Influence of Synthesis Conditions on the Physicochemical Properties and Catalytic Activity of Fe/Cr-Pillared Bentonites

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The synthesis of Fe/Cr-pillared bentonites starting from a 2% clay suspension and also from dry clay using ultrasound treatment for both the aging and the intercalation steps of the pillaring solution considerably reduces the time and the amount of water required compared with the conventional synthesis method. The catalysts were characterized using scanning electron microscopy with an energy dispersive system (SEM-EDS), powder X-ray diffraction (XRD), N₂ and CO₂-adsorption/desorption, electron paramagnetic resonance (EPR), Fourier-transform infrared spectroscopy (FTIR) and thermogravimetric (TG) analysis and the catalytic activity of selected samples was evaluated for the phenol oxidation reaction. The results of XRD analysis showed that delaminated Fe/Cr-pillared bentonite with d₀₀₁ value 68 Å was observed after intercalation a direct mixture of the pillaring solution and dry clay. The adsorption-desorption isotherm analysis showed that the samples synthesized with the proposed methodology in intercalation stage have similar textural properties and these properties do not change remarkably with synthesis conditions. In addition, the characterisation studies showed that the physicochemical properties of samples synthesized by ultrasound were comparable to those of sample synthesized by conventional method in this study. The sample synthesized by conventional method show 50% phenol conversion. This value was higher than those of samples synthesized by ultrasound.

1. Introduction

Pillared clays have been studied as potential micro/mesoporous materials for use as catalysts and catalyst supports on the industrial scale because of their well-controlled pore structure and catalytic properties [1–4]. However, the excessive amount of water required for the diluted clay suspensions and pillaring agents, combined with long synthesis times for the pillared clays, makes it difficult to produce them on the industrial scale [5, 6]. For this reason, studies related to developing a more rapid synthesis of these materials have recently become important. At this point in the development of pillared clay catalysts for the industrial scale, it is important to improve their physicochemical and catalytic properties as well as to develop synthesis methods that decrease their production time and water use [6–10].

The literature indicates that catalysts that include chromium and/or iron give good results for reactions such as methanol dehydration [11], ethylbenzene dehydrogenation [12], Fischer Tropsch synthesis [13], aromatic nitration, the toluene disproportionation [14], carbon monoxide oxidation [15, 16], catalytic acylation of alcohols [17], and phenol oxidation [6, 18–21].

In the literature, the studies related to iron/chromium mixed pillared clay are especially limited in number, even though it is well known that these metals provide superior results for various catalytic reactions. Chromium is preferable for catalytic applications because of its large range of oxidation numbers despite the major disadvantage that the pillared structure of the chromium-pillared clays is damaged when calcined at high temperatures, decreasing the surface area [22, 23]. The disadvantage of Fe-pillared interlayered clays is the result of their small basal spacing, which could adversely impact their surface areas and pore properties and thus reduce their reaction activities [24]. Related studies have implied that catalytic activity can be increased by adding a second metal to the structure of the pillared clays produced using the iron pillaring solution [25].
Phenol is an important and representative temperature resistant organic pollutant that is toxic even at low concentrations and, if found in natural water, generates harmful chlorine compounds during the disinfection of natural water via chlorination [6, 20, 26]. For this reason, it has become increasingly important to purify water contaminated by phenol and its derivatives in recent years. It seemed to be more effective to use advanced oxidation processes to purify waste water containing organic pollutants that are difficult or impossible to decompose biologically [27]. Among advanced oxidation processes, the activation of hydrogen peroxide by means of a solid catalyst (catalytic wet peroxide oxidation CWPO) is the most promising process, both economically and technologically. Pillared clays have offered an important line of research in obtaining solids responding to the CWPO process [15].

In this study, synthesis of iron/chromium-pillared bentonites was accomplished by using ultrasound treatment during both the aging and the intercalation of the pillaring solution. Furthermore, during intercalation stage the pillaring solution and clay are mixed in three different ways: (1) by adding the pillaring solution directly to the dry clay, (2) by adding the dry clay slowly to the pillaring solution, and (3) by adding the pillaring solution slowly to a 2% clay suspension. The physicochemical properties of the derived samples were analyzed by SEM-EDS, XRD, nitrogen and carbon dioxide adsorption/desorption, EPR, FTIR, and TG analysis. The catalytic activities of the Fe/Cr-pillared bentonites were assessed for the catalytic wet peroxide oxidation of phenol.

