Research Article

Hybrid Dislocated Control and General Hybrid Projective Dislocated Synchronization for Memristor Chaotic Oscillator System

Junwei Sun,^{1,2} Chun Huang,^{1,2} and Guangzhao Cui^{1,2}

¹ College of Electric and Information Engineering, Zhengzhou University of Light Industry, Zhengzhou 450002, China

² Henan Key Lab of Information-Based Electrical Appliances, Zhengzhou University of Light Industry, Zhengzhou 450002, China

Correspondence should be addressed to Junwei Sun; junweisun@yeah.net

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Some important dynamical properties of the memristor chaotic oscillator system have been studied in the paper. A novel hybrid dislocated control method and a general hybrid projective dislocated synchronization scheme have been realized for memristor chaotic oscillator system. The paper firstly presents hybrid dislocated control method for stabilizing chaos to the unstable equilibrium point. Based on the Lyapunov stability theorem, general hybrid projective dislocated synchronization has been studied for the drive memristor chaotic oscillator system and the same response memristor chaotic oscillator system. For the different dimensions, the memristor chaotic oscillator system and the other chaotic system have realized general hybrid projective dislocated synchronization. Numerical simulations are given to show the effectiveness of these methods.

1. Introduction

Memristor is considered to be the missing 4th passive circuit element postulated in 1971 [1]. And it took scientists almost 40 years to invent such a practical device until a team at Hewlett-Packard Labs announced the development of a memristor in Science on May 1, 2008 [2], by titanium dioxide thin films. Memristor takes its place along other three existing elements such as the resistor, capacitor, and inductor and shares many properties of resistors such as the unit of measurement ohms.

Chaos is an important nonlinear phenomenon and can be observed in many practical applications of various fields, including biology, chemistry, and engineering. Since the effect of chaotic system is usually undesirable, irregular, and unpredicted due to its sensitivity to initial conditions, it is necessary that the chaotic dynamics of a system can be controlled. During the last several decades, controlling chaotic systems have been widely studied due to undesirable or harmful chaotic behaviors under many circumstances. Controlling chaos has been focused on by many researchers since Ott, Grebogi, and Yorke proposed an efficient method,

called the OGY method [3]. Several theoretical methods have been developed to realize chaos synchronization such as feedback control method [4], active control method [5], backstepping method [6], adaptive control method [7–12], sliding mode control method [13], impulsive control method [14], and coupling control method [15].

Now, the research on circuits based on memristor is becoming a hot topic for research. Chaotic oscillator system containing memristor also attracts attention recently [16–20]. Various methods are used to suppress chaos. Zhong et al. have investigated the issues of fuzzy modeling and impulsive control of a memristor chaotic system and presented a memristor chaotic system as the Takagi-Sugeno model-based fuzzy system [21]. The chaotic system could be stabilized by a switched feedback controller which can be obtained by solving a set of LMIs [22]. Chaos of a memristor-based Chua's oscillator has been controlled by backstepping method [23]. A twin-T notch filter feedback controller has been designed and employed to control the chaotic behavior in the memristor-based chaotic circuit [24]. To the best of the author's knowledge, four-dimensional

chaotic system has rarely been studied; the synchronization for four-dimensional chaotic system has rarely been studied for the researchers.

Motivated by the existing works, we focus on not only the chaotic control of the memristor chaotic oscillator system but also a novel hybrid dislocated control synchronization scheme. Some important dynamical properties of the memristor chaotic oscillator system have been studied in the paper. Based on the Lyapunov stability theorem, a novel hybrid dislocated control method and a general hybrid projective dislocated synchronization scheme have been realized for memristor chaotic oscillator system.

Firstly, some important dynamical properties of the memristor chaotic oscillator system have been gained in Section 2; then, in Section 3, hybrid dislocated control method for stabilizing chaos to unstable equilibrium is realized. Section 4 realizes general hybrid projective dislocated synchronization for the memristor chaotic oscillator systems. Several illustrative examples are given in Section 5; finally, a brief concluding summary will be given in Section 6.

2. The Memristor Chaotic Oscillator and Dynamical Analysis

Recently, Chua [1] introduced a memristor chaotic system by replacing Chua's diode in the well-known Chua's chaotic system. A memristor chaotic system is extended from Chua's oscillator using a piece-wise linear memristor [22]; $q(w)$ is a piece-wise linear function of the form

$$q(w) = bw + 0.5(a - b)(|w + 1| - |w - 1|), \quad (1)$$

where $a, b > 0$. $\varphi(w)$ is provided in the following expression:

$$\varphi(w) = \frac{dq(w)}{dw} = \begin{cases} a, & |w| < 1, \\ b, & |w| > 1. \end{cases} \quad (2)$$

By applying Kirchhoff's circuit laws to the memristor Chua's circuit in Figure 1, the following state equation is gained:

$$\begin{aligned} \dot{v}_1 &= \frac{1}{c_1} [i - \varphi(w) v_1], \\ \dot{v}_2 &= \frac{1}{c_2} (Gv_2 - i), \\ \dot{i} &= v_2 - v_1 - iR, \\ \dot{\varphi} &= v_1, \end{aligned} \quad (3)$$

where v_1 and v_2 represent the voltages across the capacitors c_1 and c_2 , while i is the current through the inductor L . R, G are the circuit parameters. Set $x_1 = v_1$, $x_2 = v_2$, $x_3 = i$, $x_4 = \varphi$,

FIGURE 1: Chaotic system with memristor.

