Research Article

Physical Simulation of Colayer Water Flooding in Low Permeability Carbonate Reservoir in Middle East

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To study the flow mechanism under different displacement modes of low permeability carbonate reservoir in the Middle East and to improve the utilization of various types of reservoirs, the physical simulation experiments of water flooding by different displacement methods were carried out. Selecting two types of rock samples with different permeability levels, two-layer coinjection and separated production experiments by samples I and III and conventional water flooding experiments by samples II and IV were carried out. In addition, by using low magnetic field nuclear magnetic resonance, the development effect of microscopic pore structure under the different injection-production models was analyzed. Results show that, compared with the coinjection, the recovery rate of sample I was higher than II, 19.30%; sample III was lower than IV, 23.22%; and the comprehensive recovery degree reduced by 3.92%. NMR data also show that the crude oil is mainly distributed in the large pore throat; after water flooding, the displacement is also within the large pore throat, whereas the small pore throat is mainly obtained by the effect of infiltration absorption. The above studies provide a laboratory basis and foundation for the further development of low permeability carbonate reservoir in different Middle East strata.

1. Introduction

In recent years, the rational development of carbonate reservoirs has become a hot spot in the domestic and international oil industry. Most of the reservoirs that China was involved in their acquisition and development in the Middle East belong to the low permeability carbonate reservoirs. But the vertical heterogeneity of these reservoirs is strong, the contradiction between layers is prominent, the water content of some layers rises rapidly, and the degree of recovery is lower, which greatly influenced Chinese government for the oilfield development. Therefore, in order to recover the cost as soon as possible during the contract period and to improve the recovery degree and maximize the enterprise benefits, there are urgent needs for studying diverse development methods to improve the usage of various types of reservoirs.

Numerous scholars conducted a series of laboratory experiments on the heterogeneity characteristics of oilfields in different regions and suggested that ameliorating the water injection structure could improve the water absorption status and recovery degree through reasonable subdivision [1–4]. These research results are crucial for the efficient development of oil and gas fields, but mainly for Chinese domestic oil fields; less research on low permeability carbonate reservoirs in the Middle East rarely has a reference value. Therefore, based on the previous studies [5–8], we carried out colayer water flooding indoor simulation experiments and studied the microdistribution situation of residual oil and recovery degree of different pore range by means of low nuclear magnetic resonance (NMR) technique [9, 10]. We performed two different injection-production modes water flooding oil experiment under three states, which guide us to have a more comprehensive understanding on the effect of different interval microscopic pore structure. The results provide some efficient technical policies for the development of Middle East reservoir. In addition, it has certain reference value for the development of colayer water flooding in other low permeability carbonate reservoir.
NMR technique as a new rock analysis technology developed rapidly in recent years in the petroleum industry. It can reflect the pore size distribution and the fluid volume in different pores, which can quantitatively calculate the displacement efficiency and residual oil in different pore size during water flooding oil. Therefore, NMR technique is a potent supplement of routine laboratory water flooding technology [11]. NMR could detect the signal of hydrogen nucleus \( ^1H \) while, having fluid (oil or water) in the cores, NMR has different reflection in \( T_2 \) spectra. The property and amount of internal fluid could influence the shape of the \( T_2 \) spectra, which reflect the size of pore and throat. NMR relaxation time reflects core’s pore size. According to the study [12], the corresponding pores are as follows: clay micropores when the relaxation time is less than 10 ms, large pores when relaxation time \( T_2 \) is greater than 100 ms, and medium pore when relaxation time \( T_2 \) is 10 ms–100 ms. According to the property of recognizing hydrogen nucleus \( ^1H \) of NMR technique, chlorofluorocarbon synthetic oil (no hydrogen nucleus \( ^1H \)) was adopted to conduct physical simulation experiment, so that the signal measured by the NMR relaxation time spectrum was the distribution of the water phase in the rock sample.

## 2. Experimental Design

According to the logging interpretation and core statistics, the average permeability of the Middle East M group is 18–65 \( \times 10^{-3} \mu \text{m}^2 \) and the porosity is 14–22%. In vertical, the stratum is divided into three segments and 15 small layers, which indicate strong heterogeneous. Therefore, we used two sets of rock samples with different permeability difference to carry out the water flooding experiment of coinjection and separate production and used the single layer injection and production as the contrast experiment. Combining the nuclear magnetic resonance technique, we also studied the distribution of microscopic residual oil and recovery degree. The experiment adopts 2 layer samples connecting in parallel, simultaneously injecting, and, respectively, measuring way to simulate the mine field reservoir 2-layer water flooding process. The basic parameters of rock samples are shown in Table 1.