### 2. Materials and Methods

**2.1. Materials.** Raw bentonite clay (RB) was obtained from Ünye (Turkey) and was used without any further purification or cation exchange. All the chemicals, from Sigma-Aldrich and Merck, were of laboratory reagent grade and used without further purification. Doubly distilled water was used throughout the work.

**2.2. Synthesis of Fe/Cr-Pillared Bentonites.** Fe/Cr-pillared bentonite synthesis was carried out, with any indicated modifications, according to the procedure of Olaya et al. [9]. Pillaring solutions containing iron and chromium were prepared via dropwise addition (flow rate of 1 mL/minute) of a 0.4 M NaOH solution into a solution of FeCl₃·6H₂O and CrCl₃·6H₂O salts in either a 15 : 5 or 5 : 15 Fe : Cr molar ratio, producing on OH⁻/Fe³⁺ + Cr³⁺ ratio of 2.4. Fe/Cr-pillaring solutions were aged with ultrasound at 75°C for 30 minutes, used an ultrasonic bath (Bandelin Sanorex, operating frequency 35 kHz). The intercalation process was performed using one of three methods: (1) by directly mixing the pillaring solution and the dry clay, (2) by slowly adding the dry clay to the pillaring solution, or (3) by slowly adding the pillaring solution to a 2% suspension at of the clay to make a 20 mmol ratio of Fe + Cr/g of clay. The derived suspensions were separated from the liquid phase by centrifugation, and then they were washed to remove the chlorine ions and calcined at 300°C (heating ramp of 3°C/min) for 3 hours after drying at 60°C for 16 hours. For a comparison, Fe/Cr-pillared bentonite was prepared by conventional method. Fe/Cr-pillaring solution was prepared to make Fe/Cr ratio of 15 : 5 and an OH/Fe + Cr ratio of 2.4 and kept at room temperature for 24 hours before adding it dropwise to the previously prepared 2% m/m suspension to give a 20 mmol ratio of Fe + Cr/g bentonite, which was then kept at room temperature for 24 hours with stirring. Filtration, drying, and calcination were performed as previously described. The conditions of synthesis and the nomenclature of the solids obtained were summarized in Table 1.

### 2.3. Characterization Studies.** Scanning electron microscopy (SEM) microphotographs were obtained from powdered samples with a QUANTA 400F Field Emission SEM. The chemical composition of some of the pillared bentonites was determined using a QUANTA 400F Field Emission SEM Energy Dispersive X-ray Spectrometer (EDS).

<table>
<thead>
<tr>
<th>Nomenclature</th>
<th>Fe/Cr ratio</th>
<th>Fe/Fe + Cr ratio</th>
<th>Aging of pillaring solution</th>
<th>Intercalation</th>
</tr>
</thead>
<tbody>
<tr>
<td>Fe/Cr0.75</td>
<td>15 : 5</td>
<td>0.75</td>
<td>Fe/Cr pillaring solution aged for 24 h at room temperature</td>
<td>Fe/Cr pillaring solution slowly added to 2% bentonite suspension and aged for 24 h at room temperature</td>
</tr>
<tr>
<td>Fe/Cr0.75(D)</td>
<td>15 : 5</td>
<td>0.75</td>
<td>Fe/Cr pillaring solution sonicated for 30 minutes at 35 Hz and 75°C</td>
<td>Dry clay directly added to Fe/Cr-pillaring solution sonicated for 30 minutes at 35 Hz and 75°C</td>
</tr>
<tr>
<td>Fe/Cr0.75(CS)</td>
<td>15 : 5</td>
<td>0.75</td>
<td>Fe/Cr pillaring solution sonicated for 30 minutes at 35 Hz and 75°C</td>
<td>Dry clay slowly added to Fe/Cr-pillaring solution sonicated for 30 minutes at 35 Hz and 75°C</td>
</tr>
<tr>
<td>Fe/Cr0.75(SS)</td>
<td>15 : 5</td>
<td>0.75</td>
<td>Fe/Cr pillaring solution sonicated for 30 minutes at 35 Hz and 75°C</td>
<td>Fe/Cr pillaring solution slowly added to 2% bentonite suspension sonicated for 30 minutes at 35 Hz and 75°C</td>
</tr>
<tr>
<td>Fe/Cr0.25(D)</td>
<td>5 : 15</td>
<td>0.25</td>
<td>Fe/Cr pillaring solution sonicated for 30 minutes at 35 Hz and 75°C</td>
<td>Dry clay directly added to Fe/Cr-pillaring solution sonicated for 30 minutes at 35 Hz and 75°C</td>
</tr>
</tbody>
</table>
The obtained obtained products were characterized using X-ray diffraction on a Phillips PW 3710 diffractometer using Cu Kα radiation (40 kV, 40 mA) that ranged between 1 and 70° 2θ. Semiquantitative percentages of the clay were calculated by means of mineral intensity factors, as suggested by Yalçın and Bozkaya [28], and based on the external standard method of Brindley [29].

