Optimization of Process Parameters for $\varepsilon$-Polylysine Production by Response Surface Methods

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$\varepsilon$-Polylysine ($\varepsilon$-PL) is a highly safe natural food preservative with a broad antimicrobial spectrum, excellent corrosion resistances, and good commercial potentials. In the present work, we evaluated the $\varepsilon$-PL adsorption performances and conditions of various ion exchange resins by single-factor test, response surface method, and orthogonal design. The complexes of resin and $\varepsilon$-PL were characterized by SEM and FTIR. The results indicated that D155 resin had the best $\varepsilon$-PL adsorption performance and was selected for the separation and purification of $\varepsilon$-PL. The conditions for the static adsorption of $\varepsilon$-PL on D155 resin were optimized as follows: $\varepsilon$-PL solution 40 g/L, pH 8.5, resins 15 g/L, and absorption time 14 h. The adsorption efficiency of $\varepsilon$-PL under the optimal conditions was 96.84%. The $\varepsilon$-PL adsorbed on the D155 resin was easily desorbed with 0.4 mol/L HCl at 30°C in 10 h. The highest desorption efficiency was 97.57% and the overall recovery of $\varepsilon$-PL was 94.49% under the optimal conditions. The excellent $\varepsilon$-PL adsorption and desorption properties of D155 resin including high selectivity and adsorption capacity, easy desorption, and high stability make it a good candidate for the isolation of $\varepsilon$-PL from fermentation broths.

1. Introduction

Natural preservatives are promising food preservatives and have become a major research field worldwide in the recent years. $\varepsilon$-Polylysine ($\varepsilon$-PL) is a polypeptide containing 25 to 30 lysine residues and usually synthesized with Streptomyces [1]. It is one of highly safe natural food preservatives with a broad antimicrobial spectrum, excellent corrosion resistances, and commercial potentials [2–4]. $\varepsilon$-PL can inhibit the growth of Gram-negative bacteria, yeast, and mold in the neutral and acidic environment, especially, for E. coli and Salmonella that cannot be effectively inhibited by other natural preservatives [5–8]. Therefore, it is highly valuable and has a very promising market prospect. Most researches have been focused on breeding high-yield $\varepsilon$-PL strains and optimizing fermentation process to improve $\varepsilon$-PL yields [9, 10]. With the development of fermentation techniques, the extraction and purification of $\varepsilon$-PL in industrial production have become another research focus to lower production cost and improve product quality [11].

Ion exchange and ultra-filtration are two most widely used techniques for $\varepsilon$-PL separation [12]. Ion exchange technique has a great potential in isolation of active components from fermentation broth due to its short process, high recovery, and less pollution and has been extensively used in water treatment [13, 14] and extraction of active components from various media [14–18]. $\varepsilon$-PL is a cationic polymer at pH < pI (9.0) and can be absorbed by cation exchange resin.

In the present work, the $\varepsilon$-PL adsorption performances and conditions of various ion exchange resins were evaluated by single-factor test. The adsorption conditions of $\varepsilon$-PL on the resins were optimized by response surface method. The desorption of $\varepsilon$-PL was optimized with the desorption efficiency by single-factor test and orthogonal array test. Based on the results, an optimum extraction process of $\varepsilon$-PL was proposed.

2. Experimental

2.1. Materials. H⁺ resins HZD-5, HD-2, HZD-3B, D113, and D155 were provided by Shanghai Huazheng Technology Co.,
Ltd. (Shanghai, China), and were pretreated according to the manufacture’s manual. All other reagents were of analytical grade. ε-PL was a gift from Yiming Biological Co. Ltd. (Jiangsu, China).

