

Review Article **Titanium-Nitride Coating of Orthopaedic Implants: A Review of the Literature**

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Surfaces of medical implants can be enhanced with the favorable properties of titanium-nitride (TiN). In a review of English medical literature, the effects of TiN-coating on orthopaedic implant material in preclinical studies were identified and the influence of these effects on the clinical outcome of TiN-coated orthopaedic implants was explored. The TiN-coating has a positive effect on the biocompatibility and tribological properties of implant surfaces; however, there are several reports of third body wear due to delamination, increased ultrahigh molecular weight polyethylene wear, and cohesive failure of the TiN-coating. This might be due to the coating process. The TiN-coating process should be optimized and standardized for titanium alloy articulating surfaces. The clinical benefit of TiN-coating of CoCrMo knee implant surfaces should be further investigated.

1. Introduction

Titanium-nitride (TiN) is a ceramic which has general properties such as great hardness (2000 kg/mm²), high decomposition temperature (2949°C), defect structure, that is, deviation from stoichiometry, chemical stability at roomtemperature, superconductivity, and a gold-yellow color [1]. TiN can be prepared by direct reaction of titanium or titanium hydrogen powder with nitrogen at 1200°C [1]. Using nitrogen ion implantation, physical vapor deposition, and plasma ion nitriding, titanium surfaces can be enhanced with a TiN layer [2]. Single crystals of TiN can also be vapor deposited on other metals [1]. Recently newer techniques have been introduced for TiN-coating of titanium alloys, such as powder immersion reaction assisted coating (PIRAC) [3], nitrogen plasma immersion ion implantation (PIII) [4], and Hardion+ nitrogen implantation technique [5], to improve the adhesion of the TiN-coating to the implant material.

TiN is mainly used as a coating to enhance other materials with the properties of TiN. TiN showed encouraging blood tolerability properties with a hemolysis percentage near to zero [6]. Therefore, TiN-coatings are used in cardiology for ventricular assist devices for patients with heart failure [7] and for pacemaker leads [8]. In neurology, TiN-coated electrodes are investigated for the development of chronically implanted devices for the treatment of, for example, spinal cord injury [9]. TiN-coating is applied in dentistry to dental implants, because of the excellent biological properties of TiN, such as the reduction of the release of cobalt-chromiummolybdenum (CoCrMo) ions, and the aesthetic aspect of the "golden color" [10, 11].

In 1972, Steinemenan patented the "use of implants of titanium or a titanium alloy for the surgical treatment of bones" [12]. This included a surface layer, for example, nitride, to prevent abrasion and corrosion of the implant and to prevent fretting of contacting implants [12]. In 1997, Buechel and Pappas patented the "prosthesis with biologically inert wear resistant surface" [13]. The load bearing surfaces are coated with biologically inert abrasion resistant material, such as TiN, preferably 8–10 microns thick, harder than the substrate for preventing wear and leaching of ions [13]. Besides the suggested beneficial effect of TiN-coating of

the bearing surfaces in cemented and uncemented prosthesis, the TiN-coating might also be beneficial at the bone-implant surface of uncemented prosthesis because it is biologically inert.

Untreated titanium-aluminum-vanadium alloy (Ti6Al4V) showed excessive wear of femoral heads, and surface treatment of Ti6Al4V by TiN-coating was discussed as a possibility to enhance the Ti6Al4V surface [14]. The purpose of this review is to identify the effects of TiN-coating of orthopaedic implant material in preclinical studies and whether these effects influence the clinical outcome of TiN-coated orthopaedic implants.

2. Method

This study focuseson preclinical and clinical studies using TiN-coated orthopaedic implants and implant material. Inclusion criteria were clinical studies on TiN-coated orthopaedic implants and preclinical studies on wear and biocompatibility of TiN-coated implant material. To identify all relevant studies on TiN-coated orthopaedic implants and implant material in English scientific literature, the following databases were searched: Medline (1947 to January 2015), Embase Classic and Embase (1947 to January 2015). No restrictions were made to the type of studies. Papers outside the English language, abstracts from scientific meetings, and unpublished reports were excluded. References of retrieved publications were used to add studies meeting the inclusion criteria that were missed by the electronic search. The Medline search is defined in Appendix. The query was checked for inconsistencies using PubMed Query Editor 0.1. Selection of studies was first performed by screening titles and abstracts. In case of insufficient information in the title or abstract, full text copies were retrieved to make a decision for the article selection. References of retrieved publications were used to add studies meeting the inclusion criteria that were missed by the electronic search.