The porous structure of the samples was characterized from nitrogen and carbon dioxide adsorption-desorption isotherms. Nitrogen adsorption/desorption isotherms of the samples were obtained by means of a Quantachrome NovaWin gas adsorption system at liquid nitrogen temperature. Carbon dioxide adsorption-desorption isotherms of the samples were obtained by means of a Quantachrome Autosorp 1C gas adsorption system at liquid carbon dioxide temperature. Prior to the measurement, samples were outgassed at a temperature of 250° C under high vacuum for 16 h. Specific BET surface area (S_{BET}) values were calculated with 0.05 < P/P_0 < 0.30. The specific external surface area (S_{ext}) and the micropore volume (V_{\mu}) were obtained using the t-plot method. The total pore volume (V_t) was estimated from the adsorption data at a P/P_0 value of ~0.99. The Barrett-Joyner-Halenda (BJH) method was applied to the desorption data for P/P_0 values above 0.20 to determine the mesopore surface area (S_{BHJ}) and the mesopore volume (V_{BHJ}) for pores in the 10–500 Å range. The micropore and mesopore volume distribution as a function of pore size was calculated by Horvath-Kawazoe (HK) and Barrett-Joyner-Halenda (BJH) method, respectively. Micropore volume (V_{\mu,HK}) values were calculated by Horvath-Kawazoe (HK) method, which was applied for micropore size distribution [30, 31].

The Electron paramagnetic resonance (EPR) spectra were recorded in a continuous wave mode using the X band at room temperature using a Bruker ELEXSYS E580 spectrometer.

The FTIR spectra were obtained using KBr pellets and a Perkin Elmer BX-FTIR spectrometer, in the range of 400–4000 cm⁻¹. All spectra were collected at room temperature, with a resolution of 4 cm⁻¹. The acidity of the OH-groups was determined by collecting the spectra of the samples after saturating them with benzene by exposing them to benzene steam for 48 hours.

Thermogravimetric analysis (TGA) was performed by heating the samples in air with a flow rate of 80 mL/min using a Setaram Labsys TGA/DTA thermal analyzer with a heating rate of 10°C/min.

### 2.4. Catalytic Studies

The catalytic experiments of the wet peroxide oxidation of phenol were performed using a glass batch reactor with a capacity of 500 mL that had been open to the atmosphere, thermostated at 298 K, and thoroughly stirred. The reactor was charged with 100 mL of 50 ppm phenol solution and a catalyst (typically, 5.0 g/L). When the required temperature was achieved, the corresponding amount of hydrogen peroxide (0.1 M, 6 mL) was added to the reactor to start the reaction. The total reaction time was fixed at 3 hours. Samples were drawn at 60 and 180 minutes and were filtered through a 0.22 µm nylon filter. The concentration of phenol was determined using the colorimetric reaction of the samples with the Folin-Ciocalteau (F-C) reagent (Fluka) based on the test procedure developed by Box [32]. TOC analyses were performed on a Shimadzu VCPN model carbon analyzer (via the combustion method) that had been equipped with an autosampler.