2.2. Determination of Adsorption and Desorption Efficiency. Based on the method reported by Itzhaki et al. [18], the adsorption amount, adsorption efficiency, and desorption efficiency were calculated as follows:

\[ Q_e = \frac{(C_0 - C_1)V_0}{m}, \]
\[ A_r = \frac{C_0 - C_1}{C_0} \times 100\%, \]
\[ D_r = \frac{C_2V_2}{C_0V_0-C_1V_1} \times 100\% = \frac{C_2V_2}{mQ_e} \times 100\%, \]
\[ Y = A_r \times D_r, \]

where \( C_0 \) is the initial concentration of ε-PL (g/L); \( C_1 \) is the ε-PL concentration in the adsorption solution (g/L); \( C_2 \) is the ε-PL concentration in the eluent (g/L); \( V_0 \) is the volume of the initial ε-PL solution (ml); \( V_1 \) is the volume of ε-PL solution after adsorption (ml); \( V_2 \) is the volume of the eluent (ml); \( m \) is the weight of resin (g); \( Q_e \) is the absorbed amount of ε-PL (mg/g); \( A_r \) is adsorption efficiency; \( D_r \) is the desorption efficiency; and \( Y \) is the total recovery.

2.3. Univariate Analysis of ε-PL Adsorption

2.3.1. Effects of pH on ε-PL Adsorption. Five resins were pretreated and, respectively, divided into eight portions of 1 g resin. ε-PL solutions (20 mL 40 g/L) with pH = 2, 3, 4, 5, 6, 7, 8, and 9 were added to the eight aliquots of each resin and allowed a 10 h adsorption at 25°C under stirring at 200 r/min. The concentrations of ε-PL that remained in the solutions were then measured.

2.3.2. Effects of Resin Dosage on ε-PL Adsorption. ε-PL solutions (20 mL, 40 g/L, pH 8.5) were, respectively, added to 0.5 g, 1 g, 1.5 g, and 2 g resins at 25°C and stirred at 200 r/min for 10 h. The concentrations of ε-PL that remained in the solutions were then measured.

2.3.3. Effects of Initial ε-PL Concentration on ε-PL Adsorption. Five portions of 1 g resins were, respectively, mixed with 20 mL 10 g/L, 20 g/L, 30 g/L, 40 g/L, and 50 g/L ε-PL solutions (pH 8.5) at 25°C and stirred at 200 r/min for 10 h. The concentrations of ε-PL that remained in the solutions were then measured.

2.3.4. Effects of Adsorption Time on ε-PL Adsorption. Fifteen portions of 1 g resins were, respectively, added to fifteen 20 mL 40 g/L ε-PL solutions (pH = 8.5) at 25°C and stirred at 200 r/min for 1 h, 2 h, 3 h, 4 h, 5 h, 6 h, 7 h, 8 h, 9 h, 10 h, 11 h, 12 h, 13 h, 14 h, and 15 h, respectively. The concentrations of ε-PL that remained in the solutions were then measured.

2.4. Response Surface Analysis of the Static ε-PL Adsorption. Based on the univariate analysis results, the effects of ε-PL concentration, initial pH, resin dosage, and adsorption time on the ε-PL adsorption of HZD-3B and DI55 resins were determined with 29 cycles of a response surface design of four factors and three levels using adsorption efficiency as the index. The regression analysis of the data was conducted with Design-Expert v8.0.6 software. The four factors and three levels of the response surface design are shown in Table 1.

2.5. Single-Factor Test of Static Desorption of ε-PL

2.5.1. Effects of HCl Concentration. After being rinsed with three volumes of deionized water, ten portions of ε-PL adsorbed resins were, respectively, mixed with 20 mL 0.1, 0.2, 0.3, 0.4, 0.5, 0.6, 0.7, 0.8, 0.9, and 1.0 mol/L HCl solutions at 25°C and stirred for 200 r/min for 6 h. The ε-PL concentrations in the HCl solutions were measured.

2.5.2. Effects of Desorption Temperature. After being rinsed with three volumes of deionized water, ε-PL adsorbed resins were mixed with 20 mL 0.5 mol/L HCl solutions at 25°C and stirred for 200 r/min for 1 h–12 h. The ε-PL concentrations in the HCl solutions were measured.