![Table 1: Physical parameters of core samples.](image)

<table>
<thead>
<tr>
<th>Sample number</th>
<th>Length (cm)</th>
<th>Diameter (cm)</th>
<th>Permeability ( \times 10^{-3} \mu \text{m}^2 )</th>
<th>Porosity (%)</th>
<th>Irreducible water saturation (%)</th>
<th>Injection-production patterns</th>
</tr>
</thead>
<tbody>
<tr>
<td>(I)</td>
<td>6.263</td>
<td>3.786</td>
<td>6.061</td>
<td>23.05</td>
<td>42.99</td>
<td>Co-in</td>
</tr>
<tr>
<td>(II)</td>
<td>6.239</td>
<td>3.797</td>
<td>7.659</td>
<td>24.48</td>
<td>25.89</td>
<td>Si-in</td>
</tr>
<tr>
<td>(III)</td>
<td>6.364</td>
<td>3.787</td>
<td>15.491</td>
<td>20.53</td>
<td>27.87</td>
<td>Co-in</td>
</tr>
<tr>
<td>(IV)</td>
<td>6.502</td>
<td>3.551</td>
<td>19.447</td>
<td>14.52</td>
<td>26.99</td>
<td>Si-in</td>
</tr>
</tbody>
</table>

Note: Co-in represents 2-layer coinjection separate production; Si-in represents single layer injection and production.

The experiment was carried out at room temperature. The experiment oil was chlorofluorocarbon synthetic oil. The density of synthetic oil is 1.8 g/cm\(^3\) at 20°C, and the viscosity is 3.2 mPa·s. The experimental water is the simulated formation water based on the results of water quality test configuration, the mineralization degree is 200000 mg/L at 20°C, and the viscosity is 1.15 mPa·s. The experiment adopts constant pressure flooding way, the average single layer injection pressure is 0.2 MPa, and the outlet pressure is normal pressure.

Figure 1 is the schematic diagram of the experiment process of the 2-layer coinjection and separate production. The QUAZIX type displacement pump simulates the formation water into the rock sample, and the confining pressure is applied to the core by the ring pressure pump. The experimental pressure is measured by the sensor, oil-water mixture flowing out from the exit end of the rock sample is, respectively, measured after being separated by the separator; that is, measurement accuracy is 0.01 cm\(^3\).

Specific experimental procedures are as follows: (1) simulate saturated water condition; saturate rock sample with simulated formation water to 10 PV after the rock sample vacuums, and proceed with saturated water condition \( T_2 \) spectrum test; (2) simulate saturated oil condition. Displacing rock sample with chlorofluorocarbon synthetic oil to 10 PV after the rock sample is loaded to the core holder in parallel, and proceed with saturated oil condition \( T_2 \) spectrum test; (3) simulate oil condition. Injecting the rock sample with simulated formation water at constant pressure, record displacement speed, displacement confining pressure, and the amount of displacement oil and water at different times until there is no oil, and proceed with residual oil condition \( T_2 \) spectrum test.

## 3. Results Analysis

Figure 2 and Table 2 show the results of water flooding in different injection-production patterns with different permeability levels. It can be seen that, under the same injection-production patterns, the anhydrous recovery degree, residual oil saturation, and final recovery degree of different permeability levels are significantly different. When the low permeability layer I and high permeability layer III are simultaneously injected by constant pressure, most of injected water flooded into high permeability layer, causing the water in high permeability layer to break through. The water breakthrough time is 460 s, less than the low permeability 2875 s, and the anhydrous recovery degree is 7.11%, less than the low permeability 23.10%. Due to the fact that the high permeability layer likely forms water phase dominant flow channel and the injected water has lower degree of impact to other interval after water breakthrough, while continuously injecting water with the same pressure, this will result in the final recovery degree being lower, only 34.78%. But the low permeability layer still maintains the condition of oil and water infiltration under the lower displacement speed, which could unceasingly displace the oil phase of pores forward,
Figure 1: Experiment flow chart of coinjection and separate production water flooding.

Figure 2: Experiment results of water content and recovery degree curve.

Table 2: Experiment results of different injection-production patterns of samples.

