Research Article

Design and Implementation of 8051 Single-Chip Microcontroller for Stationary 1.0 kW PEM Fuel Cell System

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Proton exchange membrane fuel cells (PEMFCs) have attracted significant interest as a potential green energy source. However, if the performance of such systems is to be enhanced, appropriate control strategies must be applied. Accordingly, the present study proposes a sophisticated control system for a 1.0 kW PEMFC system comprising a fuel cell stack, an auxiliary power supply, a DC-DC buck converter, and a DC-AC inverter. The control system is implemented using an 8051 single-chip microcontroller and is designed to optimize the system performance and safety in both the startup phase and the long-term operation phase. The major features of the proposed control system are described and the circuit diagrams required for its implementation introduced. In addition, the touch-sensitive, intuitive human-machine interface is introduced and typical screens are presented. Finally, the electrical characteristics of the PEMFC system are briefly examined. Overall, the results confirm that the single-chip microcontroller presented in this study has significant potential for commercialization in the near future.

1. Introduction

Energy consumption around the world has increased astronomically in recent decades as a result of a burgeoning population, the demand for a higher quality of life, and the arrival of new generation technologies, most of which require a reliable and sustainable energy supply [1]. In some overpopulated countries, such as India, there exists a dearth of power-generating resources, and conventional centralized power generation units are incapable of meeting rising power demands. As a result, many cities face the problems of load shedding, brownouts, and even blackouts [2]. One potential solution for tackling these problems is to generate power in a distributed manner, in which electricity is produced by a large number of small-to-medium sized power plants, rather than a centralized large-capacity power plant.

The generation of power in a conventional manner requires the combustion of hydrocarbon-rich fossil fuels such as coal, oil, and natural gas. However, as the world’s energy demand continues to increase, these natural resources are being rapidly depleted. Moreover, the combustion of hydrocarbon-rich fuels releases carbon dioxide into the atmosphere, thereby contributing to the global warming effect [3]. Therefore, in developing distributed generation systems, the use of green energy resources such as fuel cells, photovoltaic arrays, wind turbines, microturbines, ultra capacitors, batteries, and flywheels has attracted significant attention [4].

Amongst these various technologies, proton exchange membrane fuel cells (PEMFCs), which produce electrical energy via the electrochemical reaction of air and hydrogen, have attracted particular interest since they produce only water and heat as byproducts and are characterized by a high efficiency, low noise, and a low operating temperature [5]. A typical PEMFC system comprises a fuel cell stack, a fuel feed system, an auxiliary power supply, a cooling system, a power conversion system, and so on. In practice, these components are characterized by a highly complex system of interdependencies. Thus, PEMFCs are most conveniently analyzed using some form of numerical modeling technique. Costa and Camacho [6] constructed a dynamic electrochemical model of a PEMFC stack and then used the model to predict
the output voltage, efficiency, and power of the stack as a
function of the load current. Del Real et al. [7] developed a
semiempirical formulation for predicting the fluid dynamics
within a 1.2 kW PEMFC. Tirmovan et al. [8] presented a com-
bined empirical and mathematical model for predicting the
V-I curves of a PEMFC as a function of the stack temperature
and partial oxygen pressure. Kuo and Chen [9] performed
a numerical investigation into the gas flow characteristics,
temperature distribution, electrochemical reaction efficiency,
et al. and electrical performance of a PEMFC with a novel wave-
like gas flow channel.

The performance of a PEMFC is affected by many factors,
including the operating temperature, the pressure, and rela-
tive humidity of the inlet gases, the transport characteristics
of the reactants and byproducts, the dissipation of the
reaction heat, and the purging of unreacted fuel from the cell.
If the performance of such systems is to be enhanced, all of
these factors must be properly coordinated and controlled
[10]. Accordingly, the literature contains many proposals for
sophisticated PEMFC control systems. For example, Rgab
et al. [11] presented a fuzzy logic controller for a PEMFC
stack consisting of 15 cells and showed that the stack could
be successfully controlled even under sudden changes in
the external electric load. Kim and Peng [12] developed a
control scheme for coordinating the dynamics of a PEMFC
stack and a DC-DC converter system, respectively, so as to
meet the changing demands of an external load. Hajizadeh
and Aliakbar-Golkar [13] presented a fuzzy logic scheme
for controlling the power conditioning units in standalone
PEMFC applications (requiring only DC-DC conversion)
and grid applications (requiring both DC-DC conversion and
DC-AC inversion).