2.5.3. Effects of Desorption Temperature. After being rinsed with three volumes of deionized water, the ε-PL adsorbed resins were mixed with 20 mL 0.5 mol/L HCl solutions at 15°C, 20°C, 25°C, 30°C, 35°C, and 40°C, respectively, and stirred at 200 r/min for 6 h. The ε-PL concentrations in the HCl solutions were then measured.

2.6. Orthogonal Array Test of the Static Desorption of ε-PL. Based on the single-factor test results, the effects of HCl concentration, desorption time, and desorption temperature on the desorption efficiency of ε-PL from HZD-3B and DI55 resins were evaluated by the orthogonal array test with three factors and three levels. The factors and levels for \( L_9(3^3) \) orthogonal test of the resins are shown in Table 2.

2.7. Data Analysis. All tests were repeated three times and the mean ± SD values were reported. \( t \)-test was used to determine the statistical significance. \( p < 0.05 \) was considered as statistical significance.

2.8. Apparatus. Fourier Transform Infrared Spectroscopy (FTIR) was performed on a Thermo-Fisher Nicolet FT-IR...
3. Results and Discussion

3.1. Optimization of Static Adsorption of e-PL by Single-Factor Test. Ion exchange resins have been widely applied for the high efficiency extraction of bioproducts, especially proteins and polypeptides, from fermentation broth in the form of chromatography [19]. Ion exchange resins can be divided into two types: cation and anion exchange resins. Based on their acidities, cation resins can be classified into strong acid and weak acid cation exchange resins. e-PL is a weak alkaline homopolymer composed of 25–30 L-lysine residues linked by the peptide bond between carboxyl and e-amino groups of L-lysine [19–22] and carries a number of positive charges in a specific pH range. Therefore, in the present work, five cation exchange resins were selected to isolate e-PL from the fermentation broth of Streptomyces sp. Ion exchange chromatography is usually conducted with fixed-bed columns. However, e-PL aqueous solution has a high viscosity due to the unique structure of e-PL, which causes long isolation process with fixed-bed columns. Therefore, dynamic adsorption separation is suitable to e-PL. In the present work, the batch static adsorption and desorption were conducted to evaluate the e-PL adsorption and desorption properties of the ion exchange resins.

3.1.1. Effects of pH. e-PL is amphoteric and has an isoelectric point (IP) at ~9.0 [23]. Therefore, pH can affect e-PL adsorption affinity on resins by alternating the ionization of e-PL [24]. e-PL is polyvalent cation at pH lower than 9.0 and is decomposed at pH higher than 9 [25, 26]. Therefore, the adsorption of e-PL on resins in the pH range of 2–9 was investigated. Figure 1(a) shows the increases in the adsorption efficiencies of e-PL on all five resins with the increase of pH in the test range, consistent with the conclusion reported by Zhang et al. [27]. The highest e-PL adsorption efficiencies of five resins were obtained at pH 9 with values of 41.58% for resin D113, 57.48% for resin HDZ-5, 69.55% for resin HD-2, 78.60% for D155 resin, and 84.71% for HDZ-3B resin. HDZ-3B and D155 showed higher e-PL adsorption capacities and D113 had the lowest e-PL adsorption capacity.

3.1.2. Effects of Resin Dosage. The effects of resin dosage on the e-PL adsorption efficiency are illustrated in Figure 1(b). As can be seen, the e-PL adsorption efficiencies of all resins increased with the increase of resin dosage. It can be explained that more resins provided more exchangeable sites for e-PL, resulting in higher adsorption efficiency. The e-PL adsorption efficiencies of HDZ-3B and D155 resins were dramatically increased as the resin dosage increased from 2.5 g/L to 7.5 g/L and slightly increased with the increase of resin dosage from 7.5 g/L to 10 g/L. The e-PL adsorption efficiencies of other three resins were gradually increased with the increase of the adsorbent dosage. The highest adsorption efficiencies were found in 10 g/L D155 and HDZ-3B resins with values of 92.63% and 95.23%, respectively.