3. Results

The results of the combined Medline and Embase search are shown in Figure 1. After examining titles and abstracts, a total of 335 out of 394 studies were excluded, due to the absence of abstracts (n = 32), research in medical fields other than orthopaedic (61 cardiovascular, 60 dental, 12 neurological, and 13 nuclear medicine), or other reasons (n = 157). No additional studies were identified from reference lists of the identified articles.

3.1. Preclinical Studies: Biocompatibility. A high variety of cell types were used for cell culture on TiN-coated implant materials: human bone marrow stem cells [15–17], human primary osteoblasts [18], Saos-2 osteoblast-like cells [19], human fibroblasts [20], human fetal osteoblasts [5, 21], U937 macrophages and L929 fibroblasts [22], mouse fibroblasts [23–25], murine monocytes [26], and murine calvarial osteoblasts [4, 27]. Studies on proliferation and differentiation of cells cultured on TiN-coated materials compared

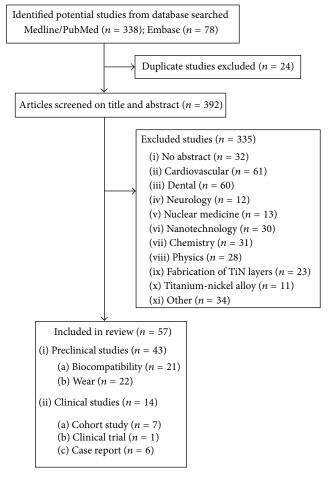


FIGURE 1: Flow diagram of the search process. Duplicate studies were excluded as well as studies of which there was no abstract. Studies on cardiovascular, dental, and neurological titanium-nitride coated implant material and other studies were excluded. Four studies on dental titanium-nitride coated implant material were included in this study in Section 3.1.

with control material are shown in Table 1. In several studies, no difference in proliferation of cells was found on TiNcoated materials compared with their controls [5, 15, 16, 19, 20]; however, an increase in proliferation of cells on TiNcoated materials compared with their controls was observed in other studies [4, 18, 23, 27, 28]. No differences were found on TiN-coated materials compared with their controls in differentiation of cells [15, 16, 18, 19, 27, 28], cell morphology [20, 24, 29], cell adhesion [15, 16, 29, 30], viability [21], and metabolic activity [24]. One study showed a higher number of cells adhered to TiN-coated material compared with the control [17]. Cell viability of cells cultured in the presence of Ti6Al4V, CoCrMo, and TiN-particles decreased after 4 hours to 58%, 44%, and 44%, respectively, but recovered after 24 hours to 78%, 51%, and 65%, respectively [26]. Viability of other cells cultured in the presence of different concentrations of TiN-debris was foremost influenced by the concentration of 50 μ m³ per cell [22].

TiN-coated materials were implanted in the femurs of dogs [31], rats [3], and rabbits [32]. In dog femurs, some

Study	Cell type	TiN-coated material	Proliferation	Differentiation
van Raay et al. (1995) [20]	Human fibroblasts	Glass cover slips	~	
Groessner-Schreiber et al. (2003) [23]	Mouse fibroblasts	cpTi	+	
Yeung et al. (2007) [4]	Mouse osteoblasts	NiTi; SS; Ti6Al4V	+	
Annunziata et al. (2008) [15]	BMSC	Ti6Al4V	~	~
Annunziata et al. (2011) [16]	BM-MSC	TPS	~	~
Czarnowska et al. (2011) [19]	Saos-2	Ti6Al4V	~	~
Durual et al. (2011) [18]	hOB	срТі	+	~
Gordin et al. (2012) [5]	hFOB 1.19	cpTi; Ti6Al4V	~	
Rieder et al. (2012) [28]	hOB	cpTi; SS	+	~
van Hove et al. (2013) [27]	MC3T3-E1	CoCrMo	+	~

TABLE 1: Preclinical studies on proliferation and differentiation of cells cultured on TiN-coated materials compared with control material.

