Research Article

Analysis and Testing of Chain Characteristics and Rheological Properties for Magnetorheological Fluid

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1. Introduction

Magnetorheological (MR) fluids are suspensions of micron-sized, magnetizable particles in a carrier fluid such as synthetic oil and silicone oil, which are regarded as the intelligent materials that respond to an applied magnetic field with a change in their rheological properties. In the absence of an applied magnetic field, MR fluids exhibit Newtonian fluid-like behavior. Upon application of a magnetic field, the polarization between two induced dipoles causes the suspended particles in the MR fluids to form a chain-like microstructure aligned with the direction of applied magnetic field. The magnetic chain structure changes the rheological properties of the suspension. Altering the strength of the applied magnetic field precisely and proportionally controls the shear yield strength of the fluids [1, 2]. Based on the mechanical characteristics, the fluids can be used in the controllable energy-dissipating applications such as dampers [3, 4], valves [5, 6], and clutches and brakes [7, 8].

Experiments showed that many other factors affect the macroscopic properties of an MR fluid. It mainly includes the applied magnetic field strength, the size and gradation, and the property and volume fraction of the particles; the property of the carrier fluid and the additives. Noma et al. [9] found that Fe nanoparticles synthesized by the arc plasma method exhibited a high saturation magnetization and may be useful for MR fluids. Ekwebelam and See [10] explored the yielding behavior and enhanced stress response exhibited by bidisperse MR fluid over monodisperse systems. He found that the stress enhancement in bidisperse suspensions is likely to be due to the population and orientation of interacting large particles in the bidisperse suspensions. Jang et al. [11] studied the behavioral model for magnetorheological fluid under a magnetic field using Lekner summation method. Pacull et al. [12] studied the effect of polar interactions on the magnetorheology of silica-coated magnetite suspensions in oil media reported. He suggested that the nonnegligible interfacial interactions are responsible for both the absence of MR effect in hydrophobic samples and the low yield stress in hydrophilic suspensions. To resolve the sedimentation of carbonyl iron (CI) based MR fluid, Fang et al. [13] introduced fibrous single-walled carbon nanotube (SWNT) into carbonyl iron (CI) suspension as additives.

2. Chain Characteristics of MR Fluid

2.1. Chain Process. When a magnetic field is applied, the magnetic particles in MR fluid are moving orderly that causes the suspended particles to attract each other under the action...
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Figure 1: The chain process of MR fluid.

Figure 2: The experimental device of measurement of MR fluids by digital microholography.

Figure 2: The chain process of MR fluid.

The chain process along the direction of magnetic field, that is, the responding speed of MR fluids for magnetic field, is easily calculated.

2.2. Shear Yield Stress. In order to analyze the relationship between the shear yield stress and the magnetic field, the size, the volume percentage of MR fluid. The assumptions for chain model of dipole are as follows.

(1) The ordered arrangement of particles after magnetic polarization and the chain structure is steady. All of the particles occupy a fixed position in the stable chain.

(2) The single chain formed by particles is along with the direction of magnetic field. The chain is parallel to magnetic field direction, and its length is equal to the distance between two plates. All of the chains are the same in geometry, so the analysis results of arbitrary chain can be representative of the others.

(3) The acting force between adjacent particles in the chains is equal, which presents the tensile strength of chains.

(4) The adjacent particles are magnetized and turn into dipoles. The direction of the centerline of particles is parallel to the magnetic field.

(5) The interaction force in particles decides the strength of chains. When applied force is greater than the interaction force between particles, the chain will be pulled off. When the shear stress is perpendicular to the direction of magnetic field, the chain will be elongated and snapped.

(6) The particles are supposed to be spherosome and uniform.

The analysis mode of shear yield stress in MR fluid is shown in Figure 5, where \( h \) represents the distance between two parallel plates and \( F_a \) is the external force [14]. The bottom plate is fixed, and external force is applied to upper plate. When the shear stress is perpendicular to magnetic field direction, the chain will deform and break. The \( \tau_y(H) \) represents the shear yield stress under unit area. The relationship between \( \tau_y(H) \) and \( F_a \) is indicated by \( \tau_y(H) = F_a \sin \theta \), where \( \theta \) represents the angle between the centerline of chain and magnetic field direction, as shown in Figure 5.

