

## Research Article

# Compact Microstrip Bandpass Diplexer Based on Twist Revised Split Ring Resonators

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Based on the twist revised split ring resonators (TR-SRRs) inspired filter unit a microstrip bandpass diplexer with highly compact size and high frequency selection and isolation properties is synthesized and systematically characterized. The proposed filter unit exhibits both electric and magnetic coupling effects and possesses two resonance modes (magnetic and electronic resonances). The two resonance modes can be flexibly controlled by adjusting the gap between the two TR-SRRs. The synthesized diplexer has very simple configuration with size of  $0.217\lambda_d \times 0.217\lambda_d$  and degree of freedom for impedance matching. Measurement and simulation demonstrations are performed in this paper and a good agreement is achieved. The measured results indicate two quite close frequency channels (centered at 2.16 GHz and 2.91 GHz) with isolation larger than 30 dB. The proposed diplexer can be easily integrated into miniaturized RF/microwave integrated circuits.

## 1. Introduction

In modern wireless communications, the obvious development tendency is to integrate more than one communication mode in a single termination. Based on this requirement, some multiband/wideband antennas have been designed and therefore we need filters following the antennas to separate the different signals toward different frequency channels and modules [1, 2]. Various diplexers/triplexes have been reported in recent years based on different filter and/or resonator units, for example, parallel-coupled filter [3], T-shaped resonator [4], stub-loaded resonator [5, 6], quarter-wavelength resonator [7], dual-mode resonator [8], and common shorted stubs [9] to realize the assignments. In particular, the filter designs focusing on compact size, high isolation, and out-of-band rejection properties are developed based on stepped impedance coupled-line resonator [10, 11], double-sided parallel-strip line [12], half-wavelength open-loop resonators [13], hybrid resonators [14], series LC tanks [15], and substrate integrated waveguide resonator [16].

On the other hand, the artificial structured resonators with dimensional size much smaller than the operating wavelength have been attracting exciting interests in the designs of compact diplexers/triplexes. For example, the split ring resonator (SRR) as the basic artificial unit cell has been widely used to design microwave/millimeter wave components [17] and its complementary inclusion applied to the coplanar waveguide and substrate integrated waveguide can realize high performance diplexers [18, 19]. By using composite quarter-wave right/left-handed (CRLH) resonators or balanced CRLH resonators [20–23], one can obtain more compact size compared with the conventional diplexers/triplexes. However, most of these archives including conventional resonators and artificial structured resonators have complex inclusions, precise-designed T-junction, and impedance circuits which will result in large size and high costs.

In this paper, a new type of diplexer is synthesized by directly using two groups of revised SRR (by electric shorting one end of the SRR to ground plane) pairs with twist arrangements. The proposed twist revised SRR (TR-SRR) inspired

filter unit exhibits both electric and magnetic coupling effects and has two resonance modes (electric and magnetic resonances) with very small electric size. Therefore the designed diplexer possesses highly compact size compared with other recently reported inclusions. The TR-SRR and filter unit are firstly analyzed, and then the synthesized diplexer is demonstrated by both experimental and numerical methods. Finally the comparisons with previously reported diplexers are presented and discussed.

## 2. Filter Design and Analysis

Figure 1(a) shows the top and side views of the proposed revised SRR configuration. Two extended microstrip lines are collected to the split of a conventional SRR and one of the extended ends is electric shorted to ground plane. Such kind of design can be considered as a new quarter-wavelength resonator from the equivalent circuit view. The new revised SRR can exhibit impedance matching to the  $50\ \Omega$  feed line, which connects to the shorted branch as shown in Figure 1(a), without additional complex circuits. The electric and magnetic fields at the resonance frequency for one revised SRR are shown in Figure 1(b), which indicate asymmetric field distributions and will give us abundant choices for the coupling filter design. After numerical investigations by HFSS full-wave simulations, the twist arrangement as shown in the inset of Figure 1(c) has better passband characteristics [24] and also can be easily used to synthesize the diplexer which will be discussed later. As an example, the simulated transmission and reflection properties of the designed filter unit are shown in Figure 1(c) with parameters shown as follows, in millimeter:  $a = 4$ ,  $b = 2.7$ ,  $c = 0.4$ ,  $w = 0.4$ ,  $r = 0.15$ ,  $g = 0.5$ , and  $t = 0.8$ . Rogers RO4003 substrate, which has the relative dielectric constant  $\epsilon_r = 3.55$  and loss tangent  $\tan \delta = 0.0027$ , is used in this paper and the thickness of the SRRs and ground plane is  $0.03\ \text{mm}$ . The dimension of filter unit is  $8\ \text{mm} \times 12.4\ \text{mm}$ . As can be seen, such filter exhibits a passband centered at  $2.97\ \text{GHz}$  with a  $3\ \text{dB}$  bandwidth of  $0.46\ \text{GHz}$ . From the reflection curve in Figure 1(c) there are two poles at  $2.88$  and  $3.05\ \text{GHz}$  and the surface currents on the twist SRR pairs at such two frequencies show typical electric and magnetic resonance modes. Moreover, there is a transmission zero below the passband. From the mixed coupling filter theory, the magnetic coupling for our twist SRR based filter is larger than the electric coupling, and as a result the transmission in lower band is related to strong magnetic coupling [25, 26]. It can contribute to the high isolation when synthesizing the diplexer in the next section by using the proposed filter unit.

