

Research Article

Kinetic Study of Acid Hydrolysis of Rice Straw

Nibedita Sarkar and Kaustav Aikat

Department of Biotechnology, National Institute of Technology, Mahatma Gandhi Avenue, Durgapur 713209, India

Correspondence should be addressed to Kaustav Aikat; kaustav.aikat@bt.nitdgp.ac.in

Received 7 November 2012; Accepted 23 November 2012

Academic Editors: K. R. Davis, G. Garrote, and J. C. Merchuk

Copyright © 2013 N. Sarkar and K. Aikat. This is an open access article distributed under the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited.

Rice straw is a renewable, cheap, and abundant waste in tropical countries. The pentose content of rice straw can be used as a substrate for many types of value-added products such as xylitol and biofuel. Dilute acid hydrolysis mainly releases pentose from rice straw. The objective of the study was to determine the effect of H_2SO_4 concentration and reaction time on the xylose production. The variation of the main product xylose with the reaction time was described by a kinetic model and kinetic parameters were calculated to describe the variation of the xylose production with time. The optimum yield (19.35 g/L) was obtained at 0.24 mol/L H_2SO_4 and 30 minutes.

1. Introduction

Rice straw is one of the most abundant agricultural wastes. For instance, approximately 731 million tons per year rice straw is produced globally (Africa: 20.9 million tons, Asia: 667.6 million tons, Europe: 3.9 million tons, America: 37.2 million tons, and Oceania: 1.7 million tons) [1]. Nearly 600 million tons of agricultural residues are produced by India annually; out of which, approximately 300 million tons of it remain unused.

The options for the disposal of rice straw are limited by the great bulk of material, slow degradation in the soil, harboring of rice stem diseases, and high mineral content. Though rice straw is used as animal feed and soil fertilizer, the utilization ratio remains low compared to other straws. Rice straw has low digestibility value as animal feed. Although rice straws contain materials for social benefit, their apparent value is less than the cost of collection, transportation, and processing for beneficial use. Open-field burning is a major practice for rice straw disposal. It causes air pollution, a threat to human health [2]. Rice straw contains 19–27% of hemicellulose, a heteropolymer composed mainly of xylose followed by arabinose [3, 4]. The hemicellulosic and cellulosic contents of rice straw can be hydrolyzed chemically or enzymatically. Chemical hydrolysis includes dilute sulfuric acid hydrolysis that can be used for either the pretreatment before enzymatic hydrolysis or the conversion of hemicellulose to pentose

[5] remaining cellulose and lignin fractions being almost unaltered. Lignocellulosic structure as well as hydrolysis reactions of sugar polymers in a dilute acid medium is very complicated. The substrate is in the solid phase and the catalyst in the liquid phase. Various factors (particle size, liquid to solid ratio, type and concentration of acid used, temperature, and reaction time) influence monomer yield [6].

In the present work, the effect of acid concentration and reaction time on xylose production was studied and a kinetic model was developed to describe the variation of xylose production with time.

2. Materials and Methods

2.1. Rice Straw. Rice straw was used as raw material in the experiments. It was procured from Bankura, India. It was air-dried, ground, size fractioned to 0.5 mm, and stored at room temperature for subsequent experiments. Main components of rice straw such as cellulose, hemicellulose, and lignin were determined [7]. The composition of rice straw is shown in Table 1.

2.1.1. Cellulose Estimation. Acetic/nitric reagent (150 mL of 80% acetic acid and 15 mL of concentrated nitric acid) was added to 0.5 g sample and placed in a water bath at 100°C for 30 minutes. The mixture was cooled and centrifuged for

20 minutes. The supernatant was discarded and the residue was washed with distilled water and mixed with 10 mL of 67% H₂SO₄. Then it was allowed to stand for 1 hour at room temperature. The solution (1 mL) was diluted to 100 mL and to 1 mL of this diluted solution and 10 mL of freshly prepared anthrone reagent (0.2% anthrone in concentrated H₂SO₄) was added. The mixture was heated in a boiling water bath for 10 minutes and cooled. The color was measured at 630 nm. Cellulose powder (Hi Media, India) was used as a standard.

2.1.2. Hemicellulose Estimation. In a refluxing flask, 10 mL cold neutral detergent solution was added to 1 g powdered sample. The neutral detergent solution was prepared as follows. Disodium ethylenediamine tetraacetate (18.61 g) and sodium borate decahydrate (6.81 g) were dissolved in about 200 mL of distilled water by heating and to this, 100 mL solution containing sodium lauryl sulphate (30 g) and ethoxy ethanol (10 mL) was added. A solution (100 mL) of 4.5% Na₂HPO₄ was then added to the mixture. The final volume was made up to 1 L with distilled water and the pH adjusted to 7.