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With the applied magnetic field, the single magnetic particle is magnetized and forms dipoles in the MR fluid. The $J$ represents the dipole moment which can be expressed as follows [15]:

$$J = \mu_0 V_1 M,$$

(1)

where $\mu_0$ is the permeability of vacuum, $V_1$ is the average volume of magnetic particles, $V_1 = 4\pi r^3 / 3$, and $M$ is magnetization intensity:

$$M = \chi H,$$

(2)

where $\chi$ is the magnetic susceptibility and $H$ is the magnetic field strength.

The magnetic pole strength of the dipole can be expressed as follows:

$$m = \frac{J}{2r},$$

(3)

The distance of dipoles which is formed by any two magnetic particles in the same chain is

$$d = \frac{n (2r + \delta)}{\cos \theta},$$

(4)

where $\delta$ is the average value of the gap between two adjacent particles in the chain.

The average value of acting force in particles in the same chain can be expressed as follows:

$$F = \frac{1}{4\pi \mu_0} \frac{m^2}{d^2}.$$  

(5)

The shear yield stress of MR fluid under magnetic field is

$$\tau_y (H) = \frac{NF \sin \theta}{A},$$

(6)

where $A$ represents the area of the flat plate.

The number of chains in the unit area can be expressed as follows:

$$N = \left( \frac{\phi Ah / V_1}{(h/R)} \right),$$

(7)

where $\phi$ is the volume fraction of magnetic particles in MR fluid and $R = 2r + \delta$.

Combining (1), (3), (4), and (6), the shear yield stress of MR fluid under magnetic field is expressed as follows:

$$\tau_y (H) = \sum_{n=1}^{k} \frac{\mu_0}{12n^2} \frac{r \phi (\mu_r - 1)^2 H^2}{(2r + \delta)^3 \sin \theta \cos^2 \theta},$$

(8)
Figure 6: The yield stress versus applied magnetic field strength.

![Graph showing yield stress vs. applied magnetic field strength.](image)

Figure 7: The relative magnetic permeability versus applied magnetic field strength.

![Graph showing relative magnetic permeability vs. applied magnetic field strength.](image)

where $\mu_r$ represents the relative magnetic permeability of MR fluid, $\mu_r = 1 + \chi$, $k$ represents the average number of particles in each chain, and $k = A h/V_1 N$.

The theoretical value and experimental value of yield stress versus applied magnetic field strength are shown in Figure 6. The magnetic particle is uniform spherosome in the MR fluid. Assume that $\varv = 30^\circ$, $\sigma = 0$, $\mu_0 = 4\pi \times 10^{-7}$ Tm/A, and $\phi = 37\%$. The relationship between the relative magnetic permeability and the applied magnetic field strength can be drawn, as shown in Figure 7. As shown in Figure 6, the theoretical value is satisfied with the experimental value, the yield stress of MR fluid is increased with the applied magnetic field and its value can be controlled by applied magnetic field.

3. Rheological Properties of MR Fluid

3.1. Test Equipment. The performance experimental device for rheological properties of MR fluid between two discs is shown in Figure 8. Based on this test system, the transmission torques of MR fluids between two discs under zero magnetic field and different applied magnetic fields are analyzed. The shearing rate of MR fluids between two discs can be adjusted by motor in the test system. The applied magnetic field strength can be controlled by electric current in coil. All parameters in system are measured in real time by gaussmeter, speed, and torque sensors.

