OPEN-CIRCUIT END EFFECT OF MICROSTRIP LINE CONFIGURATION IN PLASMA MEDIUM

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The extension in length for open microstrip configuration in plasma media is determined using spectral domain technique under quasi static approach [1, 2]. The results were verified by modifying Hammerstad equation for plasma media. Good agreement is found between the two results.

INTRODUCTION

The ideal field patterns of a open-circuited microstrip line are distorted with fringing electric fields. The fringing fields and the increase in electrostatic energy as a result of the extra stored energy is modeled by a capacitive termination C_F . The fringing capacitance at the termination of the line is equivalent to extending line by $\Delta\ell$ as given by the expression

$$\Delta\ell = \frac{1}{\beta} \tan^{-1} (Z_0 \omega C_F) \quad (1)$$

where β = propagation constant on the line
 Z_0 = characteristic impedance of the line
 ω = angular frequency

FORMULATION

The microstrip in plasma medium is shown in Fig. 1 where ϵ_p is the dielectric constant of plasma medium defined as

$$\epsilon_p = A^2 = 1 - \left(\frac{\omega_p}{\omega} \right)^2 \quad (2)$$

where A is the plasma parameter

If $\phi(x, y)$ = static potential distribution in microstrip structure

MICROSTRIP IN PLASMA MEDIUM

FIGURE 1

then $\tilde{\phi}(\beta, y) = \text{Fourier transform of } \phi(x, y)$

$$= \int_{-\infty}^{\infty} \phi(x, y) e^{j\beta x} dx$$

$$\text{Assuming in media (1) } \phi = Ae^{\beta y} + Be^{-\beta y} \quad (3)$$

$$\& \text{ in media (2) } \phi = Ce^{-\beta y} + De^{\beta y} \quad (4)$$

In Fourier transform domain, the boundary conditions are

$$\text{at } y = 0 \quad \tilde{\phi}(\beta, 0) = 0 \quad (5)$$

$$y = \infty \quad \tilde{\phi}(\beta, \infty) = 0 \quad (6)$$

At interface

$$\tilde{\phi}(\beta, h + 0) = \tilde{\phi}(\beta, h - 0) \quad (7)$$

$$\text{and } \epsilon_p \frac{d\tilde{\phi}}{dy}(\beta, h + 0) = \epsilon_1 \frac{d\tilde{\phi}}{dy}(\beta, h - 0) - \tilde{f}(\beta) \quad (8)$$

Taking $f(x)$ as the charge distribution on the strip conductor, total charge on strip conductor

$$Q = \int_{-\infty}^{\infty} f(x) dx$$

Hence

$$\tilde{f}(\beta) = \int_{-\infty}^{\infty} f(x) e^{j\beta x} dx \quad (9)$$

Solving the above, we have

$$\Phi(x, h) = C e^{-\beta h} = \frac{\tilde{f}(\beta)}{\beta(\epsilon_1 \coth \beta h + \epsilon p)} \quad (10)$$

Hence the fourier transform of potential distribution is given as:

$$\tilde{\Phi}(\beta, h) = \frac{\tilde{f}(\beta)}{\beta(\epsilon_1 \coth \beta h + \epsilon p)} \quad (11)$$

Line capacitance C is obtained using symmetry as

$$\frac{1}{C} = \frac{1}{\pi \epsilon Q^2} \int_0^{\infty} \frac{\{\tilde{f}(\beta)\}^2}{\{\epsilon p + \epsilon_1 \coth \beta h\} \beta h} d(\beta h) \quad (12)$$

Taking approximately trial function for $f(x) = |x|$ which gives capacitance as maximum

$$f(x) = \begin{cases} |x| - \omega/2 \leq x \leq \omega/2 \\ 0 \text{ elsewhere} \end{cases}$$

$$\frac{\tilde{f}(\beta)}{Q} = 2 \left[\frac{2 \sin\left(\frac{\beta \omega}{2}\right)}{\left(\frac{\beta \omega}{2}\right)} \right] - \left[\frac{\sin\left(\frac{\beta \omega}{4}\right)}{\frac{\beta \omega}{4}} \right]^2 \quad (13)$$

If $\beta h = x$, then $d\beta h = dx$.

Hence

$$\frac{1}{C} = \frac{\frac{1}{\pi \epsilon_0} \int \left[\frac{f\left(\frac{x}{h}\right)}{Q} \right]^2}{[\epsilon p + \epsilon r_1 \coth x] x} dx \quad (14)$$

or

FIGURE 2

$$\frac{C}{\epsilon_0} = \frac{\pi}{\int_2 \left[\frac{\sin\left(\frac{x \omega}{2h}\right)}{\frac{x \omega}{2h}} \right] - \left[\frac{\sin\frac{x \omega}{4h}}{\frac{x \omega}{4h}} \right]^2 dx} \quad (15)$$

$(\epsilon_p + \epsilon_{r1} \coth x)x$

The effective permittivity of microstrip is given by

FIGURE 3

$$\epsilon_{eff} = \frac{C}{C_0} \quad (16)$$

where C and C_0 are the capacitances per unit length of line with and without dielectric. The effective dielectric constant is also given as

$$\epsilon_{eff} = \frac{\epsilon_r + \epsilon_p}{2} + \frac{\epsilon_r - \epsilon_p}{2} \frac{1}{\sqrt{1 + \frac{12h}{\omega}}} \frac{\omega}{h} \geq 1 \quad (17)$$

And line extension $\Delta\ell$ as given by Hammerstad is [3]:

$$\frac{\Delta\ell}{h} = 0.412 \cdot \frac{\epsilon_e + 0.3 \frac{\omega}{h} + 0.262}{\epsilon_e - 0.258 \frac{\omega}{h} + 0.813} \quad (18)$$

NUMERICAL RESULTS

The results were obtained solving equations 15, 16, 17, and 18 numerically and are plotted in Fig. 2 to 5.

FIGURE 4

FIGURE 5

CONCLUSIONS

Calculations of length extension ($\Delta\ell$) in plasma medium for various plasma parameter values ($A = .1, .3, .5, .7, .9$) in an open microstrip configuration are obtained using spectral domain technique under quasi static approach [4,5] and by modifying Hammerstad equation for plasma media. Good agreement is found between the two results.

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REFERENCES

1. E. Yamashita "Variational method for the analysis of Microstrip-like transmission lines", IEEE trans. Microwave theory and techniques, Vol. MTT-16, pp. 529-535, August 1968.
2. B. Bhat & S.K. Koul "Lumped Capacitance, Open circuit end effects and edge capacitance of microstrip-like transmission lines for microwave and millimeter wave applications", IEEE trans., Microwave theory and techniques, Vol. MTT-32, No. 4, pp. 433-439, April 1984.
3. E.O. Hammerstad "Equations for Microstrip Circuit design", 5th European MW conference, pp. 268-272, 1975.
4. P. Silvester and P. Benedek, "Equivalent capacitance of Microstrip Open Circuits", IEEE trans. MTT-20, pp. 511-516.
5. B. Bhat & S.K. Koul, "Strip line-like transmission lines for Microwave Integrated Circuits", Willey Eastern Ltd.