~: no difference between TiN-coated material and the control; +: higher on TiN-coated material than the control; -: lower on TiN-coated material than the control. TiN: titanium-nitride; BMSC: human bone marrow stromal cells; BM-MSC: human bone marrow mesenchymal stem cells; Saos-2: sarcoma osteogenic, human osteoblast-like cells; hOB: human primary osteoblasts; hFOB 1.19: human fetal-osteoblastic cell line; MC3T3-E1: mouse calvarial osteoblast-like cell; cp Ti: commercially pure titanium; NiTi: nickel-titanium; SS: stainless steel; Ti6Al4V: titanium-aluminum-vanadium alloy; TPS: titanium plasma sprayed.

regions of the TiN-coated implants showed no bone opposition at 4 weeks, but from 24 weeks some specimens showed direct bone opposition [31]. The affinity of bone to the implant index of TiN-coated stainless steel was comparable with alumina, but not significantly better than uncoated stainless steel [31]. TiN-coated Ti6Al4V rods were implanted in rat femurs and showed similar biocompatibility and bonebonding properties compared with uncoated Ti6Al4V [3]. Relative bone area and bone-implant contact of TiN-coated commercially pure (cp) titanium threaded implants in rabbits was similar compared with TiO₂-coated cp titanium [32].

Results of three independent experiments showed a lower adhesion and proliferation (P < 0.05) over 24 hours of bacteria cultures *S. pyogenes* and *S. sanquinis* on TiNcoated titanium plasma sprayed surfaces (TPS) compared with uncoated TPS [16].

3.2. Preclinical Studies: Wear. TiN-coated Ti6Al4V showed a high scratch resistance [33, 34] and low coefficient of friction [33, 35], reduction of abrasive particle formation and less ultrahigh molecular weight polyethylene (UHMWPE) wear [35], more resistance to fretting and corrosion [5, 36, 37], reduction of wear [38], lower ion release rates [5, 39], and low fatigue cycle [40] compared with uncoated Ti6Al4V. Studies on wear of TiN-coated materials compared with their controls are shown in Table 2. The TiN-coating of Ti6Al4V showed minor to no signs of surface delamination, surface scratching, or coating failure in simulator tests [35, 37, 41-43]. However, in one study, a high incidence of adhesive coating failure was found in PVD TiN-coated Ti6Al4V, and the TiN-coating was prone to pitting and blistering at small coating defects [44]. Also, the wear behavior is affected heavily by pinholes in the PVD TiN-coating of CoCrMo [45, 46]. In a pin-on-plate test, TiN-coated CoCrMo showed a fourfold increase in wear rate compared with CoCrMo due to catastrophic adhesive failure of the TiN-coating [22]. In a metal-on-UHMWPE hip simulator test, minimal abrasive wear without signs of pitting, delamination, or overheating of the UHMWPE was found when in contact with TiNcoated Ti6Al4V [42]. TiN-coated Ti6Al4V showed lower

UHMWPE wear rates compared with Ti6Al4V [35] and 316L stainless steel [41]. TiN-coated CoCrMo showed less adhesion to polyethylene compared with CoCrMo, and CoCrMo showed a catalytic effect on the degradation of polyethylene whereas TiN is inert [46]. Although the volumetric wear rate of UHMWPE was reduced with 42% using a hybrid process for the TiN-film compared with commercialized CoCrMo [47], in another study, the average volumetric wear rate of UHMWPE to TiN-coated CoCrMo was not superior to CoCrMo or alumina [33]. Also, in a multidirectional wear test using UHMWPE specimens, no significant differences were found between TiN-coated CoCrMo and uncoated CoCrMo in coefficient of friction, and wear rate on damaged and undamaged surfaces [48]. Furthermore, friction and wear of the UHMWPE counterface was dependent of the lubricant used [24]. In the presence of protein, wear is very low independently of the surface roughness in the TiN/UHMWPE contact pair [49].

In a metal-on-metal hip simulator test, TiN-coated CoCrMo showed a lower wear rate compared with uncoated CoCrMo [50, 51]. The average wear of the uncoated insert articulating with a TiN-coated femoral head was greater compared with the uncoated femoral heads [51].

3.3. Clinical Studies. Clinical studies on survival of TiNcoated orthopaedic implants are presented in Table 3. In a cohort of 76 patients who received a cemented hip prosthesis, 60 received a CoCrMo head and 16 received a TiN-coated titanium head [52]. Loosening of the femoral component occurred in 44.4% of the hips with a TiN-coated titanium head and in 21.6% of the hips with a CoCrMo head (P = 0.11) with a 26-month follow-up [52].