By altering the gap values between the TR-SRR pairs, one can obtain the changing properties of the filter passband as shown in Figure 2(a). It indicates an expanded bandwidth when decreasing the gap. This is due to the enhancements of both electric and magnetic coupling in the adjacent area. Figure 2(b) shows the captured frequency shift properties of the two resonance modes as functions of gap value  $g$ . The coupling coefficient  $k$  and the external quality factors  $Q_e$  can

then be calculated from the two resonance frequencies by using coupling theory [26]:

$$k = \frac{(f_2^2 - f_1^2)}{(f_2^2 + f_1^2)},$$

$$Q_{e1} = \frac{f_1}{\Delta f_{3\ \text{dB}}},$$

$$Q_{e2} = \frac{f_2}{\Delta f_{3\ \text{dB}}},$$
(1)

where  $f_1$  and  $f_2$  correspond to the lower and higher resonance frequencies and  $\Delta f_{3\ \text{dB}}$  is the  $3\ \text{dB}$  frequency bandwidth. In our previous work [24], it has shown that our design exhibits high external quality factors, which can contribute to low insertion loss, flat passband, and good return loss. The calculated coupling coefficient shown in Figure 2(b) indicates that when decreasing the gap values the coupling between the two SRRs will be enhanced. However, at smaller gap values, the coupling is too strong so that the two resonance modes separate far from each other and result in the dropdown within the passband as shown in Figure 2(a). Therefore, both the bandwidth and insertion loss will be considered when choosing the gap values, and the isolation will be also taken into consideration when designing the diplexer.

## 3. Diplexer Synthesis and Demonstration

Based on the above analysis for the filter unit, here the diplexer is synthesized by placing properly two filter units side by side with different sizes and connecting to the input port with a simple T-junction as shown in Figure 3(a). Such design can effectively use the limited space to achieve the highly compact inclusion. By using the same Rogers RO4003 substrate as above, the dimensional parameters are finally optimized as follows, in millimeter:  $a_1 = 5$ ,  $a_2 = 4$ ,  $b_1 = 3.7$ ,  $b_2 = 2.7$ ,  $c = 0.4$ ,  $e = 9.2$ ,  $f = 1.76$ ,  $g_1 = 0.5$ ,  $g_2 = 0.5$ ,  $w = 0.4$ , and  $r = 0.15$ . The overall dimensional size is  $d \times d = 16\ \text{mm} \times 16\ \text{mm}$ . The photograph of fabricated diplexer is also shown in Figure 3(b) with the definitions of the three ports. Each port is soldered with a  $50\ \Omega$  microminiature coaxial connectors, operated from DC to  $6\ \text{GHz}$ .

Then the scattering parameters for the diplexer are experimentally measured by a two-port vector network analyzer (Agilent N5230A). In measurements, the third port is terminated by a wide-band  $50\ \Omega$  load when measuring two of these three ports for the diplexer. The measured results are shown in Figure 4 and the corresponding numerical results are also presented for comparisons. As can be seen, good agreements are achieved between measurements and simulations which demonstrate the corrections of the design and synthesis. The measured two channels are located at  $2.16\ \text{GHz}$  and  $2.91\ \text{GHz}$  with  $3\ \text{dB}$  bandwidths of  $0.3\ \text{GHz}$  and  $0.32\ \text{GHz}$ , respectively. The measured insertion losses are  $1.25\ \text{dB}$  and  $1.48\ \text{dB}$ , respectively, for the two channels, which show quite low values due to the simple configuration (including the extra losses from the microminiature coaxial