To the mixture of rice straw sample and cold neutral detergent solution, decahydronaphthalene (2 mL) and sodium sulphite (0.5 g) were added. Then the mixture was heated to boiling and refluxed for 1 h. The contents inside the refluxing flask were filtered through sintered glass crucible (G-2) followed by hot water washing. Finally two washings with acetone were given and the residue was transferred to a crucible. The sample was dried at 100°C for 8 h, cooled in a desiccator, and weighed. The residue was designated as neutral detergent fiber (NDF). The amount of acid detergent fiber (ADF) was subtracted from the amount of neutral detergent fiber (NDF) for the calculation of hemicellulose content. The acid detergent fiber (ADF) was prepared by the following method.

100 mL acid detergent solution (2% cetyl trimethyl ammonium bromide in 1 N sulphuric acid) was added to the powdered sample which was placed in a round bottom flask. The sample was heated to boil in 5–10 minutes and refluxed for 1 h after the onset of boiling. The boiling was adjusted to slow, even level. The contents were filtered through a preweighed sintered glass crucible (G-2) by suction and washed with hot water twice. The contents were washed with acetone until the filtrate was colorless. Then it was dried at 100°C for overnight, cooled in a desiccator, and weighed. The ADF content was expressed as a percentage, that is, $W/S \times 100$ where W was the weight of the fiber and S was the weight of the sample.

2.1.3. Lignin Estimation. 25 mL of 72% H₂SO₄ and 1 g asbestos were added to acid detergent fiber (ADF). The mixture was kept for 3 h at room temperature and intermittently stirred. After that the mixture was diluted and filtered with preweighed Whatman no. 1 filter paper. Then it was dried at 100°C, cooled in a desiccator and weighed. Then the filter paper was transferred to a preweighed silica crucible and kept in a muffle furnace at 550°C for 3 h. The crucible was cooled in a desiccator, and weighed for ash content

TABLE 1: Main components of rice straw.

Components	Percentage of dry weight
Cellulose	40.09 ± 0.02
Hemicellulose	26.8 ± 0.02
Lignin	18.9 ± 0.02

calculation. Asbestos was used as blank. The acid detergent lignin (Percentage of ADL) was determined using

$$\begin{aligned} &\text{Percentage of ADL} \\ &= \text{Weight } 72\% \text{ H}_2\text{SO}_4 \text{ washed fibre (test - asbestos blank)} \\ &\quad \times 100(\text{Weight of the sample})^{-1} \\ &\quad - \frac{\text{Ash (test - asbestos blank)} \times 100}{\text{Weight of the sample}}. \end{aligned} \quad (1)$$

2.2. Acid Hydrolysis. The basic method of acid hydrolysis of rice straw by diluted H₂SO₄ at 121°C and 15 psi was done as per Yoswathana et al., 2010 [8]. Rice straw (1 g) was treated with 10 mL of H₂SO₄ solution of various concentrations for different reaction times. At given time intervals, samples were withdrawn, cooled, and centrifuged at 12000 rpm for 15 minutes to separate out the water insoluble fraction. The supernatant was used for xylose assay. All the hydrolysis experiments were carried out in triplicate.

2.3. Analytical Methods

2.3.1. Xylose Estimation. Xylose content was determined using the phloroglucinol assay [9] with minor modifications. Briefly, the color reagent consisting of 0.5 g of phloroglucinol, 100 mL of glacial acetic acid, and 10 mL of conc. HCl was freshly prepared and used within 4 days. Stock of standard xylose solution (10 g/L) was prepared by dissolving D-xylose (Himedia, India) powder in saturated benzoic acid and used for preparation of the calibration curve. Fifty microliters of sample was mixed with 5 mL color reagent and subsequently heated at 100°C for 6 min. The reaction mixture was rapidly cooled down to room temperature in a water bath and the absorbance at 554 nm was recorded.

