Research Article

Modeling the Effect of Plants and Peat on Evapotranspiration in Constructed Wetlands

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Evapotranspiration (ET) in constructed wetlands (CWs) represents a major factor affecting hydrodynamics and treatment performances. The presence of high ET was shown to improve global treatment performances, however ET is affected by a wide range of parameters including plant development and CWs age. Our study aimed at modelling the effect of plants and peat on ET in CWs; since we hypothesized peat could behave like the presence of accumulated organic matter in old CWs. Treatment performances, hydraulic behaviour, and ET rates were measured in eight 1 m² CWs mesocosm (1 unplanted, 1 unplanted with peat, 2 planted with Phragmites australis, 2 planted with Typha latifolia and 2 planted with Phragmites australis with peat). Two models were built using first order kinetics to simulate COD and TKN removal with ET as an input. The effect of peat was positive on ET and was related to the better growth conditions it offered to macrophytes. Removal efficiency in pilot units with larger ET was higher for TKN. On average, results show for COD a k₂₀ value of 0.88 d⁻¹ and 0.36 d⁻¹ for TKN. We hypothesized that the main effect of ET was to concentrate effluent, thus enhancing degradation rates.

1. Introduction

In constructed wetlands (CWs) for wastewater treatment, evapotranspiration (ET) may represent a major factor increasing the hydraulic residence time (HRT) during summer months in temperate countries. In horizontal subsurface flow constructed wetlands (HSSFCWs), ET ranges between 0 and 50 mm/d [1] and can reach up to 200 mm/d in favorable periods [2]. High ET may improve global treatment performances [3] and modify water flow [4]. ET follows a diurnal cycle and is affected by a wide range of parameters such as plant development, CW design (surface, subsurface or vertical flow), and CW age [5].

Simulations were used to predict the performance of CWs using a direct plug flow reactor model [1], a plug flow with axial dispersion model (PFD) [4, 6–8], a stirred tank in series model [9] or a combination of these models [10]. One of the most limiting factors in predicting CWs efficiency was identified as the hydraulic behavior governed by environmental conditions [11, 12]. Furthermore, in modeling or design equations, ET can be taken into account as an input to the model [8].

The aim of our work was first to determine (1) the effect of peat and of plant species on ET, since we hypothesized peat could behave like presence of accumulated organic matter in old CWs and (2) the importance of ET on treatment performances in an experimental constructed wetland system. The hydraulic behavior of pilot scale CWs was modeled during high ET rate periods and with ET values as an input of the hydraulics and performance models.

2. Material and Methods

Eight 1 m² wetland mesocosms (1.2 m long × 0.8 m wide × 0.3 m deep) were used in this study. Each mesocosm (Figure 1) was fed with 30 L/d (two batches per day) of a reconstituted fish farm effluent (187 mg TSS/L, 373 mg
COD/L and 12.4 mg TKN/L). All mesocosms were filled with a combination of rock media (Table 1) and in four of them 60 L of peat was added and mixed (initially to reduce alkalinity caused by steel slag). The substrate was composed by mass of 25% 5–10 mm electric arc furnace EAF-steel slag, 20% 2.5–10 mm limestone, and 55% of 2.5–10 mm granite gravel. Four mesocosms were planted with *Phragmites australis*, two with *Typha latifolia* and two were left unplanted (Table 1). Planting was done one year prior to the experiment, during the summer of 2000, to allow adequate establishment. More details on the experimental setup are provided by [13].

Experiments were conducted between July and August 2001 in a greenhouse at the Botanical Garden of Montreal. Concentration of TSS, COD, and TKN were measured daily at the inlet and outlet of each mesocosms according to standards methods [14]. Pulse input tracer studies were conducted using lithium chloride (LiCl) simultaneously in all eight mesocosms operating at the same inflow. HRT was estimated using integration of response curves.

Absorption spectrophotometry. The amount of daily water lost by ET was estimated as the difference between inflow and outflow. Treatment performances ($P$) were calculated based on pollutant mass flow removal

$$P = 100 \cdot \left(1 - \frac{Q_i \cdot C_i}{Q_o \cdot C_o}\right)$$

where $Q = \text{flow}$, $C = \text{pollutant concentration}$, $i = \text{inlet}$, $o = \text{outlet}$.