3.1.3. Effects of Initial e-PL Concentration. As shown in Figure 1(c), the e-PL adsorption efficiency of the resins rapidly increased as the initial e-PL concentration increased from 10 g/L to 20 g/L. It can be explained that large amounts of e-PL at high concentrations rapidly adsorbed on the resins and consequently saturated the resins. As the e-PL concentration further increased from 20 g/L to 40 g/L, the adsorption efficiency was gradually increased and the maximum adsorption capacity of the resins was reached. Further increasing initial e-PL concentration from 40 g/L to 50 g/L led to a slight decline in the e-PL adsorption efficiency. The e-PL adsorption efficiencies of all five resins were obtained in 40 g/L e-PL solution with values of 33.27% for D113 resin, 59.77% for HDZ-5 resin, 67.77% for HD-2 resin, 81.7% for D155 resin, and 83.98% for HDZ-3B resin. Therefore, initial e-PL concentration was optimized as 40 g/L. In addition, both HDZ-3B and D155 resins showed higher e-PL adsorption capacities and D113 resin had the lowest e-PL adsorption capacity under the optimized conditions.

3.1.4. Effects of Adsorption Time. Based on their locations in resins, the adsorption sites are classified into two types: the sites on the surfaces of the resins and the sites in intraresin. The adsorption rates of these two types of sites are different. The adsorbate is rapidly absorbed by the sites on resin surface. In contrast, the adsorbate needs to diffuse into the intraparticle of the resins before being absorbed by the sites in the intraresin [28]. The diffusion to the intraparticle is a slow adsorption process subjected to fast adsorption stage, slow adsorption stage, and equilibrium stage [29–31]. As shown in Figure 1(d) for the e-PL adsorption efficiency-time curves of the resins (Figure 1(d)), the e-PL adsorption on all five resins was subjected to three stages with the extension of adsorption time as described above. At the first stage (0–7 h), e-PL rapidly adsorbed on the resins and the adsorption efficiency linearly increased with the adsorption time. At this stage, the ion exchange adsorption occurred between e-PL molecules and the ion exchange sites on the surface of resins. The adsorption became slower at the second stage from 7 h to 12 h. During this stage, e-PL diffused into the interior of resins, adsorbed on the ion exchange sites within the resins and retained in the interior of the resin. Thereafter, during the third stage (after 12 h), the adsorption reached an equilibrium. All ion exchange sites in the resin were saturated and no ion exchange adsorption occurred. The highest adsorption efficiencies on the resins were reached at 12 h with values of 40.46% for D113 resin, 61.94% for HDZ-5 resin, 73% for HD-2 resin, 87.67% for...
D155 resin, and 90.99% for HZD-3B resin. Similarly, HZD-3B and D155 resins showed higher $\varepsilon$-PL adsorption capacities and D113 resin showed lowest adsorption capacity under the testing conditions.

In all, the single-factor tests indicate that all five resins can absorb $\varepsilon$-PL with different adsorption capacities. HZD-3B and D155 resins had higher $\varepsilon$-PL adsorption capacities, followed by HD-2 and HZD-5 resins. D113 resin showed lowest adsorption capacity. Therefore, HZD-3B and D155 resins were selected to further optimize the $\varepsilon$-PL adsorption conditions by response surface method in the following experiments.

3.2. Optimization of the Static Adsorption of $\varepsilon$-PL by Response Surface Method. Based on single-factor tests of the $\varepsilon$-PL adsorption of HZD-3B and D155 resins, pH, resin dosage, initial concentration of $\varepsilon$-PL solution, and adsorption time were selected as independent variables and the adsorption efficiency was used as a dependent variable to further optimize the $\varepsilon$-PL adsorption conditions using Box-Behnken design principle with four factors, three levels, and a total of 29 experiments. Three levels were coded as $-1$, $0$, and $+1$, respectively [32]. The experimental design and results are shown in Table S1 (see Supplementary Material available online at http://dx.doi.org/10.1155/2016/3785036). The variance analysis of the data was conducted in Design-Expert v8.0.6 software (Table S2).

Regression analysis of the test results was conducted in Design-Expert v8.0.6 software. The fitting quadratic polynomial regression equations are as follows.

