

## Research Article

# CH<sub>4</sub>/N<sub>2</sub> Adsorptive Separation on Zeolite X/AC Composites

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Received 26 September 2018; Accepted 21 November 2018; Published 2 January 2019

Academic Editor: Philippe Trens

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A series of zeolite X/activated carbon (AC) composites were prepared from the same starting materials at various activation time. The corresponding modified samples were obtained by being treated with diluted NH<sub>4</sub>Cl solution. The relationship between porosity development, surface properties, and CH<sub>4</sub>/N<sub>2</sub> adsorption performance was investigated. The increase of micropore volume is beneficial to the improvement of CH<sub>4</sub> and N<sub>2</sub> adsorption capacity, but more sensitive for CH<sub>4</sub>. In addition, the polar functional groups of zeolite X/AC composites may enhance CH<sub>4</sub> adsorption capacity. More importantly, both developing micropore structure and surface modification contributed to enhance the adsorption selectivity  $\alpha_{\text{CH}_4/\text{N}_2}$ . As the optimum sample of these studies, HZAC(24) showed CH<sub>4</sub> adsorption capacity of 17.3 cm<sup>3</sup>/g and the highest adsorption selectivity  $\alpha_{\text{CH}_4/\text{N}_2}$  of 3.4. The CH<sub>4</sub> and N<sub>2</sub> adsorption isotherms of all samples can be well fitted by the Langmuir–Freundlich model. HZAC(24) showed an excellent cyclability of adsorption/desorption of CH<sub>4</sub> with a neglectable capacity loss after subsequent cycles. Moreover, HZAC(24) displayed relatively rapid adsorption kinetics. These properties of zeolite X/AC composites are essential for the adsorptive separation of CH<sub>4</sub> from N<sub>2</sub> in the pressure swing adsorption (PSA) process.

## 1. Introduction

The coal bed methane (CBM) is an unconventional gas with a main composition of CH<sub>4</sub>, N<sub>2</sub>, and CO<sub>2</sub>, which reserve is about two times higher than that known to natural gas [1]. Nowadays, due to the CH<sub>4</sub> content in the drainage gas of coal mine is only 20–45%, CBM is usually extracted into the atmosphere, which not only is a waste of energy source but also pollutes the environment as CH<sub>4</sub> is one of the major contributors to the global warming with 20 times higher global warming potential than that of CO<sub>2</sub> [2, 3]. So, it is of great significance to develop and utilize the CBM. The content of CH<sub>4</sub> higher than 80% is required for the application of chemical raw stock and 90% for merging into the civil gas system [4]. For pipeline quality natural gas, the impurities of N<sub>2</sub> and CO<sub>2</sub> content should not exceed 4% and 2%, respectively [5, 6]. So, CH<sub>4</sub> separation from N<sub>2</sub> and CO<sub>2</sub> is one of the important industrial separation processes [7, 8]. However, CH<sub>4</sub> and N<sub>2</sub> possess extremely similar physicochemical properties and kinetic diameter. Therefore, it is a really large challenge to enrich CH<sub>4</sub> from the mixture of CH<sub>4</sub> and N<sub>2</sub> such as CBM.

Generally, membrane [9], cryogenic [10, 11], and adsorption separation [12] are applied to separate the CH<sub>4</sub> and

N<sub>2</sub> mixture. Membrane separation has the drawbacks of low selectivity and the strongly dependence of the membrane which is liable to damage and block; thus, it is not economical in scale separation [13, 14]. Cryogenic separation requires high-energy consumption and is helpless for low flow rates. In comparison with other methods, adsorption separation with easy operation, lower energy requirement, lower operational cost, running continuous at ambient temperature, and so on attracts increasingly attention. During the past three decades, there has been a rapid growth in the development of adsorption-based technologies for separation and purification of different gas mixtures, so that it can be applied to medium-scale CH<sub>4</sub>/N<sub>2</sub> separation. However, it is still a big challenge as for the larger-scale CH<sub>4</sub>/N<sub>2</sub> adsorption separation due to the lack of satisfactory adsorbent with high adsorption capacity and selectivity.

Many materials have been developed for gas selective separation. Zeolites, as one of the candidates for enriching CH<sub>4</sub> from gas mixture, have shown great prospect and can potentially be used in the pressure swing adsorption (PSA) process. In order to obtain an appropriate zeolite for gas adsorption separation, the effect factors, including the pore structure of zeolite and the strength of the electric fields

caused by the presence of exchangeable cations in the frameworks, have been investigated [5, 14]. It has been found that zeolite X [15–21] is one of the most suitable zeolite adsorbents for adsorption and separation due to its large pore diameter of 0.74 nm which can accommodate large molecules and low Si/Al ratio with the presence of extra framework of cations that produces electric field which interacts strongly with the high polarizability CH<sub>4</sub> molecule or quadrupolar CO<sub>2</sub> molecules. Activated carbon [22–24], another promising candidate for gas separation, possesses lots of advantages such as tunable pore size, easy regeneration, and low cost. In general, activated carbons have higher equilibrium selectivity for CH<sub>4</sub> over N<sub>2</sub> but smaller adsorption capacities for CH<sub>4</sub> than zeolites. As a consequence, in order to integrate the advantages of both zeolite and activated carbon in industrial application, increasingly attentions have been concentrated on the synthesis of the novel porous material of zeolite/AC composites in recent years [25, 26]. Meanwhile, the environmental application such as wastewater treatment as well as gas separation using of zeolite/AC composites has been explored preliminarily [27, 28]. In our previous work, the zeolite X/AC composites from elutrilite are prepared by adding pitch powder and precipitate silicon dioxide as an additional carbonaceous and silica source, respectively [25, 29, 30].