<table>
<thead>
<tr>
<th>Sample number</th>
<th>Permeability (10^{-3} \mu m^2)</th>
<th>Porosity (%)</th>
<th>Injection-production patterns</th>
<th>Anhydrous recovery degree (%)</th>
<th>Residual oil saturation (%)</th>
<th>Final recovery degree (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>(I)</td>
<td>6.061</td>
<td>23.05</td>
<td>Co-in</td>
<td>23.10</td>
<td>25.27</td>
<td>55.68</td>
</tr>
<tr>
<td>(II)</td>
<td>7.659</td>
<td>24.48</td>
<td>Si-in</td>
<td>20.00</td>
<td>43.78</td>
<td>36.38</td>
</tr>
<tr>
<td>(III)</td>
<td>15.491</td>
<td>20.53</td>
<td>Co-in</td>
<td>7.11</td>
<td>47.04</td>
<td>34.78</td>
</tr>
<tr>
<td>(IV)</td>
<td>19.447</td>
<td>14.52</td>
<td>Si-in</td>
<td>12.39</td>
<td>31.76</td>
<td>58.00</td>
</tr>
</tbody>
</table>

Note. Co-in represents 2-layer coinjection separate production; Si-in represents single layer injection and production.
Figure 3: NMR $T_2$ spectra comparison of different injection-production modes.

resulting in the final recovery degree being high, reaching 55.68%. When displacing the low permeability layer II and the high permeability layer IV with the constant pressure, the water breakthrough time is 7800 s and 950 s respectively, and the anhydrous recovery degree is 20.00% and 12.39%, respectively. It can be seen that the lower permeability has higher anhydrous recovery degree. But the final recovery degree of high permeability is 58.00%, higher than the low permeability, 36.38%.

For the same permeability level of rock samples, different injection-production patterns on its recovery degree exert tremendous influence. Rock sample I that adopt coinjection and separate production pattern enhances anhydrous recovery degree 3.10% compared to rock sample II that adopts single layer injection and production pattern, enhances the final recovery degree 19.30%, and reduces the residual oil saturation 18.51%. Rock sample IV that adopts single layer injection and production pattern enhances anhydrous recovery degree 5.28% compared to rock sample III that adopts coinjection and separates production pattern, enhances the final recovery degree 23.22%, reduces the residual oil saturation 15.28%, and reduces the comprehensive recovery degree by 3.92%.

Figure 3 shows the process of water flooding NMR $T_2$ spectrum of two group different permeability level rock
samples. It can be seen that the different permeability samples with the same injection-production patterns have diverse responses; the same permeability samples with different injection-production patterns also have diverse responses. The $T_2$ spectra of 4 rock samples are dominated by bimodal form, which indicate that there are two or more types of pore structures in the rock samples. For the same injection-production patterns (I and II, III, and IV), as the permeability increases, the NMR $T_2$ spectrum moves to the right gradually, indicating that the movable fluid is aggrandized gradually.

From the saturated oil curve, the irreducible water is mainly distributed in the small pores, few in the large pores, which is because, during the formation process of bound water, the oil phase preferentially flows along the macropore, displacing the water in the large pores and leaving the water in the small pores to form irreducible water. From the water flooding curve and the saturated oil curve, the main displacement oil is distributed primarily in the large pores, few in the small pores, which is because, in the process of displacement, water phase likely flows along the large pores with small flow resistance, hence driving out the most of oil phase. From the saturated water curve and the water flooding curve, the residual oil is primarily distributed in the large pores, rarely in the small pores, which is because oil phase in the small pores is seldom and coupled with the effect of infiltration absorption, resulting in residual oil saturation in small pores being scarce, whereas residual oil likely forms in the rock surface and irregular formation of large pores.

4. Conclusions

(1) In the same injection-production modes, the higher permeability rock samples break through the water earlier, and the period of anhydrous recovery degree is relatively short. While breaking through the water, water content rise rapidly. The lower permeability rock samples break through the water relatively late, and the anhydrous recovery degree is larger than the higher permeability rock samples. In the same permeability level, the mode of coinjection separate production breaks through water earlier than the mode of single layer injection and production.

(2) The higher permeability rock samples have lower recovery degree while adopting coinjection and separate production modes than adopting single layer injection and production modes. In contrast, the lower permeability rock samples have higher recovery degree while adopting coinjection and separate production modes than adopting single layer injection and production modes. Therefore, for the different permeability levels, rock samples should take different injection-production modes, and the specific combination boundaries need further study.

(3) The irreducible water is mainly distributed in the small pores. During the displacement process, the oil phase was driven primary on the large pores. Moreover, the residual oil primary concentrated in the large pores due to the small pores being scarcely saturated oil phase. The large pores still have enormous development potential.

Conflicts of Interest
The authors declare that they have no conflicts of interest.

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