3. Results and Discussion

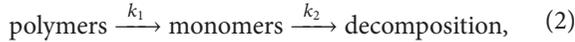
For acid hydrolysis, H₂SO₄ concentration was varied from 0.093 mol/L to 0.28 mol/L and reaction time was varied from 15 to 60 minutes. Xylose concentration obtained from the hydrolysate at various H₂SO₄ concentrations and reaction times is given in Table 2. It was observed that maximum xylose was released at 0.24 mol/L H₂SO₄ concentration and 30 minutes. Xylose concentration decreased with reaction time. This may be due to sugar decomposition and production of inhibitor. The level and composition of the sugar released depend on the type of the acid in the reaction

TABLE 2: Xylose (g/L) obtained from the rice straw hydrolysate at various H_2SO_4 concentrations and reaction times.

H_2SO_4 concentration (mol/L)	Time (min)			
	15	30	45	60
0.093	8.7	10.5	9.13	9.08
0.14	11.9	13.9	12.6	12
0.18	15.8	18.33	16.33	15.65
0.24	17.6	19.35	17.5	16.2
0.28	17.31	17.99	14.45	13.18

mixture [10] and acid treatment with H_2SO_4 mainly releases xylose [11].

The variation of the main product xylose with reaction time may be described by a kinetic model. Saeman, 1945 [12], proposed a simplified model for hydrolysis of lignocellulosic materials using pseudo-homogeneous irreversible first-order reactions [13, 14]. The model was used for hemicellulosic fraction [13]:



where k_1 and k_2 are the rate constants (min^{-1}) for generation and decomposition reaction, respectively.

Predicted model for concentration of monomers is given below by solving the differential equation [12]:

$$M = M_0 e^{-k_2 t} + P_0 \frac{k_1}{k_2 - k_1} (e^{-k_1 t} - e^{-k_2 t}), \quad (3)$$

where M is concentration of monomers (g/L), P is concentration of polymers (g/L), M_0 is initial monomer concentration ($= 0$), and t is reaction time.

Equation (3) is used for kinetic modeling of xylose concentration.

P_0 of (3) is calculated as follows:

$$P_0 = \frac{150 C_{Xn_0}}{132 \text{ WSR}} \times 10 = 23.4 \text{ g eq.xylose/L}, \quad (4)$$

where C_{Xn_0} initial xylan concentration was assumed as 20.6 g xylan per 100 g rice straw on dry basis [15]. WSR is the water/solid ratio and 150/132 is the ratio of the stoichiometric factors.

Aguilar et al. (2002) [13] modified (3) for better fitting of the experimental data to the kinetic model. The modified equation is given by

$$M = M_0 e^{-k_2 t} + \alpha P_0 \frac{k_1}{k_2 - k_1} (e^{-k_1 t} - e^{-k_2 t}). \quad (5)$$

α is the ratio between fractions (g of susceptible xylan/g of total xylan). The usual range of α is 0.5–1 g/g. Experimental data of xylose concentration in acid hydrolysate was fitted applying (5). The plots of predicted and experimental data of xylose concentration of each set are shown in Figure 1. The kinetic parameters of each set are given in Table 3. Values of correlation coefficient R^2 for each set were 0.99 which indicate the fitness of the model.

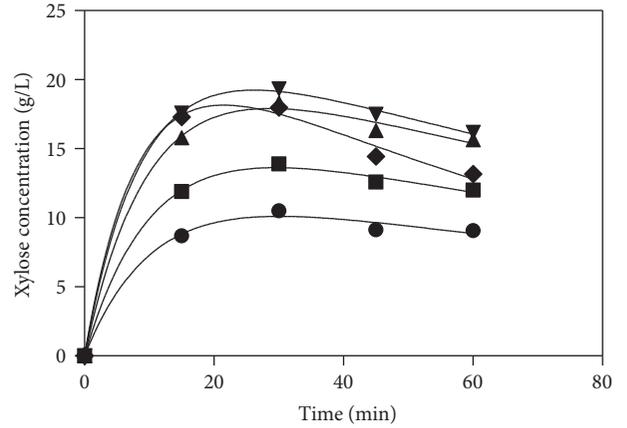


FIGURE 1: Experimental and predicted dependence of xylose concentration on time of various H_2SO_4 concentrations. (—) Saeman's model, (●) 0.093 mol/L, (■) 0.14 mol/L, (▲) 0.18 mol/L, (▼) 0.24 mol/L, and (◆) 0.28 mol/L.