The main aim in this work is to introduce amine modifications in a series of zeolite X/AC composites with different activation time in order to increase the interactions with CH<sub>4</sub> without improving those with gases. This strategy will improve the potential of these materials to separate CH<sub>4</sub>/N<sub>2</sub> mixtures, making these materials candidates for natural gas upgrading. The effect of pore texture and surface properties of the adsorbents on the adsorption performance of CH<sub>4</sub> and N<sub>2</sub> was investigated in detail.

## 2. Experimental

**2.1. Preparation of Zeolite X/AC Composites.** Zeolite X/AC composites were prepared by the following two steps. First, the locally available Elutrilite chunk, with major chemical composition of 41.0 wt.% SiO<sub>2</sub>, 35.5 wt.% Al<sub>2</sub>O<sub>3</sub>, and 7.0 wt.% C, was crashed and sieved in order to collect the grains with an average size below 200 meshes. The elutrilite powder was then simply physically mixed with precipitated silica (ca.93% SiO<sub>2</sub>) and pitch powder in order to get a constant molecular ratio SiO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> = 4.5 and a final mass composition of 50 wt.% carbon. The obtained blend powder was kneaded with defined amount of deionized water and extruded into a cylinder shape with dimensions of  $\varnothing$ 2.0 mm  $\times$  6.0 mm by extruder. After drying overnight, the extrudates were calcined in a tubular furnace under a stream of N<sub>2</sub> with a flow rate of 150 ml/min at 723 K for 2 h and following 1123 K for 2 h. After that, the temperature of 1123 K was maintained for time  $t_a$ , and the atmosphere was switched from N<sub>2</sub> to CO<sub>2</sub> (200 ml/min) for activation.  $t_a$  is a variable activation parameter, ranging from 4 h to 32 h. A heating rate of 5 K/min was applied up to the appointed temperature in the above procedure. Subsequently, the activated samples were treated with a NaOH hydrothermal system in a flash

(Al<sub>2</sub>O<sub>3</sub>:SiO<sub>2</sub>:Na<sub>2</sub>O:H<sub>2</sub>O = 1:4.5:4.5:135), and then, the products were filtered, washed with deionized water at 323–343 K until the pH of the products reached around 7, and dried at 373 K for at least 6 h. ZAC( $t_a$ ) ( $t_a$  = 4, 16, 24, and 32, which represent the activation time of 4 h, 16 h, 24 h, and 32 h) is used to mark the composites, and the corresponding burn-off of ZAC( $t_a$ ) is 42, 29, 21, and 17%, respectively.

The surface modification of the composites was carried out by the conventional soaking method. A typical soaking method involved adding 250 mL of 0.3 mol/L NH<sub>4</sub>Cl solution to about 10 g composite. The solution was heated to 340 K for 0.5 h. After that, the solution was decanted, and fresh solution was added. This procedure was repeated three times. After modification, the samples were filtered and washed with copious amount of deionized water until the effluent was free from chloride ions as tested with AgNO<sub>3</sub> solution. The resulting products were dried at 373 K for more than 6 h and calcined in a tube furnace at 623 K for 2 h under vacuum to dislodge the NH<sub>3</sub> in the products. The corresponding products after modification were denoted as HZAC( $t_a$ ) ( $t_a$  = 4, 16, 24, and 32, which represent the activation time of 4 h, 16 h, 24 h, and 32 h).

**2.2. Characterization.** X-ray powder diffraction (XRD) patterns of the materials were obtained using a Shimadzu LabX XRD-6000 system in the  $2\theta$  range of 5–35° using CuK $\alpha$ 1 ( $\lambda$  = 1.54056 Å) radiation operated with 40 kV and 30 mA. The surface area and pore volume of the products were calculated from N<sub>2</sub> adsorption isotherms measured on a surface area and pore size analyzer, QUADRASORB SI, (Quantachrome Inc., USA) after degassing the samples at 623 K for at least 4 h under high vacuum. The surface areas ( $S_{\text{BET}}$ ) were calculated by using the Brunauer–Emmett–Teller (BET) equation at the relative pressure in the range of 0.01–0.2. The micropore volume ( $V_{\text{mic}}$ ) and micropore surface ( $S_{\text{mic}}$ ) area were determined by the t-plot method. The amount of N<sub>2</sub> adsorbed at  $P/P_0$  = 0.98 was employed to calculate the total pore volume ( $V_{\text{total}}$ ). The total basicity of the samples was determined by temperature-programmed desorption of carbon dioxide (CO<sub>2</sub>-TPD) using a type of TP-5076 TPR/TPD automatic temperature-programmed chemical adsorption apparatus. The surface properties of the samples were analyzed by employing a conventional Boehm titration procedure. Aqueous solutions of NaOH, HCl, Na<sub>2</sub>CO<sub>3</sub>, and NaHCO<sub>3</sub> (0.1 mol/L) with the volume of 25 mL were decanted into conical flasks with 1 g sample each, respectively, and after shaking for 1 h, the conical flasks were kept standing for 48 h, and then filtered. The filtrates were diluted and employed back titration with standard solution to calculate the amount of surface function groups on the samples.