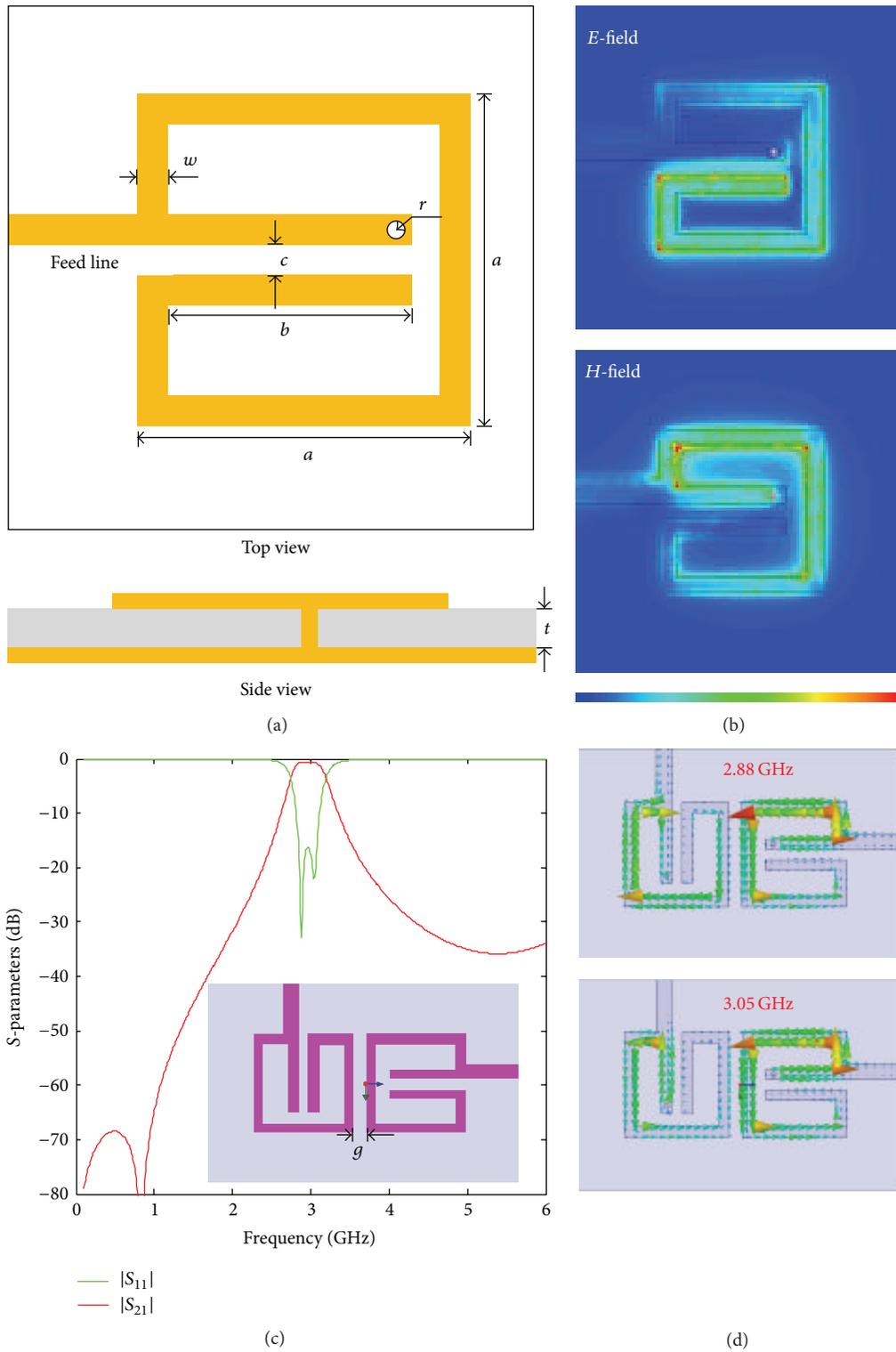


FIGURE 1: (a) The new revised SRR, (b) the electric and magnetic field distributions near the SRR at resonance frequency, (c) the twist SRRs inspired filter unit and its simulated scattering parameters, and (d) the surface current distributions at the two resonance modes.