Chi-square analysis of the experimental data at each H_2SO_4 concentration was carried out. The chi-square statistic test (χ^2) is the sum of the squares of the differences between the experimental data and predicted data obtained by calculating from models, with each squared difference divided by the corresponding predicted data obtained by calculating from models. The (χ^2) will be a small number if the experimental data and predicted data from the model are similar and vice versa. Therefore, the model that gives the smallest chi-square value is considered the best fit [16]:

$$\chi^2 = \sum \frac{(q_{e,\text{exp}} - q_{e,\text{cal}})^2}{q_{e,\text{cal}}}. \quad (6)$$

The range of the χ^2 value signifies the good fit of the model at each acid concentration (Table 4).

From Table 3, it is observed that α values varied from 0.528 to 0.999 depending on H_2SO_4 concentration. Values of α generally vary with operational conditions. Different α values ranging from 0.5 to 1 g/g have been reported [13].

Values of k_1 and k_2 values also increased with H_2SO_4 concentration and k_1 values were higher compared to k_2 values for each set. This indicates that generation rate is higher than degradation rate.

For zero initial monomer, rate of monomer formation dM/dt can be obtained by differentiating (5) and putting $M_0 = 0$:

$$\frac{dM}{dt} = \alpha P_0 \frac{k_1}{k_2 - k_1} (-k_1 e^{-k_1 t} + k_2 e^{-k_2 t}). \quad (7)$$

Now for heterogeneous solid-liquid noncatalytic reactions,

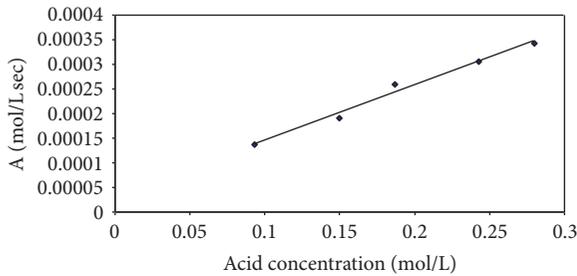
$$\frac{dM}{dt} = kFC, \quad (8)$$

TABLE 3: Kinetic parameters of xylose released from rice straw through H₂SO₄ hydrolysis.

H ₂ SO ₄ concentration (mol/L)	α (g/g)	k_1 (min ⁻¹) $\times 10^{-2}$	k_2 (min ⁻¹) $\times 10^{-3}$	R^2
0.093	0.528	9.4	6	0.993
0.14	0.714	9.6	6.8	0.998
0.18	0.936	9.9	7	0.9973
0.24	0.995	11.1	7.2	0.999
0.28	0.999	12	11.1	0.9958

TABLE 4: Chi-square analysis (χ^2) at each acid concentration.

H ₂ SO ₄ concentration (mol/L)	χ^2
0.093	0.067
0.14	0.018
0.18	0.035
0.24	0.0084
0.28	0.087

FIGURE 2: A plot of $\alpha P_0(k_1/(k_2 - k_1))(-k_1e^{-k_1t} + k_2e^{-k_2t})$ (denoted by "A") versus C (acid concentration).

where k is mass transfer constant, F is interfacial area, and C is acid concentration. Comparing (7) and (8), the following equation can be obtained:

$$kFC = \alpha P_0 \frac{k_1}{k_2 - k_1} (-k_1e^{-k_1t} + k_2e^{-k_2t}). \quad (9)$$

A plot of $\alpha P_0(k_1/(k_2 - k_1))(-k_1e^{-k_1t} + k_2e^{-k_2t})$ (denoted by "A") versus C (acid concentration) should give a straight line. The results obtained were in agreement with this as shown in Figure 2. Linear regression of (9) gave an R^2 of 0.98 assuming k and F to be nearly constant.

A short discussion of the practical utility of the present work may be relevant here. The optimized xylose production obtained in the present study (19.35 g/L) was higher than in previous reports [14, 17]. For this level of production at the laboratory scale, the raw material cost was computed to be approximately \$ 1.5 per kg xylose. This cost is quite low enough to indicate the economic feasibility of the process on the large scale.

Now acid hydrolysis breaks down mainly the hemicellulose component of rice straw to release the pentose, mainly xylose, in the hydrolysate. Acid hydrolysis can also bring about delignification of the straw to make the cellulosic component amenable to saccharification to release hexoses

such as glucose [15]. This saccharification may be carried out enzymatically or by second step acid hydrolysis [15]. Now the first step of acid hydrolysis cannot be prolonged to release both pentoses and hexoses together as excessive treatment time decomposes the pentoses which are released first.

Regarding the utilization of rice straw, an agricultural waste, for production of value-added products, both pentose and hexose sugars are useful substrates for bioethanol production. Also, xylose can be used for xylitol production. Hence, xylose production is an important component in the complete utilization of rice straw.

