increase in the initial metal ion concentrations. This may be due to the fact that, at lower concentrations, adsorption of the metal ions occurred slowly and further increase in initial metal ion concentration led to a competition for available bonding sites on the BWAC surface by the metal ions and thus increased adsorption. Similar adsorption procedures have also been reported by other researchers [46]. The adsorption capacity of an adsorbent

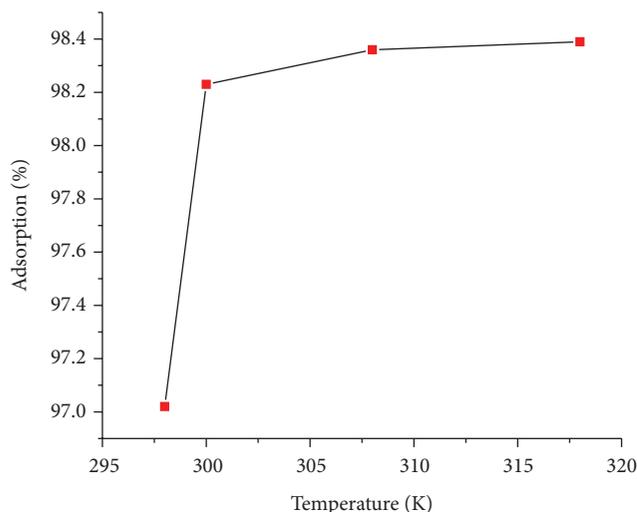


FIGURE 6: Effect of temperature for adsorption of Hexavalent Chromium.

which is obtained from the mass balance equation on the adsorbate in a system with solution volume is often used to acquire the experimental adsorption isotherms [47].

3.6. Effect of Temperature on Adsorption. Temperature is a highly significant parameter in the adsorption process. Experiments were performed at different temperatures (298 K, 300 K, 308 K, and 318 K) at optimum pH and contact time. It was observed that the percentage of adsorption increases from 97.02 to 98.39 for Hexavalent Chromium ions with the rise in temperature from 298 to 318 K. It is evident from Figure 6 that adsorption increases with the rising temperature because this adsorbent is not homogenous, and implying the active energy of adsorption sites is different. Therefore, at low temperature, the adsorption sites with lower active energy were occupied first, and the other sites with higher active energy were occupied as the temperature increases [29].

The rise of adsorption capacity with temperature was due to the increase in kinetic energy of adsorbent particles. Thus the collision frequency between adsorbent and adsorbate increases, which results in the enhanced adsorption onto the surface of the adsorbent. Secondly, at high temperature due to bond rupture of functional groups on adsorbent surface increases active adsorption sites, which may also lead to enhanced adsorption [48].

3.7. Adsorption Isotherms. Isotherm studies are essential to interpret the adsorption process adequately. Several models have been used to describe experimental data for adsorption isotherms. However, among these, the Langmuir and Freundlich isotherms are the most appropriate models for this study. According to the Langmuir isotherm, adsorption occurs at homogenous sites and forms a monolayer. In other words, once adsorbate is attached to a site, no further

adsorption can take place [13]. The linear form of Langmuir isotherm equation is given as

$$\frac{C_e}{q_e} = \frac{C_e}{q_m} + \frac{1}{q_m b_L}, \quad (3)$$

where q_e (mg/g) is the equilibrium concentration of Hexavalent Chromium in the adsorbed phase and C_e (mg/L) is the equilibrium concentration in the liquid phase. Langmuir constants, which are related to the adsorption capacity (q_m) and energy of adsorption (b_L), can be calculated from the slope of the linear plot of C_e/q_e versus C_e ; a straight line with slope $1/q_{max}$ and intercept of $1/q_{max}b_L$ is obtained. The essential characteristics of the Langmuir equation can be expressed in terms of a dimensionless factor, R_L which is given as

$$R_L = \frac{1}{1 + b_L C_0}, \quad (4)$$

where C_0 is the highest initial Hexavalent Chromium ion concentration (mg/L). The values of separation factor R_L have its usual significance.