**2.3. Adsorption Measurements.** The presence of water in the composites significantly affects the adsorption isotherm; therefore, all the samples were calcined at 573 K for 4 h under N<sub>2</sub>-flow in a tubular furnace. Prior to adsorption measurements, the samples were degassed under vacuum by heating up to 623 K for at least 4 h. The CH<sub>4</sub> and N<sub>2</sub>

adsorption isotherms were measured at 273 K using a static volumetric apparatus of NOVE1200e instrument (Quantachrome Inc., USA). The adsorption kinetics curve was measured by releasing a small amount of CO<sub>2</sub> with the type NOVE1000e instrument (Quantachrome Inc., USA). During the adsorption, measurement temperature was maintained by circulating ethanediol-water from a constant temperature bath. The adsorption capacity was determined from the adsorption isotherm measured at 273 K, and the pure component selectivity of CH<sub>4</sub> and N<sub>2</sub> ( $\alpha_{\text{CH}_4/\text{N}_2}$ ) was calculated by using the following equation:

$$\alpha_{\text{CH}_4/\text{N}_2} = \left[ \frac{V_{\text{CH}_4}}{V_{\text{N}_2}} \right]_{P,T}, \quad (1)$$

where  $V_{\text{CH}_4}$  and  $V_{\text{N}_2}$  are the adsorption amount (at 273 K, 100 kPa) of CH<sub>4</sub> and N<sub>2</sub>, respectively.

### 3. Results and Discussion

**3.1. Zeolite X/AC Composites.** The XRD patterns of zeolite X/AC composites before and after modification are shown in Figure 1. It can be seen that all samples are highly crystalline materials giving the reflections in the range of 5–35° and exhibit characteristic peaks of zeolite X without other impurity phases. The crystallinity of zeolite X decreases after surface modification as evidenced from the decrease of the intensity of the major characteristic peaks of zeolite X. This is due to the partially collapse of the crystalline structure, which is consistent with the conclusion from others [31, 32].

Figure 2 displays N<sub>2</sub> adsorption-desorption isotherms at 77 K on a series of samples. All isotherms exhibit the characteristic combination of the type-I and type-IV morphology, indicating the coexistence of micropores and mesopores in the composites [33]. Table 1 summarizes their pore structure parameters calculated from the isotherms. It can be seen that, as far as  $t_a \leq 24$  h, the  $S_{\text{BET}}$ ,  $S_{\text{mic}}$ ,  $V_{\text{total}}$ , and  $V_{\text{mic}}$  of ZAC( $t_a$ ) samples presented a significant rising trend, and it occurred sharply decrease thereafter, while the  $S_{\text{ext}}$  was increasing with lengthening the activated time. This means that extending the activation time when  $t_a \leq 24$  h mainly induces the creation of new pores, while widening of pores becomes the main mechanism of porosity development with longer activation time [25]. In addition, the treatment of NH<sub>4</sub>Cl solution has a significant effect on the textural properties. In comparison with ZAC( $t_a$ ), the pore structure parameters of HZAC( $t_a$ ) decrease except  $S_{\text{ext}}$ , due to the partially collapse of the crystalline structure in the composites during surface modification [32].

The CO<sub>2</sub>-TPD results of ZAC( $t_a$ ) and HZAC( $t_a$ ) are shown in Figure 3. For ZAC( $t_a$ ) samples, a larger desorption peak at 573–673 K and a little shoulder peak take place at around 383 K, corresponding to the surface basic site; however, there is only one desorption peak of HZAC( $t_a$ ) samples at about 473–573 K. From Figure 3, it can be seen that CO<sub>2</sub> desorption peak areas increase and CO<sub>2</sub> desorption peak moves to higher temperature for ZAC( $t_a$ ) samples when increasing activation time, indicating that the amount and strength of surface basic groups rising, respectively.