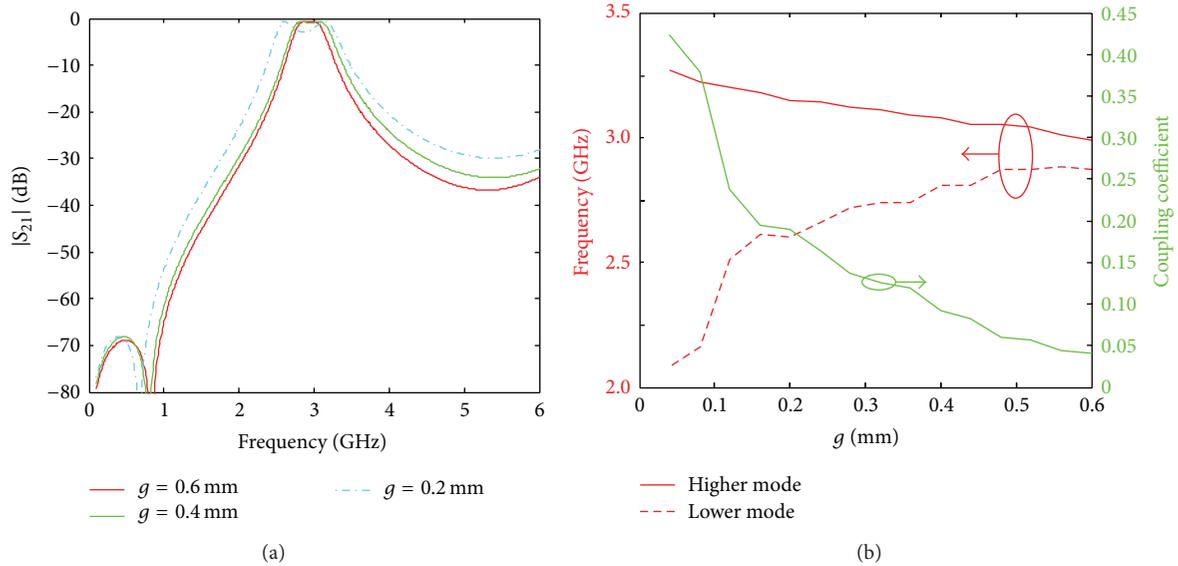


FIGURE 2: (a) Simulated transmissions for the twist SRR inspired filter unit at different gaps and (b) the changing properties for the two resonance frequencies and the calculated mix coupling coefficient as functions of gap  $g$ .

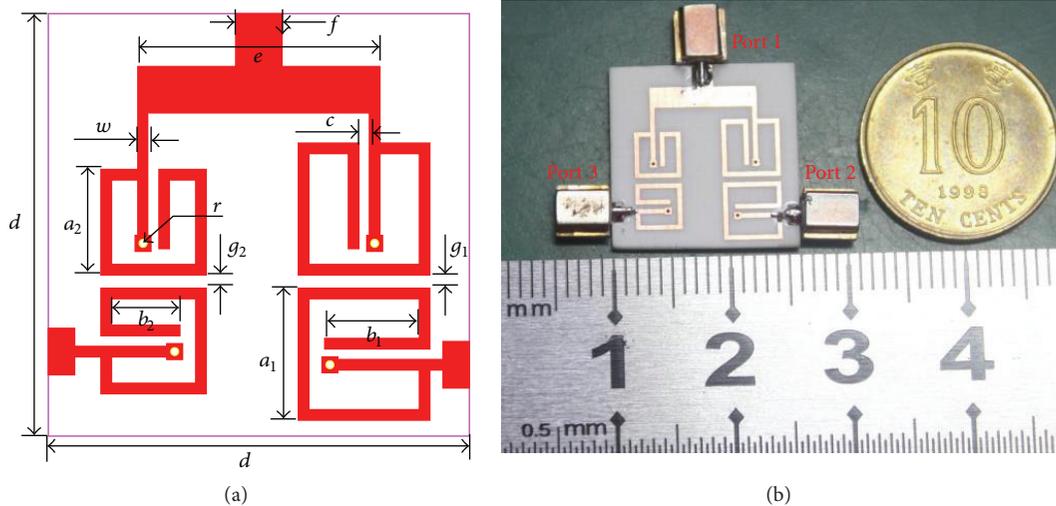


FIGURE 3: (a) The synthesized compact diplexer layout with dimensional parameters and (b) the photograph of fabricated diplexer.

connectors). The return losses for the input port (Port 1) at the two channels are 25 dB and 14 dB and for the two output ports (Ports 2 and 3) are 26 dB and 21 dB. These are quite good impedance matching properties even though they are without a carefully designed matching circuit (just conventional 50  $\Omega$  microstrip line). The out-of-band rejection is more than 30 dB and reaches up to 5 GHz for the lower channel and in the entire measured frequency region for the higher channel. Moreover, the measured isolation between the two output ports shows a value of larger than 30 dB, which is also a good isolation property for the proposed highly compact inclusion. Such isolation can be further increased by adding more SRRs in the filter units to get more transmission

zeros below and above the operating bands but will destroy the compact configuration size.