For HZD-3B resin,

$$Y = 93.15 + 1.99X_1 + 3.89X_2 + 2.03X_3 + 9.09X_4 + 3.21X_2X_3 - 3.05X_2^2 - 8.51X_4^2. \quad (2)$$
For D155 resin,

\[ Y = 93.43 + 4.05X_2 - 3.25X_1X_2 + 6.26X_2X_3 - 4.44X_2^2 - 3.01X_3^2, \]

where \( Y \) is the index value (adsorption efficiency) and \( X_1, X_2, \) \( X_3, \) and \( X_4 \) represent pH, resin dosage, initial concentration, and adsorption time, respectively.

The \( R^2 \) values of the modeling analysis of HZD-3B and D155 resins are 0.9390 and 0.8914, respectively, indicating that the model can fit experimental data well. The high coefficient of determination also suggests a strong correlation between the experimental values and the predicted values in the two models [33]. The regression equation can be used to optimize four parameters in the adsorption process of \( \epsilon-PL \). Both models showed the lack-of-fit \( p > 0.05 \), indicating that the regression equation was highly reliable and credible and the experimental error could be negligible. Therefore, the two models can be used to determine the relationship between the independent variables and dependent variables [34]. The quadratic regression equation was able to precisely predict the theoretical value of dependent variable, indicating that the model successfully analyzed and optimized the experimental results.

### 3.3. Variance Analysis of the \( \epsilon-PL \) Adsorption on HZD-3B Resin by Response Surface Method

Both resin dosage and initial \( \epsilon-PL \) concentration significantly affected the adsorption of \( \epsilon-PL \) on HZD-3B resin (Table S2). The effects of resin dosage-pH and initial \( \epsilon-PL \) concentration-resin dosage on the \( \epsilon-PL \) adsorption of D155 resin reached significant and extremely significant levels, respectively. The response surface plots of the interactions between various factors on the dependent variable (\( \epsilon-PL \) adsorption efficiency) were determined and Figure 2 shows the response surface plots of the factors that significantly affected \( \epsilon-PL \) adsorption. Steep surfaces indicate more significant effects and flat surfaces represent weaker effects of the factors. Denser contours indicate greater impacts of the factors on the \( \epsilon-PL \) adsorption efficiency and vice versa. The contour shape reflects the strength of the interaction between two factors. The circular contours represent weak interactions and less significant effects and oval contours indicate strong interactions and more significant effects.

Based on these results the following can be concluded. (1) The \( \epsilon-PL \) adsorption conditions of HZD-3B resin were determined by the response surface method as initial \( \epsilon-PL \) concentration 40 g/L, resin dosage 15 g/L, pH 8.65, and adsorption time 12.8 h. The \( \epsilon-PL \) adsorption efficiency could reach 99.49% under the optimal conditions. Considering the practical operation process, we proposed the practical optimum adsorption conditions as initial \( \epsilon-PL \) concentration 40 g/L, resin dosage 15 g/L, pH 8.5, and adsorption time 13 h. The experimental \( \epsilon-PL \) adsorption efficiency was 97.69% under the proposed conditions, consistent with the response surface results. (2) The optimal \( \epsilon-PL \) adsorption conditions of D155 resin were determined by the response surface method as initial \( \epsilon-PL \) concentration 37.94 g/L, resin dosage 2.85 g/L, pH 8.04, and adsorption time 13.76 h. The \( \epsilon-PL \) adsorption efficiency can reach 99.48%. The corrected practical adsorption operation conditions are initial \( \epsilon-PL \) concentration 40 g/L, resin dosage 3.0 g, pH 8, and adsorption time 14 h. The experimental \( \epsilon-PL \) adsorption efficiency under the optimal operation conditions was 96.84%, consistent with the response surface analysis result. These results indicate the model is reliable.