FIGURE 2: The Lyapunov exponents.

$a_1 = 1/c_1$, $a_2 = G/c_2$, $a_3 = 1/c_2$, and $a_4 = R$; then, the system can be further extended by the following expression:

$$\begin{aligned} \dot{x}_1 &= a_1 [x_3 - \varphi(x_4) x_1], \\ \dot{x}_2 &= a_2 x_2 - a_3 x_3, \\ \dot{x}_3 &= x_2 - x_1 - a_4 x_3, \\ \dot{x}_4 &= x_1. \end{aligned} \quad (4)$$

2.1. The Lyapunov Dimension, the Lyapunov Exponents, and Spectra. Assume $a_1 = 5.1$, $a_2 = 0.69$, $a_3 = 1$, $a_4 = 0.12$, $a = 0.2$, and $b = 17.8$; the Lyapunov exponents of this chaotic system are computed by the time-series method for the initial condition $(10^{-4}, 0, 0, 0)$. Corresponding Lyapunov exponents are $L_1 = 1.479485$, $L_2 = 0$, $L_3 = -0.580770$, and $L_4 = -17.903521$, as in Figure 2. It is obvious that there exists one positive exponent and the sum of the exponents is negative, and the Lyapunov dimension is given by

$$d_L = j - \frac{1}{L_{j+1}} \sum_{i=1}^j L_i = 3 - \frac{L_1 + L_2 + L_3}{L_4} = 3.05, \quad (5)$$

where j is the largest integer for

$$\sum_{i=1}^j L_i > 0, \quad \sum_{i=1}^{j+1} L_i < 0. \quad (6)$$

System (4) is chaotic with the 2-scroll attractor in Figures 3, 4, 5, and 6.

FIGURE 3: Chaotic attractor of system (3).

FIGURE 4: Chaotic attractor of system (3).

2.2. Dissipativity and Attractor. For system (4), the following expression is given by

$$\begin{aligned} \nabla(V) &= \frac{\partial \dot{x}_1}{\partial x_1} + \frac{\partial \dot{x}_2}{\partial x_2} + \frac{\partial \dot{x}_3}{\partial x_3} + \frac{\partial \dot{x}_4}{\partial x_4} \\ &= -a_1 \varphi(x_4) + a_2 - a_4. \end{aligned} \quad (7)$$

Therefore, $f = -a_1 \varphi(x_4) + a_2 - a_4 = -1.59$ or $-91.35 < 0$, so system (4) is dissipative. It converges the exponential convergence form

$$\frac{dV}{dt} = e^f. \quad (8)$$

This is to say, as $t \rightarrow \infty$, V_0 is reduced to $V_0 e^{ft}$. In other words, any volume element with the system line is contracted to 0 with the exponential convergence rate. Thus, all system

FIGURE 5: Chaotic attractor of system (3).

FIGURE 6: Chaotic attractor of system (3).

trajectories are limited to a specific subset of volume 0. The system has an attractor, and it may have very complex geometry.

3. Controlling Chaos with Hybrid Dislocated Control Method

Definition 1. For the controlled chaotic system

$$\dot{x} = f(x), \quad (9)$$

where $x = (x_1, x_2, \dots, x_n)^T \in R^n$ is a state vector and $f : R^n \rightarrow R^n$ is a continuous vector function, let

$$\begin{aligned} \dot{x}_i &= f(x_i) + k_1(x_1 - p_1) + \dots + k_{i-1}(x_{i-1} - p_{i-1}) \\ &\quad + k_{i+1}(x_{i+1} - p_{i+1}) + \dots + k_n(x_n - p_n), \end{aligned} \quad (10)$$

where k_i ($i = 1, 2, \dots, n$) are constants and $x_{E_i} = (p_1, p_2, \dots, p_n)$ stands for the equilibrium point of the original system $\dot{x} = f(x)$. If there at least exists a constant $k_i \neq 0$, such that the chaotic trajectories of system (4) can be successfully driven

to the equilibrium point x_E , then hybrid dislocated control original system is achieved.