3.2. Test Principle. For the properties of experimental system of MR fluid between two parallel disks, shown in Figure 8, the following assumptions are given: the fluid is incompressible. There is no flow in radial direction and axial direction, but only tangential flow. The flow velocity of MR fluid is a function of radius. The pressure in the thickness direction of MR fluid is constant. The strength of magnetic field in the gap of the activation region is well distributed. In cylindrical coordinates $(r, \theta, z)$, the distribution of the flow velocity is

$$V_r = 0, \quad V_\theta = r \omega(z), \quad V_z = 0,$$

where $V_r$, $V_\theta$, and $V_z$ are the flow velocity of the fluid in the $r$-direction, the $\theta$-direction, and $z$-direction, respectively; $\omega(z)$ is the rotation angular velocity of the fluid in the $\theta$-direction. The angular velocity $\omega(z)$ is the function of $z$-coordinate.

The fluid shear strain rate may be approximated as follows:

$$\dot{\gamma} = \frac{\omega_0 r}{h},$$

where $\omega_0$ is speed of rotating disk. The torque transmitted by the MR fluid between two parallel disks is calculated by integrating the shear stress of the MR fluid as follows:

$$T = 2\pi \int_{R_1}^{R_2} \tau r^2 dr,$$

where $R_1$ and $R_2$ are the effective inner and outer radius of the rotor-disc in the MR fluid exposed to the magnetic field, respectively. Based on the mean value theorem of integral, the torque $T$ in (11) can be expressed as follows:

$$T = \frac{2\pi}{3} \tau^* \left( R_2^3 - R_1^3 \right),$$

where $\tau^*$ is the shear stress of the sample. When $(R_2 - R_1) \ll R_0$, the $\tau^*$ is equal to the stress located at $R_0 = (R_2 - R_1)/2$, approximately. Using (10) and (12), the relationship between $\tau$ and $\dot{\gamma}$ can be obtained by the measuring torque $T$ and speed $\omega_0$.

3.3. Test Results. In this experiment, we choose MR fluid samples MRM1, MRM2, and MRM3 to check the theory, as shown in Table 1. Then we make a comparison with the results.

When the magnetic displacement is small, shown in Figure 9, magnetic particle is far from reaching a magnetic saturation and the shear stress quickly increases. With the increase of the magnetic induction intensity, curves gradually become slow. This is mainly because of different magnetisability of the solid ferromagnetism particles. We
must increase the applied magnetic field strength in order to obtain a greater shear stress. If the magnetic induction intensity is large enough, the particles gradually reach magnetic saturation, particle interaction reaches the extreme value, and the shear stress at this time will not increase with the magnetic induction intensity and tends to a stable value.

The particles volume percentage refers to the percentage of the volume occupied by the dispersed phase of solid particles in the MR fluid. As Figure 10 shows, the shear stress also increases when the particle volume fraction increases. In the case of not very high magnetic field strength, both are rendering the approximate linear relationship. This can be explained by MR fluid microscopic mechanism. The solid particulate magnetic becomes dipole under the action of the magnetic field. Dipole of interaction form magnetic chain between the two plates. When the volume percentage is low, the number of solid particle is limited. In a magnetic field, a few of magnetic chains are formed and the shear stress is small. When the volume percentage is high, the number of magnetic chain increases and even forms column or mesh structure and the shear stress ensues to increase.
The apparent viscosity of MR fluid is the measure shear stress \( \tau \) under certain conditions divided by the shear strain rate \( \dot{\gamma} \). Obviously, for a Newtonian fluid, the apparent viscosity is the dynamic viscosity, and the value of viscosity is a constant, independent of the shear strain rate. But for MR fluid, it is not so. As Figure II shows, the apparent viscosity of MR fluid changes with shear strain rate under different magnetic induction intensity. The apparent viscosity decreases with increasing shear strain rate and in the beginning it decreased rapidly and then leveled off.

4. Conclusion

In order to predict the mechanical property of MR fluid under magnetic field and shear strain, the microstructures of chain at different magnetic fields strength were measured. The chain model of dipole interaction for MR fluid was established. The prediction model of yield stress for MR fluid is obtained. The influence of yield stress by magnetization intensity of magnetic particle and magnetic field strength were analyzed, respectively. In this experiment, we obtain the relationship between the shear stress and magnetic induction and particle volume fraction.

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References