At the end of each trial, a solution was separated from the reactive medium by filtration in order to determine the leaching of iron and chromium during the reaction. The analysis of iron and chromium in solution was determined by atomic absorption, using a Perkin Elmer AA800 Model spectrometer.

### 3. Results and Discussion

#### 3.1. Analysis of SEM-EDS

The scanning electron micrographs of both raw and some pillared bentonites are shown in Figure 1. Some variation in the shape and surface structure of the bentonites, which occurred as a result of converting the raw bentonite to the pillared bentonite, can be seen in the SEM micrographs. The samples Fe/Cr0.75 and Fe/Cr0.25(D) show that there was both greater aggregation and greater cohesion than for the raw bentonites and that the pores between the particles were closed. However, it is seen that the number of pores between the particles increased for both the samples Fe/Cr0.75(D) and Fe/Cr 0.75(SS). This observation indicated that the use of ultrasound during intercalation favors the formation of larger pores.

The chemical composition of the raw and the pillared bentonites is reported in Table 2. The pillaring of the raw bentonite by Fe/Cr pillars resulted in an increase in the Fe₂O₃ and Cr₂O₃ content, with complete replacement of the interlayer Ca cations. This increase in the Fe₂O₃ and Cr₂O₃ content, with a corresponding decrease in the number of exchangeable Ca cations, indicates the successive replacement of interlayer cations with Fe/Cr pillars. Moreover, it is
Figure 1: SEM microphotographs of (a) RB, (b) Fe/Cr0.75, (c) Fe/Cr0.75(D), (d) Fe/Cr0.75(SS), and (e) Fe/Cr0.25(D) samples.
observed that the amount of iron and chromium incorporated into the structure during intercalation depended on the procedure being applied and treatment. Fe/Cr0.75(SS) includes more iron than other samples, with the same Fe/Fe + Cr ratio, prepared by conventional and ultrasonic treatments. This observation indicates that there is a beneficial effect of using ultrasound treatment and by adding the pillaring solution slowly to the clay suspension on amount of iron that incorporated into the structure. The use of ultrasound in the intercalation stage probably increases exchange of pillars and improves the dispersion and homogenization of the suspended solids [10]. Furthermore, from EDS analysis results, it was observed that, by changing the Fe/Fe + Cr ratio in the pillaring solution, the Fe/Cr ratio in pillared clay could be changed; the success of the replacement of iron and chromium in the structure was increased by pillaring with a solution containing an Fe/Fe + Cr ratio of 0.75.

3.2. X-Ray Diffraction Patterns. The XRD patterns of Fe/Cr-pillared bentonites, together with those of raw and Fe/Cr-intercalated bentonites, are shown in Figure 2. Basal spacing (d001) values are summarized in Table 3. The reflection angle (2θ) of raw bentonite at the 001 plane is determined as 5.65°, corresponding to a basal spacing (d001) value of 15.6 Å. In accordance with the results found in the literature, it is observed that the bentonite samples possessed the bentonite characteristic peaks at angles (2θ) 5.6°, 17.7°, 20°, 35°, and 62° that were protected, even though they were calcined at 300°C [29, 33]. Other peaks were observed that represented impurities like feldspar (15%) at the angles (2θ) ~20.8°, 27.5°, 41.4°, and 56.4°; quartz (2%) at 26.7°; and calcite (1%) at 29.6° [29].

However, at intercalation stage, other than Fe/Cr0.75(D) that is obtained by adding pillaring solution directly to the dry clay, the samples that were synthesized by both conventional and ultrasound treatments were found to possess similar basal spacing (d001) values as the 2θ value observed that the amount of iron and chromium incorporated into the structure during intercalation depended on the procedure being applied and treatment. Fe/Cr0.75(SS) includes more iron than other samples, with the same Fe/Fe + Cr ratio, prepared by conventional and ultrasonic treatments. This observation indicates that there is a beneficial effect of using ultrasound treatment and by adding the pillaring solution slowly to the clay suspension on amount of iron that incorporated into the structure. The use of ultrasound in the intercalation stage probably increases exchange of pillars and improves the dispersion and homogenization of the suspended solids [10]. Furthermore, from EDS analysis results, it was observed that, by changing the Fe/Fe + Cr ratio in the pillaring solution, the Fe/Cr ratio in pillared clay could be changed; the success of the replacement of iron and chromium in the structure was increased by pillaring with a solution containing an Fe/Fe + Cr ratio of 0.75.