Remark 2. For the three-dimensional chaotic system that is given as follows:

$$\begin{aligned}\dot{x}_1 &= f_1(x_1, x_2, x_3), \\ \dot{x}_2 &= f_2(x_1, x_2, x_3), \\ \dot{x}_3 &= f_3(x_1, x_2, x_3),\end{aligned}\quad (11)$$

where $x = (x_1, x_2, x_3)^T \in R^3$ is the state vector and $f: R^3 \rightarrow R^3$ is the continuous vector function, let

$$\begin{aligned}\dot{x}_1 &= f_1(x_1, x_2, x_3) + k_3(x_3 - p_3), \\ \dot{x}_2 &= f_2(x_1, x_2, x_3) + k_1(x_1 - p_1), \\ \dot{x}_3 &= f_3(x_1, x_2, x_3) + k_2(x_2 - p_2),\end{aligned}\quad (12)$$

or

$$\begin{aligned}\dot{x}_1 &= f_1(x_1, x_2, x_3) + k_2(x_2 - p_2), \\ \dot{x}_2 &= f_2(x_1, x_2, x_3) + k_3(x_3 - p_3), \\ \dot{x}_3 &= f_3(x_1, x_2, x_3) + k_1(x_1 - p_1),\end{aligned}\quad (13)$$

where k_i ($i = 1, 2, \dots, n$) are constants and (p_1, p_2, p_3) stands for the equilibrium point of the original system (11).

Remark 3. Generally, the controller of chaotic system is given to every state variable. Hybrid dislocated control method need not consider the place of the controller.

3.1. Stabilizing the Equilibrium Point with Hybrid Dislocated Control Method. System (4) is changed into the following controlled memristor chaotic oscillator system:

$$\begin{aligned}\dot{x}_1 &= a_1[x_3 - \varphi(x_4)x_1] + u_1, \\ \dot{x}_2 &= a_2x_2 - a_3x_3 + u_2, \\ \dot{x}_3 &= x_2 - x_1 - a_4x_3 + u_3, \\ \dot{x}_4 &= x_1 + u_4.\end{aligned}\quad (14)$$

Assume $\dot{x}_1 = \dot{x}_2 = \dot{x}_3 = \dot{x}_4 = 0$ for system (4); then, we obtain the equilibrium points $A = \{(x_1, x_2, x_3, x_4) \mid x_1 = x_2 = x_3 = 0, x_4 = c\}$. Let

$$\begin{aligned}u_1 &= k_1x_2 + k_2x_3 + k_3(x_4 - c), \\ u_2 &= k_4x_1 + k_5x_3 + k_6(x_4 - c), \\ u_3 &= k_7x_1 + k_8x_2 + k_9(x_4 - c), \\ u_4 &= k_{10}x_1 + k_{11}x_2 + k_{12}x_3,\end{aligned}\quad (15)$$

where k_i ($i = 1, 2, \dots, 12$) are constants. According to the transformation of following variables, we get

$$\begin{aligned}y_1 &= x_1, \\ y_2 &= x_2, \\ y_3 &= x_3, \\ y_4 &= x_4 - c.\end{aligned}\quad (16)$$

Hence

$$\begin{aligned}\dot{y}_1 &= a_1[y_3 - \varphi(y_4)y_1] + k_1y_2 + k_2y_3 + k_3y_4, \\ \dot{y}_2 &= a_2y_2 - a_3y_3 + k_4y_1 + k_5y_3 + k_6y_4, \\ \dot{y}_3 &= y_2 - y_1 - a_4y_3 + k_7y_1 + k_8y_2 + k_9y_4, \\ \dot{y}_4 &= y_1 + k_{10}y_1 + k_{11}y_2 + k_{12}y_3.\end{aligned}\quad (17)$$

Theorem 4. For the equilibrium point $(0, 0, 0, c)$ of system (17), if the following conditions hold true: $k_1 + k_4 = 0$, $k_2 + k_7 = 1 - a_1$, $k_3 + k_{10} = -1$, $k_5 + k_8 = a_3 - 1$, $k_6 + k_{11} = 0$, $k_9 + k_{12} = 0$, $a_1\varphi(y_4) > 0$, $a_2 < 0$, and $a_4 > 0$, then the controlled system (17) is asymptotically stable.

Proof. Choose a candidate Lyapunov function as follows:

$$V(y_1, y_2, y_3, y_4) = \frac{1}{2}(y_1^2 + y_2^2 + y_3^2 + y_4^2). \quad (18)$$

Then

$$\begin{aligned}\dot{V}(y_1, y_2, y_3, y_4) &= y_1\dot{y}_1 + y_2\dot{y}_2 + y_3\dot{y}_3 + y_4\dot{y}_4 \\ &= -a_1\varphi(y_4)y_1^2 + k_1y_1y_2 \\ &\quad + (k_2 + a_1)y_1y_3 + k_3y_1y_4 + k_4y_1y_2 \\ &\quad + a_2y_2^2 + (k_5 - a_3)y_2y_3 + k_6y_2y_4 \\ &\quad + (k_7 - 1)y_1y_3 + (k_8 + 1)y_2y_3 \\ &\quad - a_4y_3^2 + k_9y_3y_4 + (1 + k_{10})y_1y_4 \\ &\quad + k_{11}y_2y_4 + k_{12}y_3y_4 \\ &= -a_1\varphi(y_4)y_1^2 + (k_1 + k_4)y_1y_2 \\ &\quad + (k_2 + a_1 + k_7 - 1)y_1y_3 \\ &\quad + (k_3 + k_{10} + 1)y_1y_4 \\ &\quad + a_2y_2^2 + (k_5 - a_3 + k_8 + 1)y_2y_3 \\ &\quad + (k_6 + k_{11})y_2y_4 - a_4y_3^2 \\ &\quad + (k_9 + k_{12})y_3y_4 \\ &= -a_1\varphi(y_4)y_1^2 + a_2y_2^2 - a_4y_3^2;\end{aligned}\quad (19)$$

if $a_1\varphi(y_4) > 0$, $a_2 < 0$, and $a_4 > 0$, then $\dot{V} < 0$; system (17) is asymptotically stable. According to (16), the chaotic trajectory of system (17) is driven to the equilibrium point for the controller (15) in theory. $\square$