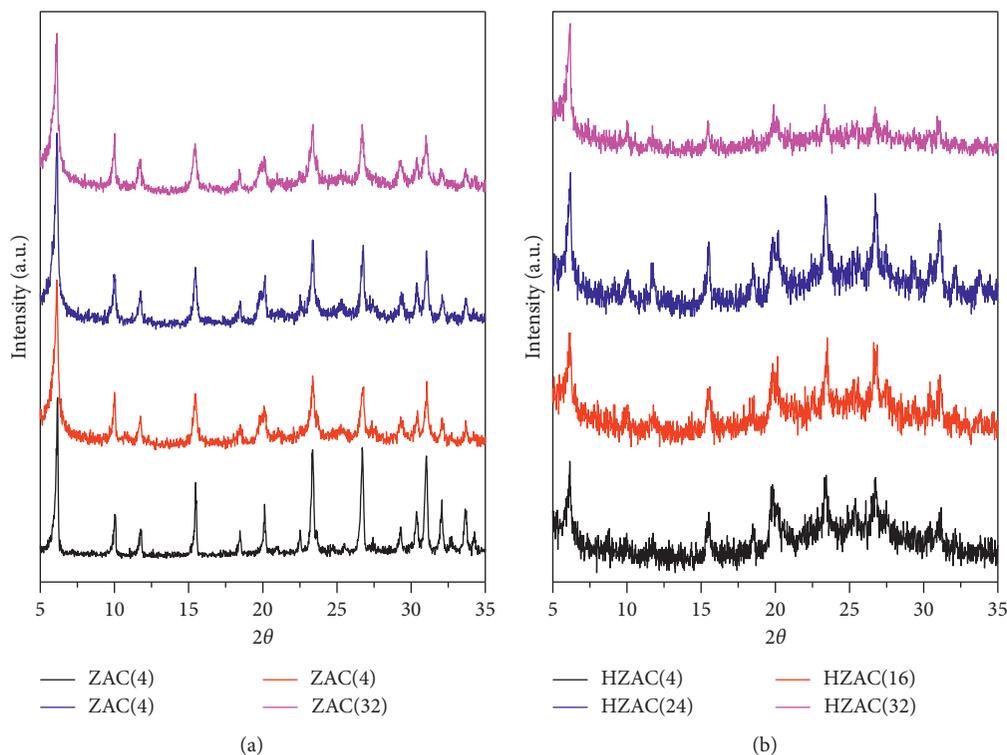
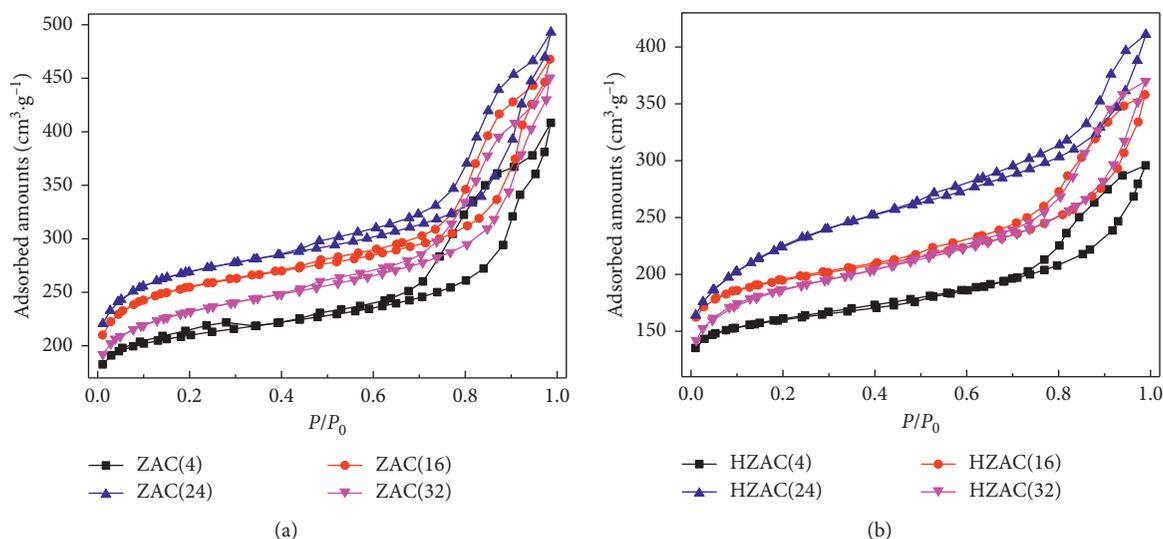
The variation tendency of the surface basic properties of HZAC( $t_a$ ) is similar with ZAC( $t_a$ ). However, both the amount of the surface basic groups and basic strength decline for HZAC( $t_a$ ) compared with ZAC( $t_a$ ), which resulted from the treatment by NH<sub>4</sub>Cl solution. In addition, Figure 4 shows the representative Boehm titration results of ZAC(24) and HZAC(24), which shows that the basic groups decrease almost half, and phenolic, carboxylic, and the total acidic groups sharply increase. These results are similar to the reports from references [34–36].

**3.2. CH<sub>4</sub> and N<sub>2</sub> Adsorption Isotherms.** The pure component CH<sub>4</sub> and N<sub>2</sub> adsorption isotherms at 273 K on the samples of ZAC( $t_a$ ) and HZAC( $t_a$ ) have been generated and are given in Figure 5. All curves are found to be type-I as per the IUPAC classification, and the low-pressure adsorption isotherms behave linearly [14, 33], which is ideal for sorbent regeneration, since most of the working capacity is recovered at moderate pressure ranges. A summary of adsorption and separation parameters extracted from adsorption isotherms is presented in Table 1. It can be seen that the CH<sub>4</sub> adsorption capacity is higher than that of N<sub>2</sub> on all of the samples. The CH<sub>4</sub> and N<sub>2</sub> adsorption capacity and CH<sub>4</sub>/N<sub>2</sub> adsorption selectivity increased with the increase of  $V_{\text{mic}}$ . After the composites being treated by NH<sub>4</sub>Cl, both of the CH<sub>4</sub> and N<sub>2</sub> adsorption capacity on the composites decreased; however, the CH<sub>4</sub>/N<sub>2</sub> adsorption selectivity increased significantly.

Equilibrium adsorption isotherms in adsorbents are required for the available modeling or simulation of the various PSA separation processes of CH<sub>4</sub> and N<sub>2</sub> in practical application. Hence, in order to extend its utility, the collected experimental adsorption isotherm data should be fitted to an isotherm model [37]. In the present work, the adsorption isotherms of CH<sub>4</sub> and N<sub>2</sub> on all samples are fitted using the conventional Langmuir–Freundlich (L-F) (equation (2)) adsorption model [38, 39]:

$$Q = \frac{Q_m b_{\text{L-F}} p^{1/n}}{(1 + b_{\text{L-F}} p^{1/n})}, \quad (2)$$

where  $p$  is the pressure,  $Q$  is the corresponding amount of the adsorbate adsorbed,  $Q_m$  is the saturation capacity of the adsorbent,  $b_{\text{L-F}}$  is the adsorption affinity defined by the van't Hoff equation for a heterogeneous solid, and  $n$  is the reciprocal of the Freundlich heterogeneity factor (the larger the value, the more the deviation from the Langmuir isotherm). Both  $b_{\text{L-F}}$  and  $n$  are empirical constants to be obtained by the data fitting method. Fitted parameters of the CH<sub>4</sub> and N<sub>2</sub> adsorption isotherms for all samples with L-F models are listed in Table 2. It can be seen that the Langmuir–Freundlich model is well correlated with the experimental adsorption data over the entire pressure range studied. Obviously, the values of  $b_{\text{L-F}}$  of CH<sub>4</sub> adsorption are higher than that of N<sub>2</sub> for ZAC( $t_a$ ), suggesting the stronger interaction between CH<sub>4</sub> and the samples than that between N<sub>2</sub> and the composites. After NH<sub>4</sub>Cl treatment, the value of  $b_{\text{L-F}}$  decreases for N<sub>2</sub> adsorption, due to a decrease in the interaction between N<sub>2</sub> and modified composites. However,

FIGURE 1: XRD patterns of ZAC( $t_a$ ) and HZAC( $t_a$ ).FIGURE 2: N<sub>2</sub> adsorption-desorption isotherms at 77 K of ZAC( $t_a$ ) and HZAC( $t_a$ ).

