Research Article

Effect of Thermal Environment on the Mechanical Behaviors of Building Marble

Haijian Su, Hongwen Jing, Qian Yin, and Liyuan Yu

State Key Laboratory for Geomechanics and Deep Underground Engineering, China University of Mining and Technology, Xuzhou, Jiangsu 221116, China

Correspondence should be addressed to Haijian Su; hjsu@cumt.edu.cn

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High temperature and thermal environment can influence the mechanical properties of building materials worked in the civil engineering, for example, concrete, building rock, and steel. This paper examines standard cylindrical building marble specimens (Φ50 × 100 mm) that were treated with high temperatures in two different thermal environments: vacuum (VE) and airiness (AE). Uniaxial compression tests were also carried out on those specimens after heat treatment to study the effect that the thermal environment has on mechanical behaviors. With an increase in temperature, the mechanical behavior of marble in this study indicates a critical temperature of 600°C. Both the peak stress and elasticity modulus were larger for the VE than they were for the AE. The thermal environment has an obvious influence on the mechanical properties, especially at temperatures of 450–750°C. The failure mode of marble specimens under uniaxial compression is mainly affected by the thermal environment at 600°C.

1. Introduction

In the civil engineering, the high-temperature disaster becomes more and more frequent, such as building and tunnel fire. Thermal damage can lead to changes in the physical and mechanical behaviors and to variations in the mineral composition and microstructure of building materials [1, 2]. The problem of thermal damage has also been observed in other projects, such as underground coal gasification, geothermal resource mining, and the deep storage of high-level nuclear wastes [3–5]. How the physical and mechanical behaviors of building materials are affected by high temperatures has become a hot topic.

Rock (e.g., sandstone, marble, and granite), as the significant building material, is widely used in the civil engineering [6, 7]. In the past few years, numerous, significant, experimental studies were conducted to quantify the effect of thermal damage on rock. Semicircular bending (CSTSCB) specimens of certain Indian rocks, including Manoharpur sandstone, Bellary dolerite, and Dholpur sandstone, were subjected to the three-point bending test by Mahanta et al. [8], who studied the effects of thermal treatment on mode I fracture toughness. The influence of temperature and rock type on the stress-strain curve, peak strength, and elastic modulus was investigated by Zhang et al. [9], who conducted MTS 815 uniaxial compression tests on marble, limestone, and sandstone specimens at high temperatures (ranging from room temperature to 800°C). Yin et al. [10] conducted an experimental comparison of the mechanical properties of granite after high-temperature treatment and under a high temperature. Their results show that, for granite under a high temperature, the peak stress is lower, the peak strain is greater, and the elastic modulus is smaller compared with that observed after high-temperature treatment. The change laws for the fracture toughness and tensile strength of rock samples that had experienced rapid thermal cooling under different temperatures and cyclic thermal cooling treatments, respectively, were obtained by Kim et al. [11]. Gonzalez-Gomez et al. [12] investigated the change features of the physical properties (including sample color, mass loss, chemical composition, and porosity) of four limestones that were extracted from the Yucatan Peninsula (Mexico) and subjected to different high temperatures. The triaxial compressive behaviors of coarse marble specimens after
high-temperature treatment (ranging from 20 to 600 °C) under different confining pressures (ranging from 0 to 40 MPa) were studied by Yao et al. [13], who proposed an empirical model of the negative exponential type that described the peak strength well. Liu et al. [14] obtained the change laws of fracture toughness, splitting tensile strength, and elastic modulus for rocks after high-temperature treatment, based on a splitting tensile test conducted on flattened Brazilian disc specimens.

In the civil engineering, the mechanical behaviors of building rock are also affected by the thermal environment in the process of fire disaster [15–17]. Existing studies involving the heat treatment of rock indicate that the effect on the thermal environment is limited. In this study, heat treatments were applied to building marble specimens within two different thermal environments: vacuum and airiness. After the heat treatment, uniaxial compression tests were conducted to determine the effect that the thermal environment has on the physical and mechanical properties of the specimens.

2. Experimental Work

The building marble material used in this study is from a quarry in the southeast region of Linyi City, Shandong Province of China. In its natural state, the marble is white in color and does not have a macroscopic texture. The average density of this marble is 2.83 g/cm³, with the main mineral compositions of calcite, dolomite, and quartz. In accordance with the ISRM and the laboratory’s strict processing requirements, standard cylindrical specimens with a diameter of 50 mm and a height of 100 mm were prepared for this experimental project. The maximum deviation in the specimen height was ±0.3 mm, and the maximum nonparallelism between ends was ±0.05 mm.