Table 3: Basal spacing (d001) values of raw and intercalated/pillared bentonites.

<table>
<thead>
<tr>
<th>Sample code</th>
<th>d001 (Å)</th>
<th>Intercalated</th>
<th>Pillared</th>
</tr>
</thead>
<tbody>
<tr>
<td>Raw bentonite</td>
<td>15.6</td>
<td>14.7</td>
<td></td>
</tr>
<tr>
<td>Fe/Cr0.75</td>
<td>15.6</td>
<td>—</td>
<td></td>
</tr>
<tr>
<td>Fe/Cr0.75(D)</td>
<td>(68.0–15.7)</td>
<td>54.2–13.7</td>
<td></td>
</tr>
<tr>
<td>Fe/Cr0.75(CS)</td>
<td>15.6</td>
<td>—</td>
<td></td>
</tr>
<tr>
<td>Fe/Cr0.75(SS)</td>
<td>15.8</td>
<td>14.1</td>
<td></td>
</tr>
<tr>
<td>Fe/Cr0.25(D)</td>
<td>17.3</td>
<td>12.0</td>
<td></td>
</tr>
</tbody>
</table>

Figure 2: X-ray diffraction patterns of pillared bentonite samples. (a) Fe/Cr-intercalated-pillared bentonites. (b) Fe/Cr-pillared bentonites.
of raw bentonite, 15.6–15.8 Å (see Table 3), according to X-ray diffraction patterns. These values might result from the formed small Fe/Cr pillars as indicated in the related literature [25]. Furthermore, the identical basal spacing observed for these intercalated bentonites indicates the presence of a similar intercalating species in the pillaring solution. However, two peaks can be observed at the reflection angles ($2\theta$) 1.29° and 5.64° for the Fe/Cr0.75(D), with basal spacing $d_{001}$ values of 68.5 Å and 15.7 Å, respectively. These results were in accordance with those of the studies related to delaminated iron-intercalated clays [23, 34, 35]. However, the delamination behavior was not observed in the other intercalated clays, as previously indicated in the literature [36, 37]. Contrarily, Fe/Cr0.25(D) sample showed a decrease in peak intensities and an increase in basal spacing values with respect to raw bentonite in the region of $2\theta$ between 1 and 10°. This result indicates that larger Fe/Cr pillars are formed by increasing the chromium content of the Fe/Cr pillaring solution [38].

Heat treatment of the raw bentonite at 300°C for 3 h decreased the $d_{001}$ spacing to 14.7 Å, indicating retention of the layered structure at higher temperatures (Figure 2(b), Table 2). Strong electrostatic and other forces between the clay layers can help retain the layer structure of the clay materials at higher temperatures. On the other hand, after calcination at 300°C, when comparing the patterns of X-ray diffraction of sample synthesized by conventional method and the patterns of X-ray diffraction of samples obtained by ultrasound treatment, distinctive d-spacing peaks were not observed at XRD patterns of Fe/Cr0.75 and Fe/Cr0.75(CS) samples. The delaminated structure of Fe/Cr0.75(D) was preserved, while the basal spacing value of Fe/Cr0.25(SS) decreased from 15.8 Å to 14.1 Å after 300°C calcination (Table 3).

3.3. $N_2$- and $CO_2$-Adsorption/Desorption Studies. The specific surface areas, the pore volumes, micropore and mesopore size distribution of the raw, and the pillared bentonite samples were determined by nitrogen adsorption/desorption at liquid nitrogen temperature. Carbon dioxide adsorption/desorption isotherms were also performed to determine the distribution of micropore and mesopore size distributions.
Figure 3(a) presents the nitrogen adsorption-desorption isotherms. Both the pillared and raw bentonites possessed type II adsorption isotherms, according to IUPAC classification. The hysteresis found in these materials is H3 type, according to IUPAC classification, and is attributed to either slit-shaped pores or plate-like particles with space between the parallel plates [30, 31].