### 2.1. Hydraulic Models

The plug flow with axial dispersion model (PFD) [15] was preferred to the classical plug flow model with a background concentration (see [16]). This choice was made in order to achieve the objective of estimating the effect of plant presence and activity on dispersion inside the mesocosom.

A second model was built (using the object oriented Visim software), based on the hypothesis of a two layers flows: (1) the surface layer modeling the rhizomial part of the mesocosom, with a time delay block taking into account ET, and (2) a bottom layer. The two-layer model (TLM) was built by associating several basic blocks (continuous stirred tank, plug flow and gain) specified using Laplace transforms (Figure 4).

### 2.2. Performance Models

COD and TKN treatment performances were predicted by using an integrated form of the two hydraulics models. Volumetric first order kinetics ($k$) were assumed for COD and TKN degradation rate. The integrated forms of the PFD model [17] and of the TLM are presented respectively in

$$C_s \over C_o = \frac{4 \cdot a \cdot e^{(Pe/2)}}{(1 + a)^2 \cdot \left[e^{(a \cdot Pe/2)} - 1\right] e^{(-a \cdot Pe/2)}}$$

with $a = \sqrt{1 + 4 \cdot k \cdot \tau \over Pe}$

$$C_s \over C_o = G \cdot \frac{1}{(1 + 2 \cdot k \cdot \tau)^2} \cdot e^{-k \cdot (td)} + (1 - G) \cdot \frac{1}{(1 + 2 \cdot k)^2}$$

with $C_s, C_o$: outlet and inlet COD and TKN concentration, respectively, [mg/L], Pe: Péclet number according to PFD model. Pe = 1/D with $D$ System dispersion number [−], $\tau$: HRT estimated with PFD model [d], $td$: time delay in first layer of the conceptualized model [d], $k$: first-order volumetric kinetic constant [d$^{-1}$], $k_0(\theta)(T-20)$ with $T$ effective temperature. $\theta$ constant (1.06). $k_0$ first-order volumetric kinetic constant at 20°C, determined for COD and TKN [d$^{-1}$]. $G$: ratio in the first layer of the TLM model [−].

Those two models have been used to simulate treatment performances on COD and TKN removal during the 30 days of test.

### 3. Results And Discussion

#### 3.1. Influence of Peat on ET Rates and Hydraulic

On average, ET was highest in planted peat mesocosms (16.7 mm/d
in R3) and lowest in the unplanted control without peat (0.1 mm/d in U1). Maximal daily values were estimated at 20 mm/d in R3 and R4, which are in accordance with values proposed in the literature [1, 3, 4].

Association between reed and peat generated the most important ET rates (Table 2). The positive effect of peat on ET can be explained on the one hand by the better growth conditions it offered to plants (presence of more plant biomass). On the other, the effect of peat on mesocosms hydraulic behavior was hypothesized to be similar to accumulated organic matter appearing in constructed wetlands over time [18]. As observed between the two unplanted units, peat enhanced the retention by acting as a sponge. In absence of peat, while the HRT remained fairly close to the theoretical value in U1, it was up to 30% greater than the theoretical hydraulic residence time value in pilot units with high ET (those with large active macrophytes). Experimental HRT, determined using response curves (Figure 2), were always greater than theoretical values (Table 2). This was a possible consequence of the non-ideal flow in the different reactors.

3.2. Influence of Plant Presence and Species on ET Rates and Hydraulic. Effects of Phragmites and Typha on ET rates were similar (Table 2). The relationship between ET and plants seemed mostly related to plant biomass irrespective of plant species.

The ratio of tracer collected at outlets was sufficient for a more detailed analysis in all cases except for the R3 and R4 mesocosms where less than 45% of the tracer was recovered (Table 1). In the response curves of the R3 and R4 mesocosms, a small tracer peak was observed after which lithium concentrations never returned to background levels, even after 30 days (not shown). This was most probably the consequence of the sorption of lithium by peat (also observed even after 30 days (not shown)). This was probably due to the small size of the mesocosms which led to a permanent bypass along the wall.

3.3. Effect of ET Rates on COD and TKN Removal, Modeling. No TSS removal differences were found between the different mesocosms (results not shown). COD removal was higher in U1 than in U2, and this was likely due to the release of organic carbon by the peat. This difference was less pronounced between R1 and R2 (planted with reed) and R3 and R4 (planted with reed and with peat). Overall, there were slight differences between performances of all the planted mesocosms for COD degradation (Figure 1), irrespective of ET and plant species.