### 3.4. Morphologies of D155 and HZD-3B Resins

Figure 3 shows the SEM images of D155 and HZD-3B resins before and after \( \epsilon-PL \) adsorbed. Both resins displayed a plicate and porous surface structure. D155 resin possessed large, deep, and sparse pores with a nearly network structure, while HZD-3B resin contained small, shallow, and dense pores (Figures 3(a) and 3(c)). Their porous structure provided more adsorption sites and increased the contact area and diffusion of \( \epsilon-PL \) in the resins during the adsorption. The SEM images of the resins after the adsorption indicated that the \( \epsilon-PL \) molecules were trapped and adsorbed into the pores and surfaces of resins (Figures 3(b) and 3(d)). The \( \epsilon-PL \) layer adsorbed on D155 resin surface was uniform and thin and that adsorbed on the surface of HZD-3B resin surface was dense and thick.

### 3.5. Infrared Spectra Analysis before and after \( \epsilon-PL \) Adsorption

\( \epsilon-PL \) is a polyamide compound and can be easily identified by its characteristic IR absorption peaks. As can be seen from Figure 4, both resins showed similar characteristic IR spectra after the \( \epsilon-PL \) adsorption. The characteristic absorption bands at ~1674.3 cm\(^{-1}\) were attributed to the stretching vibration band of C=O in amide groups (amide absorption band I). The absorption peak at 1570.1 cm\(^{-1}\) was assigned to bending vibration of -NH group and stretching vibration of -CN group (amide absorption band II). These two amide absorption bands confirmed the existence of amide groups. The absorption bands at 3270 cm\(^{-1}\) and 3099 cm\(^{-1}\) were attributed to the Fermi resonance generated from the frequency multiplication of the amide absorption band II and the stretching vibration of -NH group, respectively. The peaks at 3431.3 cm\(^{-1}\) and 2944.6 cm\(^{-1}\) were ascribed to the asymmetric stretching of -NH\(_2\) group and stretching of saturated C-H bond, respectively. The peaks at 1461.5 cm\(^{-1}\) and 1436.4 cm\(^{-1}\) were due to CH\(_3\) groups. These results suggest that \( \epsilon-PL \) was absorbed on the resin.

### 3.6. Optimization of Static Desorption of \( \epsilon-PL \) by Single-Factor Test

The \( \epsilon-PL \) adsorbed on the resin can be desorbed with NaOH, NH\(_2\)OH, sodium salt, ammonium salt, and acids. However, the pHs of both NaOH and NH\(_2\)OH eluents are higher than 9.0, which can cause the degradation of \( \epsilon-PL \) [25, 26]. In addition, the high concentrations of salts in the eluents need to be removed to obtain high purity of \( \epsilon-PL \). Acids, especially HCl, for \( \epsilon-PL \) desorption, can avoid the decomposition of \( \epsilon-PL \) and be removed simply by evaporation under reduced pressure. Therefore, HCl was used to desorb \( \epsilon-PL \) from the resins in the present work.
3.6.1. Effects of HCl Concentration. The $\varepsilon$-PL desorption from resins by HCl follows the ion exchange equation:

$$H^+ + \varepsilon$-PL-resin $\rightleftharpoons \varepsilon$-PL$^+$ + H-resin (4)$$

Therefore, high concentration of HCl is in favor of the $\varepsilon$-PL desorption. However, excessive HCl can increase the production cost and corrode equipment. Hence, the HCl concentration for the $\varepsilon$-PL desorption was first optimized. The $\varepsilon$-PL desorption was conducted in HCl solutions at concentrations ranging from 0.1 to 1.0 mol/L at 25°C for 6 h. As shown in Figures 5(a) and 5(b), the $\varepsilon$-PL desorption efficiency increased with the increase of HCl concentration and peaked at HCl concentration of 0.4 mol/L with values of 83.67% for rHZD-3B resin and 92.88% for D155 resin. Further increasing HCl concentration led to a decline in desorption efficiency. Therefore, 0.4 mol/L HCl was used for $\varepsilon$-PL desorption from the resins.