Heat treatment of the marble specimens was accomplished using an MXQ1700 box-type furnace produced by Shanghai Micro-X Furnace Co. Ltd. of China. In the heat treatment for the VE (Figure 1), air was eliminated from the furnace chamber using an air pump until the pressure in the chamber was below an atmospheric pressure of 0.04 MPa (an approximate vacuum environment, namely, VE). Next, the marble specimens were heated to a designated temperature at a rate of 5 °C per minute, which was maintained for 2 hours. Finally, the marble specimens in this environment were passively cooled to room temperature. When the heat treatment for the airiness environment (namely, AE) was implemented, both the inlet and outlet valves of the furnace chamber were turned on to allow air to enter the chamber freely and slowly. The processes for the heating and cooling treatments were same as those implemented for the VE. In this study, there were six designated heating temperatures $T$: 200, 300, 450, 600, 750, and 900 °C.

After the heat treatment, the marble specimens were subjected to a uniaxial compression test using an MTS815.2 rock mechanics servocontrolled testing system.
Figure 2: Axial stress-strain curves of marble specimens under uniaxial compression: (a) 25, (b) 300, (c) 600, and (d) 900°C.

Figure 3: Effect of temperature on the mechanical parameters of marble specimens: (a) peak stress and (b) elasticity modulus.
loading at a loading rate of $3.0 \times 10^{-3}$ mm per second was used in the test. Vaseline was evenly smeared on both ends of the specimens to eliminate the effects of end friction on the testing result. The marble specimens in their natural state (25°C) that had not undergone the heat treatment were also tested.

3. Result Analysis

3.1. Mechanical Parameters. Figure 2 provides the axial stress-strain curves of marble specimens under uniaxial compression. Figure 3 shows the effect of temperature on the peak stress and elasticity modulus. In the natural state, the average values of peak stress and elasticity modulus are 80.69 MPa and 20.05 GPa, with the dispersion coefficients (namely, the ratio of standard deviation to average value) of 0.03 and 0.13, respectively. With an increase in temperature, the peak stress and elasticity modulus decrease gradually, and this process can be divided into two stages from 600°C.

3.1.1. First Stage. At 200–600°C, both the peak stress and elasticity modulus present a slowly decreasing trend with a small extent. As the temperature rises from 200 to 600°C, the peak stress and elasticity modulus decrease from 81.42 MPa and 19.95 GPa to 74.08 MPa and 14.44 GPa for the VE, with the reduction extents of 9.01% and 27.62%, respectively, and from 79.80 MPa and 19.66 GPa to 65.77 MPa and 12.23 GPa for the AE, with the reduction extents of 17.58% and 37.79%, respectively. The extent of change of the elasticity modulus is slightly larger than that of the peak stress.

3.1.2. Second Stage. At 600–900°C, the peak stress and elasticity modulus decrease sharply. As the temperature is
raised from 600 to 900 °C, the reduction extent of peak stress is 61.96% for the VE and 63.52% for the AE, respectively, and that of the elasticity modulus is 80.54% for the VE and 82.58% for the AE, respectively.

Figure 3 indicates a critical temperature of 600 °C for the marble in this study, with obvious differences in mechanical properties at temperatures above or below the critical temperature. Figure 4 presents the variations of mechanical parameters of rocks with temperature in other literatures. Wu et al. [18] investigated the variations of dynamic compressive strength and dynamic tensile strength of marble specimens, which present the same law found in this study. Ozguven and Ozcelik [19] show the change curves of compressive strength of four types of marble, with different critical temperatures. Zhang and Lu [20, 21] investigated the variations of compressive strength and tensile strength of Linyi sandstone with the temperature. The study of Zhang et al. [9] presents a critical temperature of 700 °C for the peak strength of limestone. From Figures 3 and 4, it is clear that the change trend and critical temperature of the mechanical parameters of rocks might be influenced by the stress state, lithology, and mineral grain size owing to a complicated geological process.

Figure 3 also shows the differences in the mechanical parameters of two different thermal environments (Δ). The peak stress and elasticity modulus of the marble specimen, after heat treatment, in the AE are each less than that for the VE. Δ of peak stress is between 1.62 and 8.31 MPa and that of elasticity modulus is between 0.29 and 2.21 GPa. Both the peak stress and elasticity modulus reveal a uniform phenomenon: the mechanical parameters of the marble specimens are obviously affected by the thermal environment particularly at temperatures of 450–750°C.