References

- [1] K. Karimi, G. Emtiazi, and M. J. Taherzadeh, "Ethanol production from dilute-acid pretreated rice straw by simultaneous saccharification and fermentation with *Mucor indicus*, *Rhizopus oryzae*, and *Saccharomyces cerevisiae*," *Enzyme and Microbial Technology*, vol. 40, no. 1, pp. 138–144, 2006.
- [2] N. Sarkar, S. K. Ghosh, S. Bannerjee, and K. Aikat, "Bioethanol production from agricultural wastes: an overview," *Renewable Energy*, vol. 37, no. 1, pp. 19–27, 2012.
- [3] H. G. E. Masry, "Utilization of Egyptian rice straw in production of celluloses and microbial protein: effect of various pretreatments on yields of protein and enzyme activity," *Journal of the Science of Food and Agriculture*, vol. 34, pp. 725–732, 1983.
- [4] R. C. Kuhad and A. Singh, "Lignocellulose biotechnology: current and future prospects," *Critical Reviews in Biotechnology*, vol. 13, pp. 151–172, 1993.
- [5] M. J. Taherzadeh, *Ethanol from lignocellulose: physiological effects of inhibitors and fermentation strategies [Ph.D. thesis]*, Chalmers University of Technology, Göteborg, Sweden, 1999.
- [6] M. J. Taherzadeh, C. Niklasson, and G. Lidén, "Acetic acid—friend or foe in anaerobic batch conversion of glucose to ethanol by *Saccharomyces cerevisiae*," *Chemical Engineering Science*, vol. 52, no. 15, pp. 2653–2659, 1997.
- [7] S. Sadasivam and A. Manickam, *Biochemical Methods*, New Age, New Delhi, India, 3rd edition, 2008.
- [8] N. Yoswathana, P. Phuriphipat, P. Treyawutthiwat, and M. N. Eshtiaghi, "Bioethanol production from rice straw," *Energy Research Journal*, vol. 1, no. 1, pp. 26–31, 2010.
- [9] T. J. Eberts, R. H. B. Sample, M. R. Glick, and G. H. Ellis, "A simplified, colorimetric micromethod for xylose in serum or urine, with phloroglucinol," *Clinical Chemistry*, vol. 25, no. 8, pp. 1440–1443, 1979.
- [10] C. J. Israilides, G. A. Grant, and Y. W. Han, "Sugar level, fermentability, and acceptability of straw treated with different acids," *Applied and Environmental Microbiology*, vol. 36, no. 1, pp. 43–46, 1978.

- [11] J. M. Hernández-Salas, M. S. Villa-Ramírez, J. S. Veloz-Rendón et al., “Comparative hydrolysis and fermentation of sugarcane and agave bagasse,” *Bioresource Technology*, vol. 100, pp. 1238–1245, 2009.
- [12] J. F. Saeman, “Kinetics of wood saccharification. Hydrolysis of cellulose and decomposition of sugars in dilute acid at high temperature,” *Industrial and Engineering Chemistry*, vol. 37, pp. 43–52, 1945.
- [13] R. Aguilar, J. A. Ramírez, G. Garrote, and M. Vázquez, “Kinetic study of the acid hydrolysis of sugar cane bagasse,” *Journal of Food Engineering*, vol. 55, pp. 309–318, 2002.
- [14] S. J. Téllez-Luis, J. A. Ramírez, and M. Vázquez, “Mathematical modelling of hemicellulosic sugar production from sorghum straw,” *Journal of Food Engineering*, vol. 52, pp. 285–291, 2002.
- [15] K. Karimi, S. Kheradmandinia, and M. J. Taherzadeh, “Conversion of rice straw to sugars by dilute-acid hydrolysis,” *Biomass and Bioenergy*, vol. 30, no. 3, pp. 247–253, 2006.
- [16] K. Y. Foo and B. H. Hameed, “Insights into the modeling of adsorption isotherm systems,” *Chemical Engineering Journal*, vol. 156, pp. 2–10, 2010.
- [17] L. C. Duarte, T. S. Fernandes, F. Carvalheiro, and F. M. Gírio, “Dilute acid hydrolysis of wheat straw oligosaccharides,” *Applied Biochemistry and Biotechnology*, vol. 153, pp. 116–126, 2009.



Hindawi

Submit your manuscripts at
<http://www.hindawi.com>