$b_{L-F}$  increases for CH<sub>4</sub> adsorption, and the higher value of  $b_{L-F}$  for HZAC( $t_a$ ) is due to an increase in the interaction between CH<sub>4</sub> and HZAC( $t_a$ ). The changes in the  $b_{L-F}$  values of both CH<sub>4</sub> and N<sub>2</sub> adsorptions explain well the increase of the CH<sub>4</sub>/N<sub>2</sub> selectivity on HZAC( $t_a$ ).

**3.3. Effect of Pore Structure and Surface Properties on the Adsorption Performance.** In order to improve the CH<sub>4</sub>/N<sub>2</sub> adsorption selectivity and maintain the adsorption capacity

of CH<sub>4</sub>, the relationship between CH<sub>4</sub> and N<sub>2</sub> adsorption properties and the pore texture were studied in detail. ZAC(32) possesses a lower  $V_{mic}$  and a larger  $S_{ext}$  than ZAC(24), and the adsorption capacity and selectivity of CH<sub>4</sub> and N<sub>2</sub> showed the lower values on ZAC(32), indicating that the high adsorption capacity and selectivity of CH<sub>4</sub> and N<sub>2</sub> results from the large micropore volume rather than  $S_{ext}$  [40–45]. In Figure 6, the adsorption capacity of CH<sub>4</sub> and N<sub>2</sub> and adsorption selectivity  $\alpha_{CH_4/N_2}$  are plotted versus  $V_{mic}$ . For ZAC( $t_a$ ), as the  $V_{mic}$  increased from 0.275 cm<sup>3</sup>/g to

TABLE 1: Pore structure properties and CH<sub>4</sub>/N<sub>2</sub> adsorptive separation performance of samples.

Samples	$S_{\text{BET}}$ (m <sup>2</sup> /g)	$S_{\text{mic}}$ (m <sup>2</sup> /g)	$S_{\text{ext}}$ (m <sup>2</sup> /g)	$V_{\text{mic}}$ (cm <sup>3</sup> /g)	$V_{\text{total}}$ (cm <sup>3</sup> /g)	Adsorption capacity (cm <sup>3</sup> /g)		$\alpha$
						CH <sub>4</sub>	N <sub>2</sub>	
ZAC(4)	816	694	121	0.275	0.633	16.1	7.52	2.1
ZAC(16)	965	828	136	0.341	0.725	19.1	8.37	2.3
ZAC(24)	1018	868	150	0.357	0.765	22.6	9.39	2.4
ZAC(32)	871	709	168	0.293	0.699	18.2	8.25	2.2
HZAC(4)	610	482	128	0.196	0.459	14.4	5.16	2.7
HZAC(16)	741	592	149	0.238	0.555	16.4	5.12	3.2
HZAC(24)	802	627	175	0.273	0.636	17.3	5.10	3.4
HZAC(32)	695	511	184	0.211	0.572	16.0	5.12	3.1

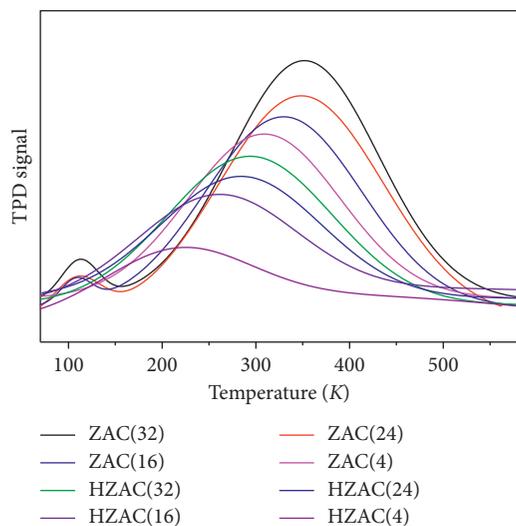
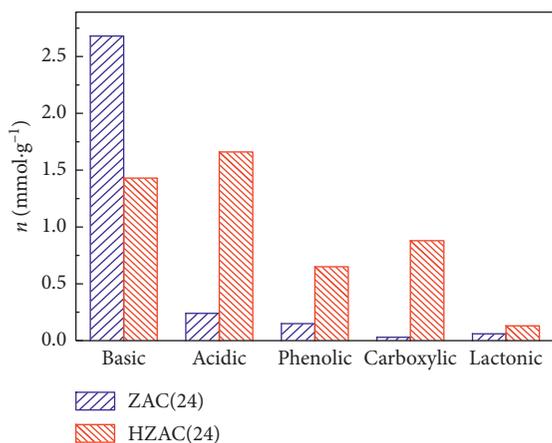
FIGURE 3: CO<sub>2</sub>-TPD of ZAC(*t<sub>a</sub>*) and HZAC(*t<sub>a</sub>*).

FIGURE 4: Results of Boehm titration on ZAC(24) and HZAC(24) samples.