In a recent study by the present group [3], a sophisticated
control scheme based on a programmable logic controller
(PLC) was proposed for improving the performance and
efficiency of a 1.0 kW prototype PEMFC system. PLC con-
trollers have many advantages, including a low cost, good
flexibility, and good reliability. However, PLC controllers
require intensive user training and can be implemented only
in certain environments (e.g., they cannot be deployed in
environments characterized by high temperature or vibra-
tion). By contrast, single-chip microcontrollers can not only
do all that PLCs can do and more but also have a smaller
physical size, a cheaper cost, the potential for mass pro-
duction, an improved programming flexibility, and so on.
As a result, single-chip microcontrollers have been used for
many applications in recent years, including electronic locks,
voice-activated devices, cleaning robots, and wireless remote-
controlled vehicles.[14]

The present study proposes a sophisticated control system
based on an 8051 single-chip microcontroller for a 1 kW
PEMFC system comprising a fuel cell stack, an auxiliary
power supply, a DC-DC buck converter, and a DC-AC
inverter. The control scheme is designed to optimize the
system performance and safety in both the startup phase and
the long-term operation phase. The controller is integrated
with a touch-sensitive, intuitive human-machine interface
implemented on a notebook (or PC) such that the operational
status of the PEMFC system can be easily determined and the
operational parameters adjusted if required.

The remainder of this paper is organized as follows.
Section 2 briefly describes the 1.0 kW PEMFC system con-
sidered in the present study. Section 3 introduces the pro-
posed 8051 single-chip microcontroller. Section 4 describes
the touch-sensitive human-machine interface and briefly
examines the electrical performance of the PEMFC system.
Finally, Section 5 provides some brief concluding remarks.

2. Prototype 1.0 kW PEMFC System

Figure 1 presents a schematic illustration of the prototype
1 kW PEMFC system. As shown, the major items of equip-
ment include a hydrogen supply system, an air fan, a PEM fuel
cell stack, a set of cooling fans, a water tank, a DC-DC buck
converter, a DC-AC inverter, an auxiliary power supply, a DC
meter, an AC meter, and an 8051 single-chip microcontroller.
Figure 2 presents a photograph of the assembled system. The
nominal operating parameters of the PEM fuel cell stack are
summarized in Table 1.

The stack consists of 60 cells, bundled into 12 segments,
with each segment containing 5 cells. On activating the
PEMFC system, the startup power is provided by a 24 V
DC rechargeable battery. In the long-term operation phase,
the DC output voltage (30–48 V DC) is stepped down to
a constant 24 V DC via a DC-DC buck converter. Part of
the DC voltage is used to recharge the battery and to power
various components within the system, while the remainder
is converted to a 110 V AC voltage in order to power small-
scale items of electrical apparatus such as fans, computers,
and photocopier machines.

3. 8051 Single-Chip PEMFC Control System

The PEMFC system described in Section 2 is controlled by a
sophisticated 8051 single-chip microcontroller. The controller
continuously monitors various system parameters (e.g., the
inlet gas pressure, stack temperature, DC and AC output
voltage, and external power demand) and then instructs
appropriate actions as required in order to optimize the
system performance and maintain operational safety. For
example, if the controller detects an increase in the external
power demand, it instructs an increase in the air fan speed
in order to increase the amount of air supplied to the stack.
Similarly, if the controller detects that the output voltage or
stack temperature is beyond the safe range, it triggers an audio
and visual warning and shuts the system down if no remedial
action is taken within a predetermined period of time.