Freundlich isotherm gives the relationship between equilibrium liquid and solid phase capacity based on the multilayer adsorption properties consisting of heterogeneous surface of the adsorbent. This isotherm is derived from the assumption that the adsorption sites are distributed exponentially with respect to the heat of adsorption [17]. The linear form of Freundlich isotherm is

$$\log q_e = \log K_f + \frac{1}{n} \log C_e, \quad (5)$$

where q_e is the amount adsorbed at equilibrium (mg/g), K_f and n are the Freundlich constant, $1/n$ is the heterogeneity factor which is related to the capacity and intensity of the adsorption, and C_e is the equilibrium concentration (mgL^{-1}). The values of K_f and $1/n$ can be obtained from the slope and intercept of the plot of $\log q_e$ against $\log C_e$. However, present investigation attempted to analyze the above-mentioned isotherm parameters at 300 K and the correlation coefficients R^2 were calculated by fitting the experimental equilibrium data for Hexavalent Chromium ion BWAC system using both Langmuir and Freundlich isotherms, which is presented in Table 2.

The results clearly show that the adsorption of Hexavalent Chromium on BWAC fits well with the Freundlich model. The fact that the Freundlich model is a good fit to the experimental adsorption data suggests physical adsorption as well as a heterogeneous distribution of active sites on the BWAC surface. The observed correlation coefficients for Freundlich isotherms were 0.775. If the value of n is equal to unity, the adsorption is linear. If the value of constant n is below unity, it implies that the adsorption process is unfavorable, and if the value of n is above unity, adsorption is favorable [33]. In the present study, the value of n at equilibrium was above unity, suggesting favorable adsorption. Furthermore, the values of the dimensionless factor, R_L , were between 0 and 1 which suggest a favorable adsorption between BWAC and Hexavalent Chromium ion.

TABLE 2: Results of isotherm models for the adsorption of Hexavalent Chromium by BWAC at 300 K.

| Adsorption isotherms constants | Values |
|---------------------------------|--------|
| Langmuir isotherm | |
| q_m (mg/g) | 125 |
| b_L (L/mg) | 8.23 |
| R^2 | 0.018 |
| Freundlich isotherm | |
| K_f | 0.644 |
| $1/n$ | 0.932 |
| R^2 | 0.775 |
| Separation factor, R_L (mg/L) | 0.012 |

TABLE 3: Kinetics parameters for the adsorption of Hexavalent Chromium on BWAC at 300 K.

| Kinetic constants | Values |
|--|--------|
| Pseudo-first-order | |
| q_e (exp.)(mg/g) | 1.21 |
| q_e (cal.)(mg/g) | 1 |
| $k_1 \times 10^{-4}$ (min ⁻¹) | 1.16 |
| R^2 | 0.842 |
| Pseudo-second-order | |
| q_e (cal.)(mg/g) | 1.2 |
| k_2 (mg/g/min) | 0.834 |
| R^2 | 0.997 |
| Intraparticle diffusion | |
| k_d (mg/g/min) | 0.009 |
| C (mg/g), intraparticle diffusion constant | 0.34 |
| R^2 | 0.908 |

exp.: experimental result; cal.: calculated result.

3.8. *Adsorption Kinetic Studies.* In order to evaluate the kinetic parameters, pseudo-first-order and pseudo-second-order models were implemented to analyze the experimental data. The pseudo-first-order equation can be expressed as [46]

$$\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303}t, \quad (6)$$

where q_e and q_t represent the amount of adsorbed (mg/g) at equilibrium and at any time t and k_1 is the first-order rate constant (min⁻¹). From the plots of $\log(q_e - q_t)$ versus t in Figure 7, k_1 can be calculated from the slope and theoretical q_e can be obtained from intercepts.

Pseudo-second-order equation can be given by

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e}t, \quad (7)$$

where k_2 is the rate constant of second-order adsorption. The linear plots of t/q_t versus t determine $1/q_e$ as slope and $1/k_2 q_e^2$ as intercepts. The linear plots of pseudo-second-order model are shown in Figure 7.