The textural properties of pillared bentonites are presented in Table 4. It is seen that all pillared bentonites with Fe/Fe + Cr ratio of 0.75 have similar textural properties and
these properties do not change remarkably with different synthesis conditions. The similar textural properties of these pillared bentonites, other than the Fe/Cr0.75(D) sample, may be explained by the formation of a similar sized basal spacing and similar dispersions of the pillars in the interlayer region. However, the Fe/Cr0.25(D) sample has a greater d_{001} value than the other samples, but it has a lower S_{BET} value, which is associated with the amount and dispersion of the pillars among the interlayers of this sample. Furthermore, this result is supported by the Fe/Cr0.25(D) sample possessing V_{m} values lower than both the natural and the other pillared bentonites (Table 4). In addition, when the textural properties of the Fe/Cr0.75(D), Fe/Cr0.75(CS), and Fe/Cr0.75(SS) samples are compared, it is seen that the sample Fe/Cr0.75(CS) has the greatest surface area and pore volume values. These results indicated that the micro-pores formation increases by slow addition of the dry clay to the pillaring solution with ultrasound treatment at intercalation stage.

Figure 3(b) shows the carbon dioxide adsorption-desorption isotherms of the samples. Both the Fe/Cr0.75(D) and Fe/Cr0.25(D) samples have similar adsorption capacities to the raw bentonite, while the Fe/Cr0.75(CS) and Fe/Cr0.75(SS) samples have higher values than the other samples. It was obtained that the adsorption capacities evaluated from carbon dioxide adsorption data were comparable but smaller than the corresponding adsorption capacities obtained from nitrogen adsorption.

The HK-micropore and BJH-mesopore size distributions obtained from the nitrogen adsorption isotherms for the samples that were studied are presented in Figure 4, along with the comparison to the corresponding distributions from the carbon dioxide data. As can be seen from Figure 4, there is a good agreement between the pore size distributions of the adsorbents studied. Raw and all the pillared bentonite samples have two modes of distribution of 4.32 Å and broad 5–8 Å (Figures 4(a) and 4(b)). This behavior indicates the presence of two types of micropore. As clearly shown in Figure 4, no important increases to the volume adsorbed by the micropores resulted from the pillaring processes.

The BJH-mesopore size distribution peaks obtained from nitrogen adsorption are relatively narrow, which allowed us to use the average pore diameter on the maximum of the pore size distribution as the characteristic parameter (Figure 4(c)). However, a larger BJH-mesopore size distribution dispersion is observed for the carbon dioxide adsorption isotherm (Figure 4(d)). It was observed that the pore volumes given by nitrogen isotherms were greater than those of carbon dioxide. The observed differences may be caused by differing sensitivities of the isotherms to different types of porosity; for example, nitrogen adsorption at 77 K may not be as sensitive as carbon dioxide adsorption at 273 K to the same types of microporosity when the micropore size distribution is large [39].

3.4. EPR Analysis. Two characteristic Fe^{3+} signals were observed in smectite-type minerals with values of g equal to 4.3 and 2.0 in the EPR analysis (Figure 5). The presence of isolated Fe^{3+} [19, 40] with either tetrahedral or octahedral coordination is associated to the signal of g equal to 4.3, which for smectite minerals is associated with iron located inside of the clay sheets (iron exchanging aluminum in the octahedral layers). In contrast, the presence of clusters of iron corresponds with the signal of g equal to 2.0. In this work, the signal observed at a g of 2.0 did not change based on the process and the employed Fe/Fe + Cr ratio, but the intensity of the signal observed at a g of 4.3 was greater for the Fe/Cr0.25(D) sample.
Table 4: Textural properties of raw and pillared bentonites.