In a postmortem retrieval analysis of a cementless TiNcoated Ti6Al4V THA one year after index surgery, the TiNcoated Ti6Al4V femoral head showed circular voids without TiN-coating and voids filled with circular droplets of pure titanium [53]. Adhered to the TiN-coating, pure titanium and Ti6Al4V debris was found [53]. In an analysis of four TiN-coated Ti6Al4V femoral heads retrieved at revision after a period of in vivo articulation against UHMWPE liners,

Ti6Al4V	Findings	TiN-coating related problems
	Reduction of UHMWPE wear*	
116A14 V	Reduction of weight loss and metal release*	
Ti6Al4V	Better scratch resistance*	
Ti6Al4V	No evidence of significant wear*	Microparticles and pinholes
TO-Ti6Al4V/SP-700	More mechanical damage*	Adhesive coating failure; pitting and blistering
CoCrMo	Lower wear*	Relatively high wear inserts
CoCrMo	Fourfold increase of wear [*]	Cohesive failure
SS	Lower UHMWPE wear rate*	
CoCrMo	Lower wear*	Some localized damage
CoCrMo	Higher UHMWPE volumetric wear rate*	
CoCrMo	No scratches*	Polyethylene in pinholes
Ti6Al4V	Lower wear*	Higher wear of TiN compared with TiAlN
CoCrMo	Lower UHMWPE volumetric wear rate [*]	
	CoCrMo SS CoCrMo CoCrMo CoCrMo Ti6Al4V Ti6Al4V CoCrMo Ti6Al4V arion:arion:arion-m	alyethyler ron-moly ting: AV

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Study	Type	Type Prosthesis	TiN-coated material Number	Number	Fixation	Follow-up	Survival	Survival Reasons for revision
Buechel and Pappas (1992) [64]	Cohort	TAP	Ti6Al4V	14	Cementless	15 (5-24)	100%	None
Massoud et al. (1997) [52]	Cohort	THP	Ti nos	16	Cemented	26	56%	Aseptic loosening
Buechel et al. (2003) [63]	Cohort	TAP	Ti6Al4V	50	Cementless	Cementless 60 (24–120)	93.5%	Malalignment; PE wear; component subsidence
Buechel et al. (2004) [62]	Cohort	THP	Ti6Al4V	130	Cementless	77 (27–134)	95.5%	Aseptic loosening; bearing dissociation
Buechel and Pappas (2011) [55]	Cohort	RHP	Ti6Al4V	60	Cementless	36 (8-70)	91.8%	Not specified
Mohammed et al. (2014) [58]	Cohort	TKP	CoCrMo	305	Cementless 79 (36-122)	79 (36–122)	95.1%	Prosthetic fractures; aseptic loosening; alignment
van Hove et al. (2015) [61]	RCT	TKP	CoCrMo	50	Cementless	60	96%	Aseptic loosening
All prosthetic joint articulations were TiN-coa	ted implant n	naterial to UHN	IWPE. Follow-up is presen	ted as mean (range) in months	. RCT: randomiz	ed clinical tri	All prosthetic joint articulations were TiN-coated implant material to UHMWPE. Follow-up is presented as mean (range) in months. RCT: randomized clinical trial; TAP: total ankle prosthesis; THP: total hip
prosthesis; RHP: resurfacing total hip prosthesis; TKP: total knee prosthesis; Ti6A14V: titanium-vanadium alloy; CoCrMo: cobalt-chromium-molybdenum alloy; Ti nos: titanium not otherwise specified.	s; TKP: total k	nee prosthesis;]	li6Al4V: titanium-aluminu	m-vanadium	alloy; CoCrMo: c	obalt-chromium-	molybdenum	alloy; Ti nos: titanium not otherwise specified.

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TiN-coating breakthrough and fretting occurred in 2 out of 4 retrieved prostheses [54].

Failures of a cementless TiN-coated titanium alloy-on-UHMWPE resurfacing THA were suggested to be due to the use of conventional UHMWPE instead of highly cross-linked UHMWPE [55]. In a case of a failed cementless TiN-coated titanium alloy-on-UHMWPE resurfacing THA eleven years after index surgery, severe wear of the polyethylene liner with erosion of the femoral head into the metal acetabular shell was reported [56].

In the radiological follow-up (16.6 months, range 12–39 months) of 330 hips with a press-fit polyethylene cup with TiN-coated stainless steel mesh (Sulmesh, Sulzer, Winterthur, Switzerland) for the bone-implant interface, there was one case showing a radiolucent line around the cup; however, this was without clinical problems [57]. There was insufficient stability of the mesh in 4 of the 330 cases [57].