0.357 cm<sup>3</sup>/g, the adsorption capacity of CH<sub>4</sub> and N<sub>2</sub> increased from 16.1 cm<sup>3</sup>/g to 22.6 cm<sup>3</sup>/g and 7.52 cm<sup>3</sup>/g to 9.39 cm<sup>3</sup>/g, respectively. When the  $V_{\text{mic}}$  increases from 0.196 cm<sup>3</sup>/g to 0.273 cm<sup>3</sup>/g for HZAC(*t<sub>a</sub>*), the CH<sub>4</sub> adsorption capacity increases from 14.4 cm<sup>3</sup>/g to 17.3 cm<sup>3</sup>/g. The adsorption selectivity  $\alpha_{\text{CH}_4/\text{N}_2}$  for ZAC(*t<sub>a</sub>*) and HZAC(*t<sub>a</sub>*)

presents a slight rise tendency. As a summary, with the increase of  $V_{\text{mic}}$ , CH<sub>4</sub> and N<sub>2</sub> adsorption capacity increased, and adsorption selectivity  $\alpha_{\text{CH}_4/\text{N}_2}$  enhances slightly at the same time. However, the CH<sub>4</sub> and N<sub>2</sub> adsorption properties of ZAC(4) are different from HZAC(24) although the values of  $V_{\text{mic}}$  for the two samples are similar, which suggests that the pore structure is not the only factor affecting the gases adsorption performance on the samples.

Besides pore structure, the surface properties are also considered to be a significant factor on the gas adsorption process of the studied samples. After the treatment by NH<sub>4</sub>Cl, the basic groups decreased severely and the acidic groups including phenolic and carboxylic groups sharply increased. Although CH<sub>4</sub> is a nonpolar molecule, it has a higher polarizability of  $26 \times 10^{-25}$  cm<sup>3</sup> [46]. Such polarizability causes a momentary shift in the time when the neutral electrostatic field of CH<sub>4</sub> is in close proximity to the larger polar function groups such as phenolic and carboxylic groups within the composites. The polarizability of N<sub>2</sub> ( $17.6 \times 10^{-25}$  cm<sup>3</sup>) is much lower than that of CH<sub>4</sub>. Hence, the increasing of polar functional groups is more conducive to enhance the interaction between CH<sub>4</sub> molecule and the adsorbents [32, 39, 40, 47]. The reduction of the CH<sub>4</sub> adsorption capacity resulted from the decrease of  $V_{\text{mic}}$  in HZAC(*t<sub>a</sub>*) was offset partially by the increase in interaction strongly between CH<sub>4</sub> molecule and HZAC(*t<sub>a</sub>*). These characteristics lead to a moderate decrease in CH<sub>4</sub> adsorption capacity and a drastic decrease in N<sub>2</sub> adsorption capacity after NH<sub>4</sub>Cl treatment; therefore, the adsorption selectivity  $\alpha_{\text{CH}_4/\text{N}_2}$  on the HZAC(*t<sub>a</sub>*) is extremely higher than that on the ZAC(*t<sub>a</sub>*). In conclusion, there is a positive correlation between CH<sub>4</sub> adsorption capacity and adsorption selectivity  $\alpha_{\text{CH}_4/\text{N}_2}$  and the  $V_{\text{mic}}$ . When the  $V_{\text{mic}}$  of samples is similar, the CH<sub>4</sub> adsorption capacity and the adsorption selectivity  $\alpha_{\text{CH}_4/\text{N}_2}$  depended on the surface properties of the samples. HZAC(24) with a considerable  $V_{\text{mic}}$  and a higher amount of acidic groups has satisfactory CH<sub>4</sub> adsorption capacity and the maximum adsorption selectivity  $\alpha_{\text{CH}_4/\text{N}_2}$  among the studied samples.

3.4. Cycle Adsorption and Time-Dependent Adsorption Capacity of CH<sub>4</sub>. As adsorption-driven gas separation processes depend on the cyclic regeneration of the adsorbent,