3.6.2. Effects of Desorption Time. The $\varepsilon$-PL desorption from the resins was conducted in 0.5 mol/L HCl at 25°C for various periods of time. As shown in Figures 5(c) and 5(d), the $\varepsilon$-PL desorption efficiencies of HZD-3B and D155 resins increased from 1 h to 8 h and reached 62.48% and 83.86%, respectively.
Further extending desorption time showed no significant effect on the \( \varepsilon \)-PL desorption efficiency. The desorption time was then optimized as 8 h.

3.6.3 Effects of Desorption Temperature. It has been reported that temperature can significantly influence the equilibrium reaction of ion exchange [35]. The \( \varepsilon \)-PL desorption was conducted in 0.5 mol/L HCL at various temperatures for 6 h. No significant effects of temperature on the \( \varepsilon \)-PL desorption were observed (Figures 5(e) and 5(f)). The desorption efficiencies of both HZD-3B and D155 resins increased slightly as the temperature increased from 15°C to 30°C and reached
81.64% and 57.59%, at 30°C, respectively. Further increasing desorption temperature led to a slight decrease in desorption efficiency.

3.7. Optimization of Static Desorption of e-PL by Orthogonal Array Test. Orthogonal array test has been successfully used in the optimization of bioproduct extractions from fermentation broths and other plant materials [36–38]. In the present study, based on the single-factor analysis results, a $L_9(3^4)$ orthogonal array composed of 16 run, 4 factors, and 3 levels was used to optimize desorption conditions of e-PL from resins. HCl concentration ($A$), desorption time ($B$),
Table 3: Factors and levels in $L_9(3^3)$ orthogonal array and desorption efficiencies in different media.

<table>
<thead>
<tr>
<th>Run</th>
<th>Factor and level</th>
<th>Desorption rate (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>$k_1$</td>
<td>$k_2$</td>
</tr>
<tr>
<td>1</td>
<td>1</td>
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</tr>
<tr>
<td>2</td>
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<tr>
<td>9</td>
<td>3</td>
<td>3</td>
</tr>
</tbody>
</table>

Table 4: The analysis of orthogonal extremum. $k_1$, $k_2$, and $k_3$ are the average values of three levels. $R$ is the difference between extremums.

<table>
<thead>
<tr>
<th>Level</th>
<th>$k_1$</th>
<th>$k_2$</th>
<th>$k_3$</th>
<th>$R$</th>
<th>Optimum level</th>
</tr>
</thead>
<tbody>
<tr>
<td>$k_1$</td>
<td>75.26</td>
<td>81.97</td>
<td>81.15</td>
<td>65.40</td>
<td>$A &gt; C &gt; B$</td>
</tr>
<tr>
<td>$k_2$</td>
<td>86.67</td>
<td>81.84</td>
<td>81.86</td>
<td>86.94</td>
<td>$A &gt; C &gt; B$</td>
</tr>
<tr>
<td>$k_3$</td>
<td>84.08</td>
<td>82.21</td>
<td>83.01</td>
<td>95.50</td>
<td>$A &gt; C &gt; B$</td>
</tr>
<tr>
<td>$R$</td>
<td>11.41</td>
<td>0.37</td>
<td>1.86</td>
<td>30.10</td>
<td>$A &gt; C &gt; B$</td>
</tr>
</tbody>
</table>

and desorption temperature (C) were used as the processing factors and desorption rate of $\varepsilon$-PL was used as the evaluation indicator (Table 3).