In a retrospective study of mainly cementless TiNcoated CoCrMo mobile bearing TKAs, revision surgery was performed in 4.9% [58]. Prosthetic fractures were found in four knees and involved the posteromedial flange of rightsided, size 5, femoral components only [58]. A case report on the fracture of a cementless TiN-coated CoCrMo femoral component met with these findings [59]. Another case, which concerned the fracture of the medial flange posterior to the peg of a TiN-coated Ti6Al4V TKA, was also reported [60].

In a recently published RCT, no differences in postoperative pain, KSS, revision surgery, knee flexion and knee flexion contracture, knee circumference, and knee skin temperature were observed between the TiN-coated CoCrMo TKA (n =51) and a CoCrMo TKA (n = 50) [61]. In both groups two knees were revised for reasons unrelated to the TiN-coating, which resulted in a 5-year survival of 96% [61].

4. Discussion

In preclinical studies, TiN-coating of implant materials showed to be biocompatible with mainly favorable tribological properties. Several cohort studies of TiN-coated implants showed an overall survival exceeding 90% with a followup of 15 to 77 months and good clinical results [55, 58, 62-64]. There were no clinical studies that compared TiNcoated Ti6Al4V implants with uncoated Ti6Al4V implants. One study compared a TiN-coated CoCrMo implant with an uncoated CoCrMo implant and found no difference in clinical outcome or survival [61]. Although preclinical studies showed that TiN-coating of implant material supplies the implant surface with favorable properties, there is insufficient evidence that the TiN-coating affects the clinical outcome and survival of implants in clinical studies. Nonetheless, concerns were raised in a preclinical study about PVD TiN-coated Ti6Al4V because of adhesive coating failure due to coating defects [44]. In retrieved PVD TiN-coated Ti6Al4V femoral heads, the TiN-coating was damaged [53, 54]. Delaminated surface asperities of the TiN-coated femoral head might result in wear debris and lead to adhesive wear on the articular surface [53]. It was suggested that the underlying substrate is prone for third body wear, in case of coating breakthrough [53, 54, 65]. Also, it was advised to handle

TiN-coated implants carefully with proper soft instruments, because the thin coating may be easily cracked or scratched by hard surgical tools due to high local stresses at contact points between hard materials opening direct pathways for corrosion leading to delamination [65]. There were no reports of failures of other surface treatments which result in a TiN layer on Ti6Al4V, such as PIRAC [3, 41], PIII [4], and Hardion+ [5].

In a pins-and-plate test of polished PVD TiN-coated CoCrMo a higher surface roughness, catastrophic cohesive failure within the layers of the TiN-coating and a fourfold increase in wear was found [22]. Higher surface roughness of PVD TiN-coated CoCrMo was due to small pits and pinholes related to the PVD process [45]. These pits and pinholes were filled with UHMWPE debris [45, 46]. Although this could be a reason for implant failure, there was no report of failure of a TiN-coated CoCrMo implant in contrast to TiNcoated Ti6Al4V implant. This could be due to a worse TiNcoating layer performance on Ti6Al4V than on CoCrMo [45]. Although the hardness of Ti6Al4V and CoCrMo is similar, Ti6Al4V has a higher difference in elastic modulus with the TiN-coating compared with CoCrMo [45]. It is suggested that this difference in elastic modulus leads to failure of the bonding layer between the TiN-coating and Ti6Al4V [45]. This might induce a cascade of wear and failure of the implant.

A high incidence of aseptic loosening was found with a new design of cemented THA using CoCrMo and TiNcoated titanium heads on UHMWPE liner [52]. There was no significant difference in aseptic loosening of the femoral stem with either the CoCrMo or TiN-coated titanium heads [52]. Furthermore, two brands of cement were used, but no multivariate analysis was performed [52]. Of the cases revised the polyethylene had no visible wear [52]. It remains unclear in this study whether TiN-coated titanium heads have a negative effect on the survival of the implant. That particular implant has been taken off the market.

Prosthetic fractures of the medial flange of size 5 rightsided TiN-coated CoCrMo femoral component of a TKA were found [58, 59]. It is unclear if all size 5 right-sided TiNcoated CoCrMo femoral components in that study fractured. However, the junction of the posterior and the distal chamfer at the medial flange of the implant had a narrow surface cross section, which resulted in a high stress concentration [58]. Adjustments were made to the design and there have been no reports of prosthetic fractures ever since [58]. It is unlikely that the TiN-coating was a cause for these prosthetic fractures.