Removal efficiency in pilot units with higher ET (more than 50% of inflow) was greater for TKN (Figure 1). In R3 and R4 mesocosms, average net rate of N mineralization values of 0.36 g m⁻² d⁻¹ were reported (which represented almost all of the input) until in unplanted units it was about 0.15 g m⁻² d⁻¹. In similar pilot units and experimental conditions, rates of 0.22 to 0.53 g m⁻² d⁻¹ have been reported [20]. Nitrification should have been enhanced by the presence of well established plant biomass associated to high ET rates, furthermore the contact time between plants shoots (the principal oxygen supplier in HSSFCWs) and effluent was extended.

Performance models (2) were used to predict treatment performances of pilots U1, R1, R2, C1, C2. The first step was to determine the best k₂₀ value for COD and TKN, to fit the model with experimental data. On average, results show a k₂₀ value of 0.88 for COD removal and 0.36 for TKN removal. Large ranges of annual average values, from 0.06 to 6.11 for BOD₅ and from 0.06 to 0.16 for TKN are reported for CWs [16]. Our results are on the same order for COD (while assuming a ratio of 0.25 for BOD₅/COD). High values obtained for TKN kinetics are probably a consequence of the favourable conditions (high temperatures, plant activities) during the experiment.

| Table 2: Simulation results of hydraulic models (* Pearson correlation). |
|---------------------|---------------------|---------------------|---------------------|
|                      | PFD model           | TLM Visim model     |
|                      | D (−)               | τₚFD (day)          | R²* Ratio in layer  |
|                      |                      |                     | 1 (G) Time delay    |
| R1                   | 0.14                | 4.4                 | 97.1 0.7            |
| R2                   | 0.25                | 3.4                 | 98.7 0.6            |
| C1                   | 0.3                 | 3                   | 97.8 0.6            |
| C2                   | 0.27                | 3.2                 | 95.4 0.6            |

Figure 2: Treatment performances during the 30-day test.
Figure 3: Response curves of the different pilots.

Figure 4: Conceptualized two-layer model (TLM) with results from R1.
Simulation results were closer to experimental data when using the TLM, but care should be taken when interpreting the correlation coefficients obtained. Simulation with PDF model ($R^2 = 0.46$ for COD and 0.33 for TKN) seemed to give inferior results than simulation with TLM model ($R^2 = 0.94$ for COD and 0.71 for TKN). The only input in the PDF model was the Peclet number while the TLM model counted two inputs, the G ratio and the total delay (Td), which led to a more accurate determination of performances. On the other hand, the TLM enabled a better comprehension of flow and removal gradient in mesocosms. The ratio “G” used in the TLM model was proportional to ET magnitude and the time delay increased with high ET (Table 2).

The Damköhler number ($Da = k \cdot \tau$) is the normalised first order reaction rate constant and is defined as the ratio of the degradation rate to the mass transfer rate. A correlation between ET and Da values for TKN removal was underlined for all cases except pilots R3 and R4 (Figure 5). This suggested that ET enhanced the degradation rates. We hypothesised that the first effect of ET was to concentrate effluent, thus enhancing degradation rates (especially for TKN). Another contribution of ET could have been the amplification of gas transfer in aerenchyma, thus enhancing oxygen supply in the rhizosphere.

4. Conclusion

A positive contribution of peat on plant biomass development and consequently ET rates was observed. Effects of peat can also be related to those of large amounts of accumulated organic matter that can be found in old constructed wetlands. Thus adding peat in young CWs represents a clear improvement for plant establishment and can increase treatment performances for TKN.

In our study, the effects of ET were not clearly observed in hydraulic behavior by modeling the different mesocosms. No effect of ET on the dispersion coefficient was observed when using the plug flow with axial dispersion model. This was probably due to the small size of the mesocosms which led to a permanent bypass along the wall.

There was no clear difference between Phragmites and Typha effect on ET rates. The major factor increasing the ET was most likely the amount of plant biomass. Effect of ET was beneficial to TKN removal by increasing HRT. In temperate countries, favoring ET (building CWs well exposed to sun light) represents a clear increase on treatment performances, especially TKN. Effects of peat and of large ET on hydrodynamics of full scale CWs have to be measured to confirm those results.

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