The influences of the processing variables on the indicators were determined using range (R) analysis (Table 4) and ANOVA (Table S3). The statistical significances of the effects of the factors on the $\varepsilon$-PL desorption from both HZD-3B and D155 resins were in the order of $A$ (HCL concentration) $> C$ (adsorption temperature) $> B$ (adsorption time). F-test was then used to determine, at a specific confidence level, whether these factors had significant effects on the $\varepsilon$-PL desorption efficiency of resins. Higher F-values indicate more significant effects of the factors. The F-test of the variances of the orthogonal array showed that the only factors $A$ (HCL concentration) and $C$ (adsorption temperature) were significant ($p < 0.05$) for $\varepsilon$-PL desorption efficiency (Table S3) and factor $B$ (adsorption time) was insignificant ($p > 0.05$) for the $\varepsilon$-PL desorption efficiency. The $\varepsilon$-PL adsorption conditions for HZD-3B resin were optimized as $A_3B_1C_3$, for example, 0.4 mol/L HCL, desorption time 8 h and desorption temperature 30°C. The optimal $\varepsilon$-PL desorption conditions of D155 resin were determined as $A_3B_3C_3$, for example, 0.4 mol/L HCL, desorption time 10 h, and desorption temperature 30°C. Under the optimal conditions, the experimental $\varepsilon$-PL desorption efficiencies of HZD-3B and D155 resins were 87.98% and 97.57%, respectively, indicating that the desorption conditions optimized by the orthogonal array test were reliable.

3.8 $\varepsilon$-PL Adsorption and Desorption Performances of HZD-3B and D155 Resins. Table 5 shows the $\varepsilon$-PL adsorption and desorption performances of HZD-3B and D155 resins. Both HZD-3B and D155 resins showed good adsorption capacities with $\varepsilon$-PL adsorption efficiencies of 97.69% and 96.84%, respectively. Their desorption efficiencies were 87.98% and 97.57%, respectively, under the optimal conditions, which, respectively, resulted in 85.95% and 94.49% $\varepsilon$-PL recoveries.

As can be seen, D155 resin is a better option for $\varepsilon$-PL extraction and purification. D155 resin is a macroporous weak acid resin made with a novel polymeric material containing a functional group (-COOH) [39]. The proton can exchange with a cation, and the oxygen atom can coordinate directly with cations, which results in the high sorption capacity, easy regeneration, and convenient operation of the resin [39]. In all, D155 resin is an effective resin for $\varepsilon$-PL sorption.

### Table 5: The static $\varepsilon$-PL adsorption capacity and elution ratios of HZD-3B and D155 resins.

<table>
<thead>
<tr>
<th>Resin</th>
<th>Adsorption amount (mg/g)</th>
<th>Adsorption rate (%)</th>
<th>Desorption rate (%)</th>
<th>The total recovery rate (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>HZD-3B</td>
<td>260.51</td>
<td>97.69</td>
<td>97.57</td>
<td>85.95</td>
</tr>
<tr>
<td>D155</td>
<td>258.24</td>
<td>96.84</td>
<td>97.57</td>
<td>94.49</td>
</tr>
</tbody>
</table>

### 4. Conclusion

Among the five test resins, HZD-3B and D155 resins showed better adsorption performances. The $\varepsilon$-PL adsorption conditions of HZD-3B resin were optimized as initial $\varepsilon$-PL concentration 40 g/L, pH 8.5, resin dosage 15 g/L, and adsorption time 13 h. The maximum $\varepsilon$-PL adsorption efficiency was 97.69% under the optimal condition. The $\varepsilon$-PL adsorption conditions of D155 resin were optimized as initial $\varepsilon$-PL concentration 40 g/L, pH of 8.5, resin dosage 15 g/L, and adsorption time 14 h. The maximum $\varepsilon$-PL adsorption efficiency was 96.84% under the optimal condition.

HZD-3B and D155 resins showed the similar variation tendency in ultrastructural surface and infrared spectroscopy before and after the $\varepsilon$-PL adsorption.

The $\varepsilon$-PL desorption conditions of HZD-3B resin were optimized as 0.4 mol/L HCl, desorption time 8 h and desorption temperature 30°C, which resulted in a $\varepsilon$-PL desorption efficiency of 87.98%. Similar desorption conditions were optimized for D155 resin except a longer desorption time of 10 h. The $\varepsilon$-PL desorption efficiency under the optimal conditions was 97.57%. D155 resin gave higher $\varepsilon$-PL recovery, indicating it is a better ion exchange resin for $\varepsilon$-PL extraction.

### Abbreviations

$\varepsilon$-PL: $\varepsilon$-Polylysine.

### Competing Interests

The authors declare that they have no competing interests.
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