<table>
<thead>
<tr>
<th>Samples</th>
<th>Surface area (m²/g)</th>
<th>Pore volume (cm³/g)</th>
<th>Pore diameter (Å)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>(S_{\text{BET}})</td>
<td>(S_{\text{ext}})</td>
<td>(S_{\text{BJHdes}})</td>
</tr>
<tr>
<td>Raw Bentonite</td>
<td>65</td>
<td>38</td>
<td>58</td>
</tr>
<tr>
<td>Fe/Cr0.75</td>
<td>109</td>
<td>70</td>
<td>79</td>
</tr>
<tr>
<td>Fe/Cr0.75(D)</td>
<td>97</td>
<td>59</td>
<td>75</td>
</tr>
<tr>
<td>Fe/Cr0.75(CS)</td>
<td>106</td>
<td>67</td>
<td>84</td>
</tr>
<tr>
<td>Fe/Cr0.75(SS)</td>
<td>104</td>
<td>65</td>
<td>82</td>
</tr>
<tr>
<td>Fe/Cr0.25(D)</td>
<td>87</td>
<td>62</td>
<td>96</td>
</tr>
</tbody>
</table>
3.5. FTIR Spectrums. Figure 6 shows the FTIR spectra (400–4000 cm\(^{-1}\)) of both natural and all pillared bentonites. The wave numbers and assignments of the main vibrational peaks come from values found in the literature [41–43]. There were few IR spectral differences between the natural and Fe/Cr-pillared bentonites which implied that the modified clay material kept its original structural configuration after pillaring. The appearance of a broad peak at approximately 3435 cm\(^{-1}\) corresponds to the O–H stretching mode of the absorbed water, with a simultaneous shift to lower wavenumbers and an increase in width. This behavior indicates an increase in the interlayer water content due to the replacement of inorganic cations with the Fe/Cr pillars [24, 42]. Also, the decrease of the peaks at 3631 cm\(^{-1}\) can be detected for all of the pillared bentonites, suggesting that the Fe/Cr pillars could link with Al–O in the alumina octahedral sheet. The peak at 1640 cm\(^{-1}\) can be associated to the bending vibration of the water and shifted to 1636 cm\(^{-1}\) after pillaring. Also, a shift of the peak of raw bentonite at 1036 cm\(^{-1}\) towards higher frequencies was nearly the same in all pillared bentonites (1044 cm\(^{-1}\)). This change has been previously related to a change in the symmetry of the surface Si–O–Si vibration, which is perhaps associated with a change in the electric field near the Si groups due to the proximity of the more positively charged Fe/Cr pillars [44]. Also, the bands at 526 and 467 cm\(^{-1}\) can be ascribed to the Al–O stretching and Si–O bending vibrations shifted to higher wavenumbers (529–469 cm\(^{-1}\)) all pillared bentonites. Absence of additional peaks suggests that no bond formation occurs between bentonite and Fe/Cr-pillars [45].

Adsorption of benzene shows that no strong acid sites are present in all samples (Figure 7). However, because of the interaction between benzene and silanols, there is a small peak observed at 3756 cm\(^{-1}\) for all samples (Figure 7(a)). It was observed that the peak intensity at 3756 cm\(^{-1}\) increased slowly after pillaring with the Fe/Cr pillars. Furthermore, it is seen that after benzene adsorption the peak at 1640 cm\(^{-1}\) increased in intensity (Figure 7(b)). There are two small peaks observed in the all samples, at 1831 cm\(^{-1}\) and 1968 cm\(^{-1}\) from the C–H out-of-plane bending vibration.
3.6. Thermogravimetric Analysis. In order to investigate the thermal behavior of the air-dried Fe/Cr0.75(D), Fe/Cr0.75(SS), and Fe/Cr0.25(D) samples, the thermogravimetric (TG) analyses were carried out in the temperature range of 25–800°C. Pillared bentonites show similar weight loss behavior in the TG analysis (Figure 8). The pillared bentonites show high initial weight losses which gradually decrease at higher temperatures. Two weight loss regions have been observed for all samples in the range of 25–300°C and 300–700°C. The major weight loss occurred at 25–300°C is due to the removal of water molecules present in the interlayer. This dehydration process is one of the characteristics of clay minerals [46]. However, the weight losses observed in the range of 300–700°C are attributed to the water molecules coordinated to the pillars as well as the dehydroxylation of the pillars and clay sheets and can be correlated indirectly to the quantity and distribution of the Fe/Cr-pillars. Contrarily, the total weight loss with the Fe/Cr0.25(D) sample is higher than that of the Fe/Cr0.75(D) and Fe/Cr0.75(SS) sample, which suggests that a significantly higher amount of water is present in the micropores of the two samples. The Fe/Cr0.75(D) and Fe/Cr0.75(SS) samples showed similar total weight losses.