4. General Hybrid Projective Dislocated Synchronization of Chaotic Systems

The section will discuss general hybrid projective dislocated synchronization to achieve synchronization. Consider a drive system

$$\dot{x} = f(x); \quad (20)$$

the corresponding response system is

$$\dot{y} = g(y) + u(x, y), \quad (21)$$

where $x = (x_1, x_2, \dots, x_n)^T \in R^n$ and $y = (y_1, y_2, \dots, y_n)^T \in R^n$ are two state vectors, $f : R^n \rightarrow R^n$ and $g : R^m \rightarrow R^m$ are two continuous functions, and $u(x, y)$ is a controller to be designed later.

Definition 5. If there exists at least a constant $a_{ji} \neq 0$ ($j = 1, 2, \dots, m, i = 1, 2, \dots, n$), the condition

$$\lim_{t \rightarrow \infty} \left\| y_j - \sum_{i=1, i \neq j}^n a_{ji} x_i \right\| = 0 \quad (22)$$

can hold true; then the drive system (20) and the corresponding response system (21) are general hybrid projective dislocated synchronization.

In other words, let the error dynamics system of general hybrid projective dislocated synchronization be

$$\dot{e} = \left(\dot{y}_1 - \sum_{i=2}^n \alpha_{1i} \dot{x}_i, \dot{y}_2 - \sum_{i=1, i \neq 2}^n \alpha_{2i} \dot{x}_i, \dots, \dot{y}_m - \sum_{i=1, i \neq m}^n \alpha_{mi} \dot{x}_i \right)^T; \quad (23)$$

then there exist a suitable feedback controller $u(x, y) \in R^m$ and a constant α_{si} , so

$$\lim_{t \rightarrow \infty} \|e(t)\| = 0. \quad (24)$$

In the following section, we will give a principle to find a suitable feedback controller $u(x, y)$ such that the two chaotic systems are general hybrid projective dislocated synchronization. Lyapunov function is chosen as follows:

$$V = \frac{1}{2} e^T P e, \quad (25)$$

where P is a positive definite constant matrix. The time derivative of V along the trajectories of (25) is

$$\dot{V} = \frac{1}{2} (\dot{e}^T P e + e^T P \dot{e}). \quad (26)$$

If the feedback controller $u(x, y)$ is chosen for $\dot{V} < 0$, according to the Lyapunov stability theorem, the drive system (20) and the corresponding response system (21) are general hybrid projective dislocated synchronization.

4.1. General Hybrid Projective Dislocated Synchronization of Memristor Chaotic Oscillator Systems. General hybrid projective dislocated synchronization will be discussed for memristor chaotic oscillator systems.

4.1.1. Equality of the Dimensions for the Drive System and the Response System. In this section, we take into account the equality of the dimensions of the drive and response systems. The memristor chaotic oscillator system is given as the drive system

$$\begin{aligned} \dot{x}_1 &= a_1 [x_3 - \varphi(x_4) x_1], \\ \dot{x}_2 &= a_2 x_2 - a_3 x_3, \\ \dot{x}_3 &= x_2 - x_1 - a_4 x_3, \\ \dot{x}_4 &= x_1; \end{aligned} \quad (27)$$

the identical memristor chaotic oscillator system is written as the response system

$$\begin{aligned} \dot{y}_1 &= a_1 [y_3 - \varphi(y_4) y_1] + u_1, \\ \dot{y}_2 &= a_2 y_2 - a_3 y_3 + u_2, \\ \dot{y}_3 &= y_2 - y_1 - a_4 y_3 + u_3, \\ \dot{y}_4 &= y_1 + u_4. \end{aligned} \quad (28)$$

Let

$$\begin{aligned} e_1 &= y_1 + d_1 x_2 + d_2 x_3 + d_3 x_4, \\ e_2 &= y_2 + d_4 x_1 + d_5 x_3 + d_6 x_4, \\ e_3 &= y_3 + d_7 x_1 + d_8 x_2 + d_9 x_4, \end{aligned} \quad (29)$$