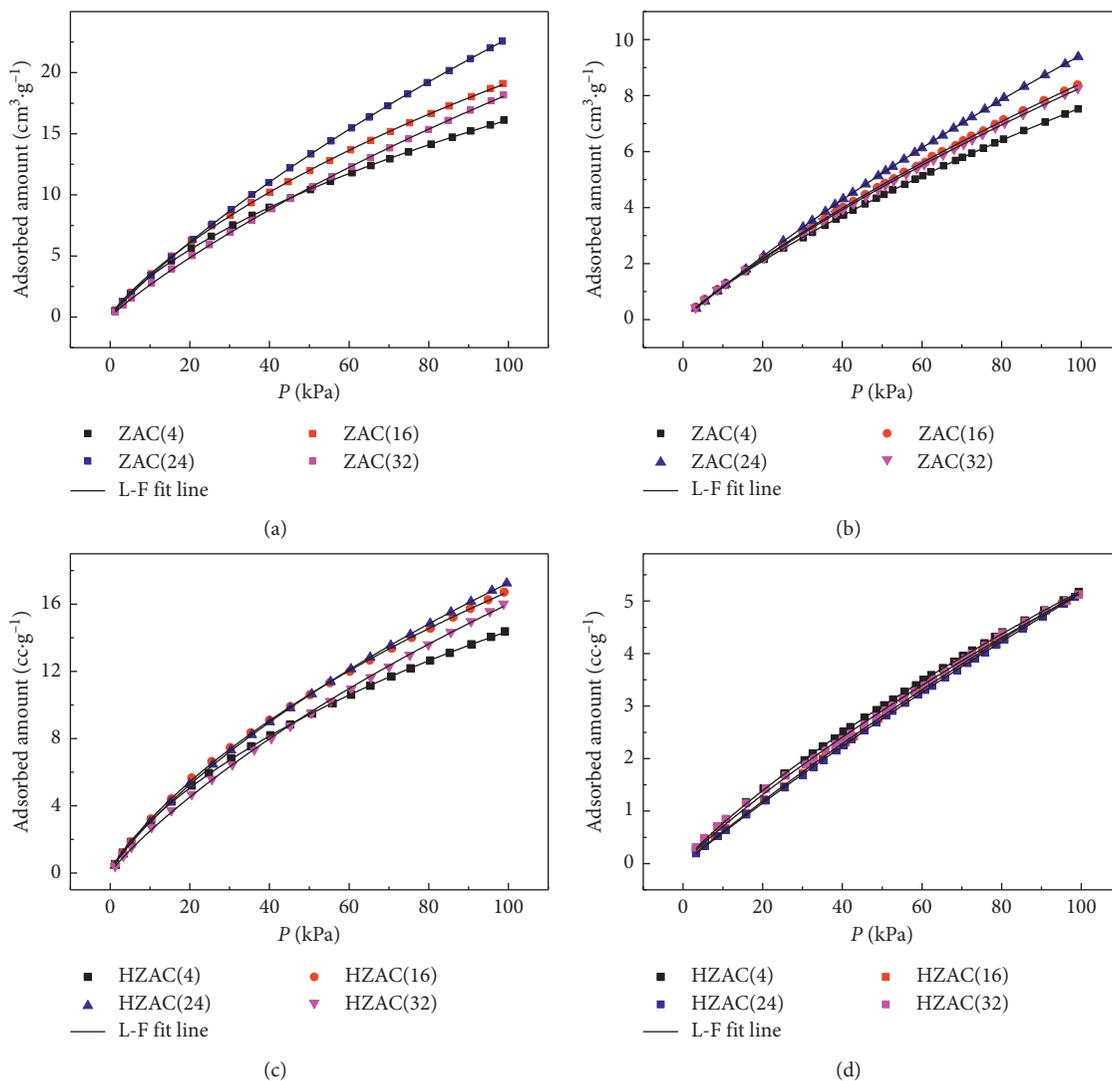


FIGURE 5: Adsorption isotherm of (a, c) CH<sub>4</sub> and (b, d) N<sub>2</sub> at 273 K on ZAC(*t<sub>a</sub>*) and HZAC(*t<sub>a</sub>*).

TABLE 2: L-F fitting parameters of CH<sub>4</sub> and N<sub>2</sub> isotherms on ZAC(*t<sub>a</sub>*) and HZAC(*t<sub>a</sub>*).

Adsorbate	Adsorbent	L-F model			
		$Q_m$ (cm <sup>3</sup> /g)	$b_{L-F} \times 10^{-3}$ (kPa <sup>-1</sup> )	$n$	$R^2$
N <sub>2</sub>	ZAC(4)	48.6	3.3	1.14	0.999
	ZAC(16)	55.0	2.7	1.09	0.999
	ZAC(24)	57.4	2.2	1.02	0.999
	ZAC(32)	52.0	2.7	1.08	0.999
	HZAC(4)	38.5	2.6	1.13	0.999
	HZAC(16)	36.7	1.7	1.01	0.999
	HZAC(24)	40.1	1.5	1.00	0.999
	HZAC(32)	38.2	2.3	1.09	0.998
CH <sub>4</sub>	ZAC(4)	64.6	8.7	1.27	0.999
	ZAC(16)	81.5	6.6	1.20	0.999
	ZAC(24)	105.6	3.8	1.17	0.999
	ZAC(32)	81.9	3.7	1.06	0.999
	HZAC(4)	53.4	10.0	1.28	0.999
	HZAC(16)	64.5	7.6	1.20	0.999
	HZAC(24)	86.0	5.3	1.19	0.999
	HZAC(32)	77.1	4.3	1.11	0.999

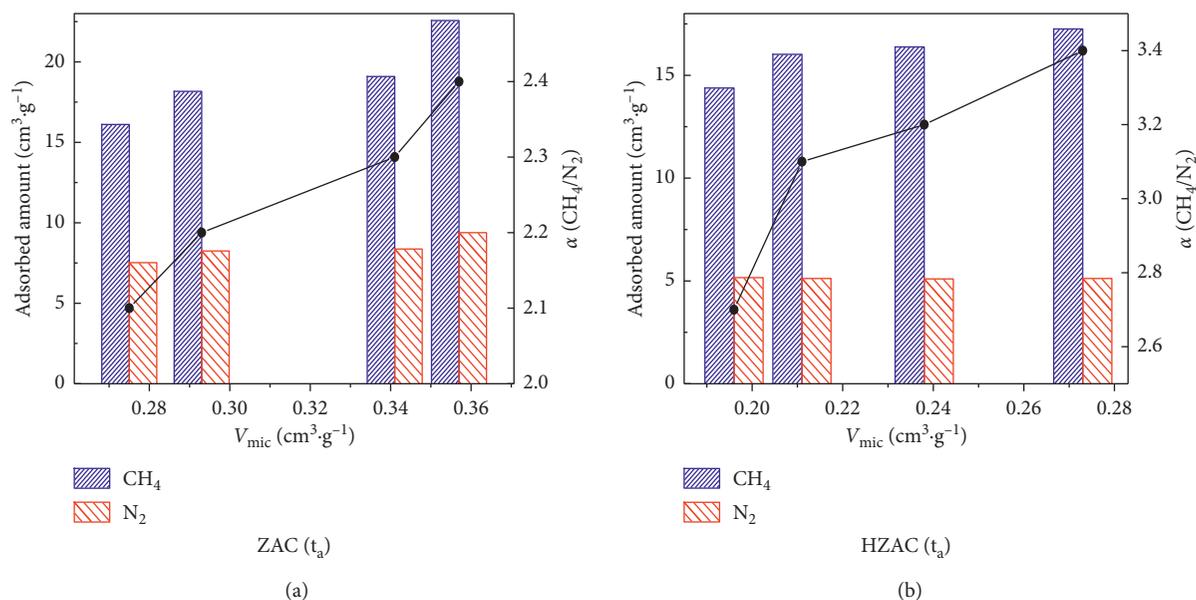


FIGURE 6:  $CH_4$  and  $N_2$  adsorption capacity and selectivity plotted of  $V_{mic}$ : (a) ZAC( $t_a$ ) and (b) HZAC( $t_a$ ).