The correlation coefficient, R^2 , of pseudo-first-order kinetics was 0.872 but the calculated q_e (mg/g) value obtained

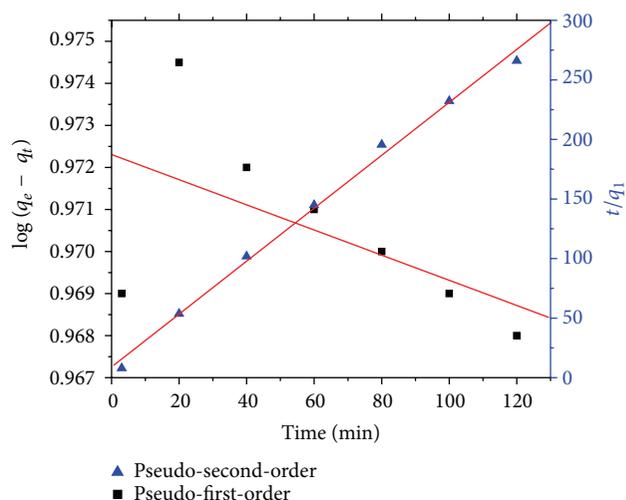


FIGURE 7: Kinetics plot for the adsorption of Hexavalent Chromium onto BWAC. (Blue triangle showing pseudo-second- and black squares is representing pseudo-first-order rate kinetics.)

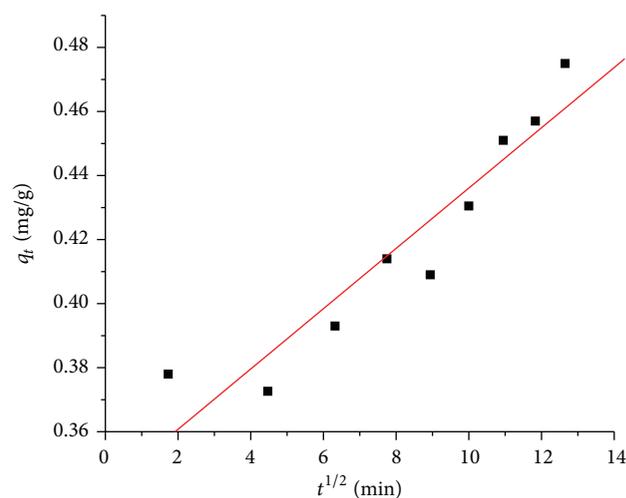


FIGURE 8: Intraparticle diffusion curve for adsorption of Hexavalent Chromium onto BWAC at 300 K temperature.

from pseudo-first-order kinetics did not agree well with the experimental (mg/g) values as shown in Table 3. Thus it can be concluded that it is not appropriate to use the pseudo-first-order kinetic model to predict the adsorption kinetics for the adsorption of Hexavalent Chromium onto BWAC.

On the contrary, the correlation coefficient, R^2 , for the second-order kinetic model was almost equal to unity for all the concentrations signifying the applicability of the model. Moreover, the calculated q_e (mg/g) values obtained from pseudo-second-order kinetics were in good agreement with the experimental (mg/g) values (Table 3). Thus it appeared that the system under study is more suitably described by pseudo-second-order kinetics which was based on the assumption that the rate limiting step may be chemisorptions concerning valences forces through sharing and exchange of electrons. The pseudo-second-order kinetics model has been

TABLE 4: Thermodynamic parameters for the adsorption of Hexavalent Chromium ion on BWAC at different temperatures.

| T (K) | $\ln K_c$ | ΔG^0 (kJ/mol) | ΔH^0 (kJ/mol) | ΔS^0 (kJ/mol·K) |
|-------|-----------|-----------------------|-----------------------|-------------------------|
| 298.2 | 3.340 | -8.28 | -18.912 | 0.06614 |
| 308.2 | 3.7145 | -9.518 | | |
| 318.2 | 7.3666 | -19.488 | | |

TABLE 5: Comparison of adsorption capacity of different adsorbents for the adsorption of Hexavalent Chromium.

| Adsorbents | Adsorbent capacity (mg/g) | References |
|--|---------------------------|------------|
| Wood apple shell | 13.74 | [7] |
| <i>Ricinus communis</i> seed shell active carbon | 7.761 | [33] |
| Palm shell activated carbon | 12.6 | [34] |
| PEI/palm shell activated carbon | 20.5 | [35] |
| Acid-modified waste activated carbon | 10.93 | [36] |
| Fe-modified bamboo carbon | 35.7 | [37] |
| BWAC (bamboo waste activated carbon) | 59.23 | This work |

successfully applied to several adsorption systems as reported in [46].