$$\begin{aligned} e_4 &= y_4 + d_{10} x_1 + d_{11} x_2 + d_{12} x_3, \\ u_1 &= -a_1 [y_3 - \varphi(y_4) y_1] - d_1 (a_2 x_2 - a_3 x_3) \\ &\quad - d_2 (x_2 - x_1 - a_4 x_3) - d_3 x_1 \\ &\quad - a_1 (y_1 + d_1 x_2 + d_2 x_3 + d_3 x_4), \\ u_2 &= a_3 y_3 - a_2 y_2 - a_1 d_4 [x_3 - \varphi(x_4) x_1] \\ &\quad - d_5 (x_2 - x_1 - a_4 x_3) - d_6 x_1 \\ &\quad - a_2 (y_2 + d_4 x_1 + d_5 x_3 + d_6 x_4), \\ u_3 &= -(y_2 - y_1 - a_4 y_3) \\ &\quad - d_7 a_1 [x_3 - \varphi(x_4) x_1] \\ &\quad - d_8 (a_2 x_2 - a_3 x_3) - d_9 x_1 \\ &\quad - a_3 (y_3 + d_7 x_1 + d_8 x_2 + d_9 x_4), \\ u_4 &= -y_1 - a_1 d_{10} [x_3 - \varphi(x_4) x_1] \\ &\quad - d_{11} (a_2 x_2 - a_3 x_3) \\ &\quad - d_{12} (x_2 - x_1 - a_4 x_3) \\ &\quad - a_4 (y_4 + d_{10} d_1 + d_{11} x_2 + d_{12} x_3), \end{aligned} \quad (30)$$

where d_i ($i = 1, 2, \dots, 12$) are constants.

Theorem 6. If the conditions $a_1 > 0$, $a_2 > 0$, $a_3 > 0$, and $a_4 > 0$ hold true, then systems (27) and (28) can realize general hybrid projective dislocated synchronization under the adaptive control law (30).

Proof. It is easy to see from (27) and (28) that the error dynamics system can be obtained as follows:

$$\begin{aligned}\dot{e}_1 &= a_1 [y_3 - \varphi(y_4) y_1] + u_1 + d_1 (a_2 x_2 - a_3 x_3) \\ &\quad + d_2 (x_2 - x_1 - a_4 x_3) + d_3 x_1, \\ \dot{e}_2 &= a_2 y_2 - a_3 y_3 + u_2 + d_4 (x_3 - \varphi(x_4) x_1) \\ &\quad + d_5 (x_2 - x_1 - a_4 x_3) + d_6 x_1, \\ \dot{e}_3 &= y_2 - y_1 - a_4 y_3 + u_3 + d_7 a_1 [x_3 - \varphi(x_4) x_1] \\ &\quad + d_8 (a_2 x_2 - a_3 x_3) + d_9 x_1, \\ \dot{e}_4 &= y_1 + u_4 + d_{10} a_1 [x_3 - \varphi(x_4) x_1] \\ &\quad + d_{11} (a_2 x_2 - a_3 x_3) + d_{12} (x_2 - x_1 - a_4 x_3).\end{aligned}\quad (31)$$

Choose a candidate Lyapunov function

$$V = \frac{1}{2} (e_1^2 + e_2^2 + e_3^2 + e_4^2). \quad (32)$$

Then

$$\begin{aligned}\dot{V}(e_1, e_2, e_3, e_4) &= e_1 \dot{e}_1 + e_2 \dot{e}_2 + e_3 \dot{e}_3 + e_4 \dot{e}_4 \\ &= -a_1 e_1^2 - a_2 e_2^2 - a_3 e_3^2 - a_4 e_4^2 \\ &= -e^T P e,\end{aligned}\quad (33)$$

where $e = [e_1, e_2, e_3, e_4]^T$,

$$P = \begin{bmatrix} a_1 & 0 & 0 & 0 \\ 0 & a_2 & 0 & 0 \\ 0 & 0 & a_3 & 0 \\ 0 & 0 & 0 & a_4 \end{bmatrix}. \quad (34)$$

According to Lyapunov theorem, $a_1 > 0$, $a_2 > 0$, $a_3 > 0$, and $a_4 > 0$; P is a positive definite constant matrix; this leads to

$$\lim_{t \rightarrow \infty} \|e(t)\| = 0. \quad (35)$$

Therefore, the corresponding response system (28) can realize general hybrid projective dislocated synchronization with the drive system (27) for the controller (30). $\square$

4.1.2. Inequality of the Dimensions for the Drive System and the Response System. Here, there are different dimensions for the drive system and the corresponding response system. The general hybrid projective dislocated synchronization between the memristor chaotic oscillator system (27) and the chaotic system [25] will be discussed. The chaotic system is given as follows:

$$\begin{aligned}\dot{x}_1 &= b_1 (x_2 - x_1), \\ \dot{x}_2 &= b_2 x_1 - x_1 x_3, \\ \dot{x}_3 &= x_1 x_2 + b_3 x_3.\end{aligned}\quad (36)$$

Case (a) ($n < m$). The corresponding response system is written as follows:

$$\begin{aligned}\dot{y}_1 &= b_1 (y_2 - y_1) + u_1, \\ \dot{y}_2 &= b_2 y_1 - y_1 y_3 + u_2, \\ \dot{y}_3 &= y_1 y_2 + b_3 y_3 + u_3.\end{aligned}\quad (37)$$