Finally, the performance comparisons for the proposed diplexer and other recently reported designs are concluded in Table 1. Here  $\lambda_d$  is the operating wavelength within the dielectric substrate defined as  $\lambda_d = c/(\sqrt{\epsilon_r}f)$ , where  $\epsilon_r$  is the relative permittivity of substrate,  $f$  is the center frequency of first channel, and  $c$  is the speed of light in free space. It can be found that the diplexer proposed in this paper has comparable frequency selection and isolation properties and almost the smallest inclusion size (except the design reported in [13] using complex series LC tanks and meander line inductors to achieve the compact resonators).

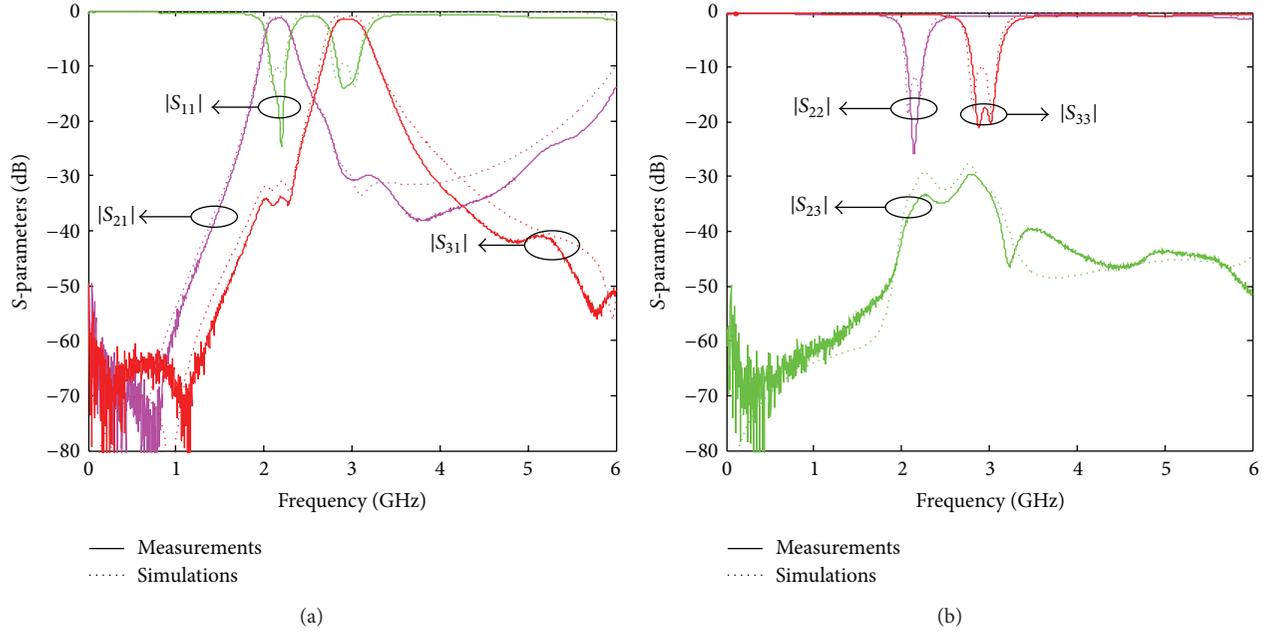


FIGURE 4: (a) The measured and simulated reflections of Port 1 and transmissions of Ports 2 and 3 from Port 1 and (b) reflection for Ports 2 and 3 and the transmission between Ports 2 and 3.

TABLE 1: Comparisons between the proposed diplexer and other compact designs.

Designs	$\epsilon_r$ of substrate	Frequency (GHz)	Size ( $\lambda_d^2$ )	Insertion loss (dB)	Isolation (dB)
[11]	4.5	1.85, 2.5	$0.424 \times 0.382$	2.05, 2.15	>25
[14]	2.2	1.82, 2.5	$0.193 \times 0.297$	2.51, 2.17	>55
[15]	3.38	1.8, 3.6	$0.153 \times 0.09$	0.4, 0.5	>30
[16]	2.55	8, 9	$1.325 \times 1.325$	2.86, 3.04	>40
[22]	2.2	1.8, 2.35	$0.178 \times 0.341$	1.34, 1.44	>25
[23]	2.65	3.5, 4	$0.944 \times 0.765$	1.95, 1.97	>25
This work	3.55	2.16, 2.91	$0.217 \times 0.217$	1.25, 1.48	>30

## 4. Conclusions

In this paper, a new type of TR-SRRs inspired bandpass filter unit is designed and then a highly compact diplexer based on the designed filters is synthesized and demonstrated. Such diplexer with size of  $0.217\lambda_d \times 0.217\lambda_d$  exhibits good characteristics, including the close channels, low insertion loss, wide out-of-band rejection, and high isolation, which can be flexibly integrated into miniaturized RF/microwave/millimeter wave circuits and systems.

## Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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