The amount of Hexavalent Chromium adsorbed per unit mass of adsorbent at time t , q_t , as a function of the square root of the contact time, $t^{1/2}$ (Figure 8), was examined using the intraparticle diffusion model (Table 3) which is based on the theory proposed by Weber and Morris [49]:

$$q_t = k_d t^{1/2} + C, \quad (8)$$

where k_d (mg/g/min) is the intraparticle diffusion coefficient which was calculated from the slope of the linear portion of curves and C (mg/g) is intraparticle diffusion constant, that is, intercept of the line (mg/g). It is directly proportional to the boundary layer thickness. It is assumed that the larger the intercept, the greater the contribution of the surface adsorption in the rate-controlling step.

Intraparticle diffusion plays a significant role in controlling the kinetics of the adsorption process, if the plot of q_t versus $t^{1/2}$ yields a straight line passing through the origin, with the slope giving the rate constant, k_d , and C . If the lines do not pass through the origin it is indicative of some degree of boundary layer control and this further shows that the intraparticle diffusion is not the only rate limiting step, but other kinetic models may also control the rate of adsorption [34, 50].

3.9. Thermodynamic Study. The thermodynamic parameters that help us to understand the nature of the adsorption of Cr(VI) ion on adsorbents are the standard change in Gibbs free energy (ΔG°), the standard change in entropy (ΔS°), and the standard change in enthalpy (ΔH°). The enthalpy change (ΔH°) from 298.2 to 318.2 K was computed from the following equation:

$$\ln K_c = \frac{\Delta S^\circ}{R} - \frac{\Delta H^\circ}{RT}, \quad (9)$$

where ΔH° (kJ · mol⁻¹) and ΔS° (kJ · mol⁻¹ · K⁻¹) were calculated from the slope and intercept of the linear plot

of $\ln K_c$ versus $1/T$. However, the calculated values of thermodynamic parameters are listed in Table 4. The negative value of enthalpy change confirms the exothermic nature of the adsorption process. The enthalpy value for adsorption process may be used to distinguish between chemical and physical adsorption. For chemical adsorption, values of enthalpy change range from -83 to -830 kJ/mol, while for physical adsorption they range from -8 to -25 kJ/mol. The low values of ΔH give clear evidence that the interaction of Hexavalent Chromium and BWAC was weak suggesting physical adsorption process [50]. The positive value of entropy, ΔS° , represents an increase in the degree of freedom of the adsorbed species which indicates that some changes occur in the internal structure of BWAC during the adsorption process. The negative values of Gibbs free energy, ΔG° demonstrate that the adsorption is rapid and spontaneous. The negative value of ΔG° ensures the feasibility of the process. Generally, ΔG° values range from 0 to -20 KJ/mol for physical adsorption and -80 to -400 KJ/mol for chemical adsorptions [34]. In this study, the ΔG° values ranged from -6.347 to -19.488 KJ/mol, indicating that adsorption is mainly physical.

3.10. Comparison of Hexavalent Chromium Adsorption with Different Adsorbents. The adsorption capacity of the adsorbents for the adsorption of Hexavalent Chromium has been compared with those of others reported in the literature and the values of adsorption capacity as presented in Table 5. The experimental data of the present investigation were compared with reported values. Results of our investigation revealed that BWAC has the highest percent adsorption and adsorption capacity.

4. Conclusion

Experimental findings of this work suggested that the adsorption of Hexavalent Chromium on BWAC is a physical adsorption process attaining equilibrium within 20 min. Both Freundlich and Langmuir models were used to fit the data

to estimated model parameters but the overall data is better fitted by Freundlich isotherm. The kinetic studies conducted using the Weber and Morris equation showed that the adsorption mechanism involves intraparticle diffusion but it was not the fully operative mechanism in the adsorption of Hexavalent Chromium by BWAC. The pseudo-second-order kinetic model was found to be a better fit for the adsorption of Hexavalent Chromium by BWAC. Thermodynamic studies predict that the adsorption is feasible, spontaneous, and exothermic in nature at temperatures of 298.2, 308.2, and 318.2 K with negative values of standard change in Gibbs free energy (ΔG°), enthalpy (ΔH°), and positive values of standard entropy change (ΔS°).

Conflict of Interests

The authors declare that there is no conflict of interests.

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