Assume

$$\begin{aligned}e_1 &= y_1 + h_1 x_2 + h_2 x_3 + h_3 x_4, \\ e_2 &= y_2 + h_4 x_1 + h_5 x_3 + h_6 x_4, \\ e_3 &= y_3 + h_7 x_1 + h_8 x_2 + h_9 x_4,\end{aligned}\quad (38)$$

$$\begin{aligned}u_1 &= -b_1 (y_2 - y_1) - h_1 (a_2 x_2 - a_3 x_3) \\ &\quad - h_2 (x_2 - x_1 - a_4 x_3) - h_3 x_1 \\ &\quad - b_1 (y_1 + h_1 x_2 + h_2 x_3 + h_3 x_4),\end{aligned}$$

$$\begin{aligned}u_2 &= y_1 y_3 - b_2 y_1 - h_4 a_1 [x_3 - \varphi(x_4) x_1] \\ &\quad - h_5 (x_2 - x_1 - a_4 x_3) - h_6 x_1 \\ &\quad - b_2 (y_2 + h_4 x_1 + h_5 x_3 + h_6 x_4),\end{aligned}\quad (39)$$

$$\begin{aligned}u_3 &= -y_1 y_2 - b_3 y_3 - h_7 a_1 [x_3 - \varphi(x_4) x_1] \\ &\quad - h_8 (a_2 x_2 - a_3 x_3) - h_9 x_1 \\ &\quad - b_3 (y_3 + h_7 x_1 + h_8 x_2 + h_9 x_4),\end{aligned}$$

where h_i ($i = 1, 2, \dots, 9$) are constants.

Theorem 7. If the conditions $b_1 > 0$, $b_2 > 0$, and $b_3 > 0$ hold true, then systems (27) and (37) can realize general hybrid projective dislocated synchronization under the adaptive control law (39).

Proof. It is easy to see from (27) and (37) that the error dynamics system can be obtained as follows:

$$\begin{aligned}\dot{e}_1 &= b_1 (y_2 - y_1) + u_1 + h_1 (a_2 x_2 - a_3 x_3) \\ &\quad + h_2 (x_2 - x_1 - a_4 x_3) + h_3 x_1, \\ \dot{e}_2 &= b_2 y_1 - y_1 y_3 + u_2 + h_4 a_1 [x_3 - \varphi(x_4) x_1] \\ &\quad + h_5 (x_2 - x_1 - a_4 x_3) + h_6 x_1, \\ \dot{e}_3 &= y_1 y_2 + b_3 y_3 + u_3 + h_7 a_1 [x_3 - \varphi(x_4) x_1] \\ &\quad + h_8 (a_2 x_2 - a_3 x_3) + h_9 x_1.\end{aligned}\quad (40)$$

Choose a candidate Lyapunov function as follows:

$$V(e_1, e_2, e_3) = \frac{1}{2} (e_1^2 + e_2^2 + e_3^2). \quad (41)$$

Then

$$\begin{aligned}\dot{V}(e_1, e_2, e_3) &= e_1 \dot{e}_1 + e_2 \dot{e}_2 + e_3 \dot{e}_3 \\ &= -b_1 e_1^2 - b_2 e_2^2 - b_3 e_3^2 \\ &= -e^T P e,\end{aligned}\quad (42)$$

where $e = [e_1, e_2, e_3]^T$,

$$P = \begin{bmatrix} b_1 & 0 & 0 \\ 0 & b_2 & 0 \\ 0 & 0 & b_3 \end{bmatrix}. \quad (43)$$

According to Lyapunov theorem, $b_1 > 0$, $b_2 > 0$, and $b_3 > 0$; P is a positive definite constant matrix; this leads to

$$\lim_{t \rightarrow \infty} \|e(t)\| = 0. \quad (44)$$

Hence the drive system (27) and the corresponding response system (37) are general hybrid projective dislocated synchronization for the controller (39). $\square$

Case (b) ($n > m$). System (36) is the drive system. The memristor chaotic oscillator system is the corresponding response system:

$$\begin{aligned}\dot{y}_1 &= a_1 [y_3 - \varphi(w) y_1] + u_1, \\ \dot{y}_2 &= a_2 y_2 - a_3 y_3 + u_2, \\ \dot{y}_3 &= y_2 - y_1 - a_4 y_3 + u_3, \\ \dot{y}_4 &= y_1 + u_4.\end{aligned}\quad (45)$$

Assume

$$\begin{aligned}e_1 &= y_1 + k_1 x_2 + k_2 x_3, \\ e_2 &= y_2 + k_3 x_1 + k_4 x_3, \\ e_3 &= y_3 + k_5 x_1 + k_6 x_2, \\ e_4 &= y_4 + k_7 x_1 + k_8 x_2 + k_9 x_3,\end{aligned}\quad (46)$$

$$\begin{aligned}u_1 &= -a_1 [y_3 - \varphi(w) y_1] - k_1 (b_2 x_1 - x_1 x_3) \\ &\quad - k_2 (x_1 x_2 + b_3 x_3) - a_1 (y_1 + k_1 x_2 + k_2 x_3), \\ u_2 &= a_3 y_3 - a_2 y_2 - b_1 k_3 (x_2 - x_1) \\ &\quad - k_4 (x_1 x_2 + b_3 x_3) - a_2 (y_2 + k_3 x_1 + k_4 x_3), \\ u_3 &= -(y_2 - y_1 - a_4 y_3) - b_1 k_5 (x_2 - x_1) \\ &\quad - k_6 (b_2 x_1 - x_1 x_3) - a_3 (y_3 + k_5 x_1 + k_6 x_2), \\ u_4 &= -y_1 - b_1 k_7 (x_2 - x_1) \\ &\quad - k_8 (b_2 x_1 - x_1 x_3) - k_9 (x_1 x_2 + b_3 x_3) \\ &\quad - a_4 (y_4 + k_7 x_1 + k_8 x_2 + k_9 x_3),\end{aligned}\quad (47)$$

where k_i ($i = 1, 2, \dots, 9$) are constants.