it is important to study the cyclic adsorption performance of the adsorbents during long-term cyclical operation [48]. The successive adsorption/desorption cycles on HZAC(24) were carried out for nine times, and the results are shown in Figure 7. Within each cycle, the HZAC(24) was regenerated by reducing the pressure of  $CH_4$  along the desorption branch and finally reached the conditions of a dynamic vacuum. The maximum  $CH_4$  adsorbed amount was almost constant in nine cycles of adsorption and desorption, indicating that the  $CH_4$  adsorption performance of HZAC(24) is stable. The results suggest that the zeolite X/AC composite can be easily regenerated by vacuum in the  $CH_4$  adsorption system and be reused for many circles without any decay for the adsorption capacity.

For potential applications of zeolite X/AC composite in adsorption-driven separation of  $CH_4$  from  $CH_4/N_2$  mixture, it is also crucial that the adsorption of  $CH_4$  is rapid. Typically, the industrial adsorption process is shorter than 1 min [49]. Here, we studied the time-dependent adsorption of  $CH_4$  on HZAC(24) by releasing a small amount of  $CH_4$  and studying the adsorbed amount as a function of time as shown in Figure 8. HZAC(24) displayed a relatively rapid adsorption kinetics, reaching 96% of the  $CH_4$  capacity within 40 s. The rapid uptake indicates that zeolite X/AC composite can meet the requirements for an adsorbent used in the PSA process for the separation of  $CH_4$ .

#### 4. Conclusions

Zeolite X/AC composites with different pore textures were prepared and then treated by diluted  $NH_4Cl$  solution. With the increase of activation time, the micropore volume increased, which reaches the maximum at the activation time of 24 hours. Furthermore, the increase of the micropore volume is beneficial to enhance the adsorption capacity of  $CH_4$  and the adsorption selectivity  $\alpha_{CH_4/N_2}$ . The increase of

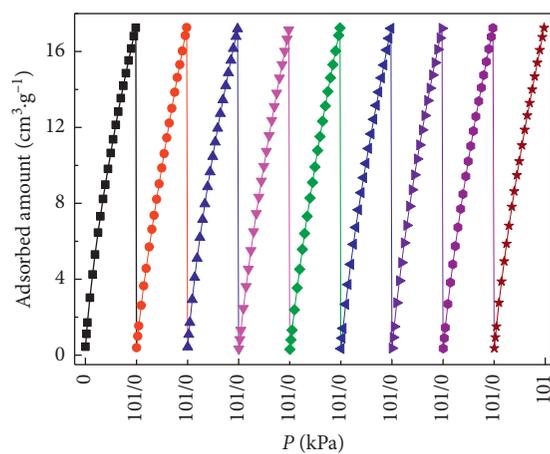


FIGURE 7: Adsorption and desorption cycles for  $CH_4$  on HZAC(24).

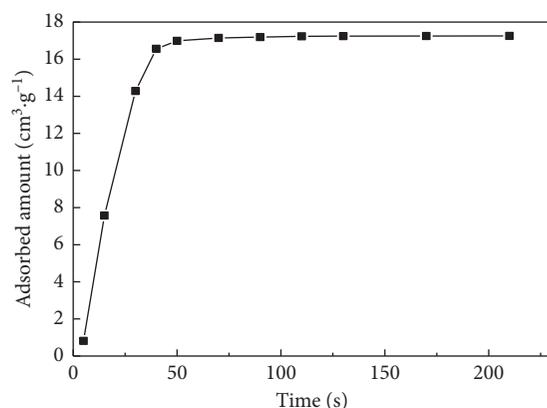


FIGURE 8: Uptake kinetics for HZAC(24) at 273 K.

acidic oxygen-containing functional groups on sample surface significantly contributed to enhancing the adsorption selectivity  $\alpha_{CH_4/N_2}$ , but leading to the decrease of the

adsorption capacity of CH<sub>4</sub>. The HZAC(24) sample showed the highest adsorption selectivity  $\alpha_{\text{CH}_4/\text{N}_2}$  of 3.4 among the studied samples and a high CH<sub>4</sub> adsorption capacity of 17.3 cm<sup>3</sup>/g. The isotherms of CH<sub>4</sub> and N<sub>2</sub> on the composites before and after NH<sub>4</sub>Cl treatment can be well fitted by the Langmuir–Freundlich model. Moreover, the HZAC(24) showed excellent cyclability of adsorption/desorption of CH<sub>4</sub> and relatively rapid adsorption kinetics. The present work provides a promising sight of applying zeolite X/AC composites from an economic and simple synthesis route as CH<sub>4</sub> adsorbent with high adsorption selectivity  $\alpha_{\text{CH}_4/\text{N}_2}$ .

## Data Availability

The data used to support the findings of this study are included within the article.

## Conflicts of Interest

The authors declare that they have no conflicts of interest.

## Acknowledgments

We gratefully appreciate the financial support from the National Natural Science Foundation of China (No. 51204120), Natural Science Foundation of Shanxi (No. 2014021014-1), and Key Scientific and Technological Project of Coal Fund of Shanxi province (No. FT201402-03).

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