Noteworthy is that of the 7 clinical studies, case reports not included, 4 studies [55, 62–64] on survival and results of TiN-coated implants were performed by researchers, who patented one of the implants [13] and who also founded the company which produced the implant. This might imply a conflict of interests and might be of influence on the results.

5. Conclusion

Titanium alloys used for articulating surfaces require surface treatment to increase hardness and reduce wear. TiNcoating has a favorable effect on the biocompatibility and tribological properties of implant surfaces. However, there are reports of third body wear due to delamination of the PVD TiN-coating on Ti6Al4V, increased UHMWPE wear and cohesive failure of the PVD TiN-coating on CoCrMo of hip implants in preclinical studies, and TiN-coating breakthrough and fretting in a retrieval study of TiN-coated Ti6Al4V femoral heads. These adverse effects might be related to the various coating processes of titanium alloys. The TiN-coating process of titanium alloy articulating surfaces should be optimized and standardized. There were no reports of adverse effects related to TiN-coating of CoCrMo knee implants. Clinical benefit of TiN-coating of CoCrMo knee implant articulating surfaces should be investigated further.

Appendix

Pubmed/Medline Search strategy: ((((((("shoulder" [MeSH Terms] OR "shoulder"[Tiab]) AND ("prosthesis implantation"[MeSH Terms] OR ("prosthesis"[Tiab] AND "implantation" [Tiab]) OR "prosthesis implantation" [Tiab] OR "prosthesis" [Tiab] OR "prostheses and implants" [MeSH Terms] OR ("prostheses" [Tiab] AND "implants" [Tiab]) OR "prostheses and implants" [Tiab])) OR (("shoulder" [MeSH Terms] OR "shoulder" [Tiab]) AND ("arthroplasty" [MeSH Terms] OR "arthroplasty" [Tiab]))) OR (("shoulder" [MeSH Terms] OR "shoulder"[Tiab]) AND ("replantation"[MeSH Terms] OR "replantation" [Tiab] OR "replacement" [Tiab]))) OR (("hip prosthesis" [MeSH Terms] OR ("hip" [Tiab] AND "prosthesis"[Tiab]) OR "hip prosthesis"[Tiab] OR "arthroplasty, replacement, hip" [MeSH Terms] OR ("arthroplasty" [Tiab] AND "replacement" [Tiab] AND "hip"[Tiab]) OR "hip replacement arthroplasty"[Tiab] OR ("hip"[Tiab] AND "prosthesis"[Tiab])) OR (("hip"[MeSH Terms] OR "hip"[Tiab]) AND ("arthroplasty"[MeSH Terms] OR "arthroplasty" [Tiab])))) OR (("arthroplasty, replacement, knee" [MeSH Terms] OR ("arthroplasty" [Tiab] AND "replacement" [Tiab] AND "knee" [Tiab]) OR "knee replacement arthroplasty"[Tiab] OR ("knee"[Tiab] AND "arthroplasty"[Tiab]) OR "knee arthroplasty"[Tiab]) OR ("knee prosthesis" [MeSH Terms] OR ("knee" [Tiab] AND "prosthesis" [Tiab]) OR "knee prosthesis" [Tiab] OR "arthroplasty, replacement, knee" [MeSH Terms] OR ("arthroplasty" [Tiab] AND "replacement" [Tiab] AND "knee"[Tiab]) OR "knee replacement arthroplasty"[Tiab] OR ("knee"[Tiab] AND "prosthesis"[Tiab])))) OR (("ankle" [MeSH Terms] OR "ankle" [Tiab] OR "ankle joint" [MeSH Terms] OR ("ankle"[Tiab] AND "joint"[Tiab]) OR "ankle joint" [Tiab]) AND ("arthroplasty" [MeSH Terms] OR "arthroplasty"[Tiab])) OR ("ankle"[MeSH Terms] OR "ankle" [Tiab] OR "ankle joint" [MeSH Terms] OR ("ankle" [Tiab] AND "joint" [Tiab]) OR "ankle joint" [Tiab]) AND "prosthesis implantation" [MeSH Terms] OR ("prosthesis"[Tiab] AND "implantation"[Tiab]) OR "prosthesis implantation"[Tiab] OR "prosthesis"[Tiab] OR "prostheses and implants" [MeSH Terms] OR "prostheses" [Tiab]) AND ((ti2n[Tiab] OR TiNi[Tiab]) OR ("titanium nitride"[Tiab] AND coating[Tiab])) OR "titanium nitride"[Tiab].

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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