### 3.2 Ultimate Failure Mode

After heat treatment, there are four typical modes of failure in marble specimens under uniaxial compression: tensile, tensile-shear, shear, and smash failure (Figure 5).

(i) **Tensile failure**: This failure mode is most common in hard or brittle rock. When there is one or more splitting, fracture planes on the specimen run in the same direction as the axial loading.
(ii) Tensile-shear failure: It occurs when there are both tensile and shear failure. The tensile and shear fracture planes could intersect or be independent of one another.

(iii) Shear failure: One or more shear planes occur on the specimen, and the shear plane is located at an angle in the direction of axial loading. The shear failure in this paper has some difference from the conventional shear failure, in that a few secondary tensile cracks are also observed. However, rock failure mainly depends on the shear failure.

(iv) Smash failure: After testing, specimen can present smash failure. Many powders are observed from the fractured blocks. The extent of failure in the specimen is extremely serious.

Table 1 shows the effect of temperature and thermal environment on the failure mode of the marble specimens under uniaxial compression. Marble specimens in a natural state (25°C) undergo tensile failure. With an increase in temperature, the failure mode changes gradually from tensile to tensile-shear, tensile-shear to shear, and then shear to smash failure. At \( T = 200°C \), all of the specimens after heat treatment in the two thermal environments experienced tensile failure. When the temperature is between 300 and 450°C, all marble specimens experience tensile-shear failure. However, when \( T = 600°C \), the thermal environment has an apparent effect upon the failure mode: tensile-shear failure occurs in the VE and shear failure occurs in the AE. When the temperature is 750 and 900°C, shear failure and smash failure, respectively, occur in both thermal environments.

4. Discussion

In this discussion, density and microscopic feature of marble before and after heat treatment are investigated. Figure 6 shows the effect of temperature on \( \rho_a/\rho_b \) of marble. Figure 7 also presents the difference of density in different thermal environments, particularly at temperatures of 750~900°C. This phenomenon can be verified by the microscopic feature, as shown in Figure 7. As \( T = 900°C \), the
primary minerals in the marble present thermal decomposition (such as $\text{CaCO}_3 \rightarrow \text{CaO} + \text{CO}_2$). For the AE, gases from mineral thermal decomposition are continually replaced by air. And the extent of the thermal decomposition is more violent. In contrast, for the VE, gases from mineral thermal decomposition are absorbed on the surface of the specimen. This could restrain the thermal decomposition and lead to a reverse reaction. Therefore, mineral thermal decomposition for the AE is more serious than that for the VE.

The nuclear magnetic resonance (NMR) tests were also conducted on the marble specimens (at 25, 450, and 750°C, resp.). $T_2$ curves and magnetic resonance imaging (MRI) are shown in Figure 8. The $T_2$ curve of specimens in the natural state presents a three-peak feature. The peak points are resulted at $T_2 = 0.23$, 5.17, and 126.04 ms, with the signal amplitudes of 61.40, 113.13, and 159.64, respectively. The MRI image also shows homogeneity of the marble in this study. The $T_2$ curves of marble after 450°C heat treatment also present a three-peak feature, while the results of $T_2$ curve and MRI image have no significant difference between that for the VE and AE. At 750°C, MRI image displays a more serious damage for the AE than for the VE. For the VE, as the temperature increases from 25 to 750°C, the $T_2$ curve trend transforms from a three-peak feature to an approximate single-peak feature with the gradual degradation of the first two peaks. While at 750°C for the AE, the $T_2$ curve shows an approximate two-peak feature, with the signal amplitudes of 1798.08 and 1437.67 at $T_2 = 0.52$ and 33.70, respectively.

5. Conclusion

In this study, building marble after heat treatment with two different thermal environments was subjected to a uniaxial compression test. Their mechanical properties were measured, and the following conclusions can be drawn:

1. With an increase in temperature, the mechanical parameters (peak stress and elasticity modulus) of marble specimens decrease gradually in this study, with a critical temperature of 600°C.

2. The ultimate failure mode of marble specimens changes from tension to tensile-shear to shear to smash failure with the increase of temperature. The failure mode presents a different feature between the AE and VE at the temperature of 600°C.
(3) The thermal environment has an obvious influence on the mechanical behaviors of marble specimens under uniaxial compression, especially at 450–750°C. This effect of thermal environment on other rocks needs a further investigation.

Conflicts of Interest

The authors declare that they have no conflicts of interest.

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