As shown in Figure 3, the 8051 microcontroller monitors
five major aspects of the PEMFC system, namely, (1) the
reactant supply system, (2) the PEMFC stack, (3) the DC-
DC buck converter, (4) the DC-AC inverter, and (5) the
external load. It is noted that the microcontroller is physically
situated within the PEMFC system but is interfaced to the
user by means of a notebook (or PC). This section commences
by describing two fundamental components of the PEMFC
control scheme, namely, the reactant supply system and the
3.1 Reactant Supply System. In the prototype PEMFC fuel cell system considered in the present study, the stack is supplied with hydrogen and clean air with a relative humidity (RH) of more than 80%. On system startup (or reset), the controller instructs the air fan to run at full power for a short period of time (20 sec) in order to purge any water and/or inert gas from the stack. During long-term operation, the pressure (supply rate) of the hydrogen fuel is fixed at 150 kPa (see Table 1). However, the flow rate of the oxidant (air) is varied adaptively via a PID controller in response to changes in the external load so as to maintain a constant stoichiometric ratio of 2.5.
Table 1: Nominal data of prototype 1.0 kW PEMFC stack.

<table>
<thead>
<tr>
<th>Specification</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>Number of cells</td>
<td>60</td>
</tr>
<tr>
<td>Nominal power (at 0.7 V/cell)</td>
<td>0.8 kW</td>
</tr>
<tr>
<td>Nominal voltage</td>
<td>37 V</td>
</tr>
<tr>
<td>Nominal current</td>
<td>27 A</td>
</tr>
<tr>
<td>Peak power (at 0.6 V/cell)</td>
<td>1.0 kW</td>
</tr>
<tr>
<td>Active area (cm²)</td>
<td>100 cm²</td>
</tr>
</tbody>
</table>

**Operational conditions**

**Anode (pure H₂)**
- Pressure: 150 kPa
- Temperature: 25°C
- Relative humidity: 100%

**Cathode (air)**
- Pressure: Ambient pressure
- Temperature: 25°C
- Relative humidity: 100%
- Stoichiometric ratio: 2.5

![Figure 4: Output voltage of DC-DC buck converter.](image)

3.2. **Power Conditioning Unit.** As shown in Figure 1, the output voltage of the fuel cell stack varies dynamically in the range of 30~48 V DC. To be of practical use, this voltage must be regulated in some way so as to meet the power supply requirements of different applications. In the prototype PEMFC system considered in this study, this is achieved by means of a power conditioning unit comprising a DC-DC buck converter and a DC-AC inverter. As shown in Figure 4, the DC-DC converter transforms the unregulated voltage produced by the fuel cell stack into a constant 24 V DC voltage (note that this is achieved by monitoring the unregulated voltage produced by the stack and the conditioned voltage produced by the converter and then adjusting the duty ratio of the converter accordingly). As described in Section 2, a small part of the conditioned voltage is used to recharge the auxiliary power supply and to power various DC-based components within the PEMFC system (e.g., the air fan or cooling fans). However, the majority of the 24 V DC voltage is processed by a DC-AC inverter to produce a 110 V AC voltage (60 Hz) to satisfy the power demands of external electrical devices.

3.3. **Operational Flow of 8051 Microcontroller.** Figure 5 presents a flowchart showing the operational flow of the 8051 control system during the startup phase. As shown, the system commences by checking the hydrogen pressure. In the event that the pressure is higher than the preset safety level (i.e., 0.6 kg m⁻²), a warning alarm is sounded. The system then checks the nitrogen pressure and again issues an alarm if the pressure is greater than 0.6 kg/m². Having completed the initial checks, the controller instructs a purging of the fuel cell using nitrogen gas in order to expel any residual unreacted hydrogen. Once the preset purge time (10 sec) has elapsed, the controller instructs the supply of hydrogen and air and the PEMFC system enters the warmup phase.

As the stack warms up, the controller instructs a periodic purge of the unreacted hydrogen and activates the cooling fans as required to maintain the stack at the specified operating temperature (85°C). In addition, the controller continuously monitors the stack output voltage. If the voltage fails to reach the normal operating voltage (30~48 V) within the specified warmup time (3 min), a warning signal is issued; else the DC output voltage of the DC-DC converter is used to recharge the auxiliary power supply. Once the battery is fully recharged, the control system transits to the normal long-term operation mode, in which the 24 V DC output of the DC-DC converter is inverted to a 110 V AC voltage by means of the DC-AC inverter.