Theorem 8. If the conditions $a_1 > 0$, $a_2 > 0$, $a_3 > 0$, and $a_4 > 0$ hold true, then systems (27) and (45) can realize general hybrid projective dislocated synchronization under the adaptive control law (47).

Proof. It is easy to see from (27) and (45) that the error dynamics system can be obtained as follows:

$$\begin{aligned}\dot{e}_1 &= a_1 [y_3 - \varphi(w) y_1] + u_1 \\ &\quad + k_1 (b_2 x_1 - x_1 x_3) + k_2 (x_1 x_2 + b_3 x_3), \\ \dot{e}_2 &= a_2 y_2 - a_3 y_3 + u_2 \\ &\quad + b_1 k_3 (x_2 - x_1) + k_4 (x_1 x_2 + b_3 x_3), \\ \dot{e}_3 &= y_2 - y_1 - a_4 y_3 + u_3 \\ &\quad + b_1 k_5 (x_2 - x_1) + k_6 (b_2 x_1 - x_1 x_3), \\ \dot{e}_4 &= y_1 + u_4 + b_1 k_7 (x_2 - x_1) \\ &\quad + k_8 (b_2 x_1 - x_1 x_3) + k_9 (x_1 x_2 + b_3 x_3).\end{aligned}\quad (48)$$

Choose a candidate Lyapunov function as follows:

$$V(e_1, e_2, e_3, e_4) = \frac{1}{2} (e_1^2 + e_2^2 + e_3^2 + e_4^2). \quad (49)$$

Then

$$\begin{aligned}\dot{V}(e_1, e_2, e_3, e_4) &= e_1 \dot{e}_1 + e_2 \dot{e}_2 + e_3 \dot{e}_3 + e_4 \dot{e}_4 \\ &= -a_1 e_1^2 - a_2 e_2^2 - a_3 e_3^2 - a_4 e_4^2 \\ &= -e^T P e,\end{aligned}\quad (50)$$

where $e = [e_1, e_2, e_3, e_4]^T$,

$$P = \begin{bmatrix} a_1 & 0 & 0 & 0 \\ 0 & a_2 & 0 & 0 \\ 0 & 0 & a_3 & 0 \\ 0 & 0 & 0 & a_4 \end{bmatrix}. \quad (51)$$

According to the Lyapunov theorem, $a_1 > 0$, $a_2 > 0$, $a_3 > 0$, and $a_4 > 0$; P is a positive definite constant matrix; this leads to

$$\lim_{t \rightarrow \infty} \|e(t)\| = 0. \quad (52)$$

Hence the drive system (27) and the corresponding response system (45) can realize general hybrid projective dislocated synchronization for the controller (47) (see Figure 7). $\square$

5. Illustrative Examples

Example 1. Consider the control chaos with hybrid dislocated control method. The parameters of system (4) are chosen as $a_1 = 5.1$, $a_2 = -0.5$, $a_3 = 1$, $a_4 = 0.12$, $k_1 = 1$, $k_2 = -1$, $k_3 = -1$, $k_4 = -1$, $k_5 = 1$, $k_6 = 1$, $k_7 = -3.1$, $k_8 = -1$, $k_9 = 1$, $k_{10} = 0$, $k_{11} = -1$, and $k_{12} = -1$, and the

FIGURE 7: Time-domain waveforms.

initial condition is $(10^{-4}, 0, 0, 0)$. According to Theorem 4, the system is successfully controlled to the equilibrium point.

Simulation results of y_1, y_2, y_3 , and y_4 are depicted in Figures 8 and 9. The system is controlled to the equilibrium point $(0, 0, 0, 1)$ in Figure 8. The system is controlled to the equilibrium point $(0, 0, 0, -1)$ in Figure 9. It is easy to see that $y_1 \rightarrow 0, y_2 \rightarrow 0, y_3 \rightarrow 0$, and $y_4 \rightarrow 0$; system (4) is asymptotically stable. System (4) is successfully controlled to the equilibrium points.