Figure 6 presents a flowchart showing the operational flow of the 8051 microcontroller in the normal operation mode. As shown on the left side of the figure, the controller monitors three critical aspects of the system performance, namely, the stack temperature, the stack output current, and the inverter output current. In the event that any of these three operating parameters exceed (or are close to) the maximum permissible values, the controller issues an audible alarm (or warning). As shown in the middle region of the figure, the controller also monitors the output voltage of the DC-AC inverter and issues a warning if the voltage is anything other than the expected output of 110 V AC. As shown toward the right of the figure, the controller continuously monitors the external load placed on the fuel cell system and adjusts the air fan speed as required to maintain a constant stoichiometric ratio of 2.5 by means of a PID control scheme. Finally, as shown on the right side of the figure, the controller instructs a periodic purging of the fuel cell stack in accordance to the following power-based strategy:

- **L:** 0 W ≤ output power < 300 W purge off 20 seconds, purge on 0.3 seconds;
- **M:** 300 W ≤ output power < 600 W purge off 15 seconds, purge on 0.4 seconds;
- **H:** 600 W ≤ output power < 1000 W purge off 10 seconds, purge on 0.5 seconds.
Figure 5: Operational flow of 8051 control system during warmup stage.
4. Human-Machine Interface and Electrical Performance of PEMFC

4.1. Human-Machine Interface. As described in Section 3, the microcontroller is physically situated within the PEMFC system but is interfaced to the user by means of a touch-sensitive notebook (or PC). The human-machine interface performs three basic functions. For a general user, the interface provides the means to observe working status (e.g., the pressure, temperature, current, and voltage) at a high mode (e.g., at the stack mode). For a more experienced user or a qualified technician, the interface provides the ability to explore the system status in more detail (e.g., at the cell level), to examine and adjust the system settings as required, and to download the system data for diagnostic purposes. Finally, the human-machine interface permits the 8051 controller to be accessed remotely via the Internet such that maintenance and system adjustments can be carried out by a certified individual.

Figure 7 shows the home screen of the human-machine interface prior to system startup. It is seen that the screen provides a pictorial representation of all the major components within the PEMFC system and indicates the corresponding parameters of interest, for example, the stack temperature; the output voltage, output current, and output power of the fuel cell stack; the output voltage of the DC-DC converter; and the output voltage, current, frequency, and power of the DC-AC inverter. Notably, by touching any region of the screen, the user can call up a more detailed set of related subscreens in order to analyze the corresponding system component in more detail. For example, Figure 8 shows the subscreen obtained when touching the fuel cell stack region of the home screen. As shown, the screen presents a detailed analysis of the voltage output from each segment of the stack and indicates the corresponding voltage, current, and power (note that the screen shows the prestartup phase, and hence all the system parameters have a value of zero). Figure 9 presents the subscreen provided within the human-machine interface to set the major system parameters, that is, the fuel cell operating temperature, the fuel cell start voltage, the hydrogen purging parameters, and the hydrogen supply pressure.
4.2. Electrical Performance of Controlled PEMFC System. Figure 10 shows the variation of the fuel cell voltage and DC-DC converter voltage during the transition from the system startup phase to the long-term operation phase (note that an external load is not applied). As expected, the fuel cell voltage varies dynamically over the transition period. However, the DC-DC converter successfully stabilizes the output voltage at a value of 24 V following a period of approximately 6 s.

5. Conclusions

This study has presented a sophisticated control scheme based on an 8051 single-chip microcontroller for a prototype 1.0 kW PEMFC system. The operational flow of the control system has been described at a high level and the detailed circuit diagrams required for its implementation have been presented. In addition, the touch-sensitive human-machine interface used to monitor and control the PEMFC system has been introduced. Finally, the electrical performance of the PEMFC system has been briefly examined. Overall, the 8051 single-chip microcontroller proposed in this study has significant potential for low-cost mass production and commercialization in the near future.

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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References