Example 2. Consider the drive system (27) and the corresponding response system (28); the initial conditions are $(10^{-8}, 2 * 10^{-8}, 3 * 10^{-2}, 4 * 10^{-8})$ and $(5 * 10^{-8}, 6 * 10^{-8}, 7 * 10^{-2}, 8 * 10^{-8})$; parameters are $d_1 = 1, d_2 = -2, d_3 = -1, d_4 = 1, d_5 = -2, d_6 = -1, d_7 = 1, d_8 = -2, d_9 = -1, d_{10} = 1, d_{11} = -2, d_{12} = -1, a_1 = 5.1 * 10^{-8}, a_2 = 1, a_3 = 0.69, a_4 = 0.12$. $a_1 > 0, a_2 > 0, a_3 > 0$, and $a_4 > 0$, and P is a positive definite constant matrix. According to Theorem 6, the drive system (27) and the corresponding response system (28) can realize general hybrid projective dislocated synchronization for the controller (30).

The iterations have been done 100 times. Simulation results of e_1, e_2, e_3 , and e_4 are depicted in Figure 10. It is easy to see that $e_1 \rightarrow 0, e_2 \rightarrow 0, e_3 \rightarrow 0$, and $e_4 \rightarrow 0$. Thus, the drive system (27) and the corresponding response system (28) can realize general hybrid projective dislocated synchronization for the controller (30).

Example 3. Consider the drive system (27) and the corresponding response system (37); the initial conditions are $(10^{-8}, 2 * 10^{-8}, 3 * 10^{-2})$ and $(5 * 10^{-8}, 6 * 10^{-8}, 7 * 10^{-2}, 8 * 10^{-8})$; parameters are $h_1 = 1, h_2 = -2, h_3 = -1, h_4 = 1, h_5 = -2, h_6 = -1, h_7 = 1, h_8 = -2, h_9 = -1, b_1 = 5.1 * 10^{-8}, b_2 = 2, b_3 = 0.69, a_1 = 5.1 * 10^{-8}, a_2 = 0.69, a_3 = 1,$

FIGURE 8: Control to the equilibrium point $(0, 0, 0, 1)$. FIGURE 9: Control to the equilibrium point $(0, 0, 0, -1)$.

$a_4 = 0.12, b_1 > 0, b_2 > 0$, and $b_3 > 0$, and P is a positive definite constant matrix. According to Theorem 7, the drive system (27) and the corresponding response system (37) can realize general hybrid projective dislocated synchronization for the controller (39).

The iterations have been done 200 times. Simulation results of e_1, e_2 , and e_3 are depicted in Figure 11. It is easy to see that $e_1 \rightarrow 0, e_2 \rightarrow 0$, and $e_3 \rightarrow 0$. Thus, the drive system

FIGURE 10: Synchronization errors e_1, e_2, e_3, e_4 of $m = n$. FIGURE 11: Synchronization errors e_1, e_2, e_3 of $n < m$.

(27) and the corresponding response system (37) can realize general hybrid projective dislocated synchronization for the controller (39).

Example 4. Consider the drive system (27) and the corresponding response system (45); the initial conditions are $(10^{-8}, 2 * 10^{-8}, 3 * 10^{-2})$ and $(5 * 10^{-8}, 6 * 10^{-8}, 7 * 10^{-2}, 8 * 10^{-8})$; parameters are $k_1 = 1, k_2 = -1, k_3 = 1, k_4 = -1, k_5 = 1, k_6 = -1, k_7 = 1, k_8 = -1, k_9 = 1, a_1 = 5.1 * 10^{-8}, a_2 = 0.69, a_3 = 1, a_4 = 0.12, b_1 = 5.1 * 10^{-8}, b_2 = 2, b_3 = 0.69. a_1 > 0,$

FIGURE 12: Synchronization errors e_1, e_2, e_3, e_4 of $n > m$.

$a_2 > 0, a_3 > 0,$ and $a_4 > 0,$ and P is a positive definite constant matrix. According to Theorem 8, the drive system (27) and the corresponding response system (45) can realize general hybrid projective dislocated synchronization for the controller (47).

The iterations have been done 100 times. Simulation results of $e_1, e_2, e_3,$ and e_4 are depicted in Figure 12. It is easy to see that $e_1 \rightarrow 0, e_2 \rightarrow 0, e_3 \rightarrow 0,$ and $e_4 \rightarrow 0.$ Thus, the drive system (27) and the corresponding response system (45) can realize general hybrid projective dislocated synchronization for the controller (47).

6. Conclusion

Some important dynamical properties have been gained for the memristor chaotic oscillator system. Based on these properties, we realize hybrid projective dislocated control method for stabilizing chaos to unstable equilibrium. There have been more significant advantages in controlling chaos in the memristor chaotic oscillator system. We need not consider the position of controller in our method. Particularly, hybrid dislocated control method can control chaos to all the unstable equilibrium points.

In addition, based on the Lyapunov stability theorem, general hybrid projective dislocated synchronization has been investigated for the memristor chaotic oscillator system. The drive and response systems discussed in this paper can be the same as the memristor chaotic oscillator systems. Finally, the memristor chaotic oscillator system and the chaotic system have realized general hybrid projective dislocated synchronization for the different dimensions. Numerical illustrative simulation examples are given to show the effectiveness of these methods and the accuracy of the statements

proved. With the rapid development of science and technology and combination of multidisciplinary science, hybrid dislocated control and general hybrid projective dislocated synchronization for memristor chaotic oscillator system have a very bright future in various practical application fields.

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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