3.7. Catalytic Activity for the Wet Peroxide Oxidation of Phenol. After the synthesis and characterization, the obtained Fe/Cr-pillared bentonites were tested for catalytic activity for the catalytic wet hydrogen peroxide oxidation of phenol under the conditions defined previously. For the purpose of comparison, a control reaction was conducted under the same conditions using only raw bentonite. The quantity of phenol removed using RB, Fe/Cr0.75, Fe/Cr0.75(D), Fe/Cr0.75(SS), and Fe/Cr0.25(D) in the presence of H2O2 is presented in Figure 9. Comparing the oxidation data of the raw and pillared bentonites reveals that pillaring effectively increases the activity of the bentonites. This catalytic activity can be mainly related to the metal content and textural properties. The catalytic activity increases for the solids treated with the active metals. When the oxidation activities of samples synthesized via the conventional method are compared to the activities of samples synthesized by ultrasonication, the sample synthesized by the conventional method, Fe/Cr0.75, showed a higher activity than the other pillared samples (Figure 9). The Fe/Cr0.75 sample resulted in a conversion of 50% of the phenol after 3 h. The phenol conversions of the Fe/Cr0.75(D), Fe/Cr0.75(SS), and Fe/Cr0.25(D) samples were 34, 26, and 40%, respectively over 3 h. The total organic carbon conversion was 3, 31, 26, and 30% for RB, Fe/Cr0.75, Fe/Cr0.75(D), Fe/Cr0.75(SS), and Fe/Cr0.25(D) catalysts, respectively, over 3 h. According to these results, proper number of active sites and their distribution on the catalyst surface is more important for catalyst activity in TOC conversion than the metal content in Fe/Cr-pillared bentonites. Sample Fe/Cr0.75(SS) with fairly high iron and chromium content has the small activity as the other pillared bentonites with lower metal content. Also, these results indicate that, for the complete degradation of phenol under the specified condition, a 3-hour reaction time is inadequate for Fe/Cr0.75 and Fe/Cr0.25(D) samples. The catalytic behavior in phenol oxidation in pillared clays has been recently reported in the literature. In this regard, Carriazo et al. [47] found 100% phenol conversion in less than an hour, and high TOC conversion value (55%) using Al-Ce-Fe-pillared clays. Similarly, Sanabria et al. [48] found total fenol conversion and high TOC conversion (49–53%) in two hours using Al/Fe-pillared clays.

To verify the chemical stability of the materials that were synthesized during this investigation, the presence of inorganic cations in the reaction mixture was analyzed. The obtained AAS confirmed that the iron concentrations in the filtrates taken after 3 h of the reaction did not exceed 0.11 ppm. This value was lower than those reported for Al, Al-Fe-, Al-Ce-Fe-, and Al-Fe-Ce-pillared clays synthesized by the conventional, ultrasound, and microwave method [6, 19, 49], thus demonstrating the stability of the active phase. However, chromium concentrations for the Fe/Cr0.75, Fe/Cr0.75(D), and Fe/Cr0.25(D) samples were observed as 24.08 ± 0.34, 24.53 ± 0.16, and 80.13 ± 1.27 ppm, respectively, indicating that iron pillars are more stable than chromium pillars. However, the catalytic...
behavior in catalytic wet peroxide oxidation of phenol in Fe/Cr-pillared clays has not been recently reported in the literature.

4. Conclusions

The synthesis of Fe/Cr-pillared bentonites starting from either a 2% clay suspension or dry clay and using ultrasound treatment during both the aging and intercalation steps of the pillaring solution allows a considerable decrease in the volume of water and the synthesis times compared with the conventional synthesis method. The results of the XRD and adsorption-desorption isotherms analysis showed that pillaring caused a small increase in basal spacing ($d_{001}$) (except of occurring delamination synthesized by ultrasonic treatment and sample that is directly added to the pillaring solution of dry clay), surface area, and pore volume values. TG analysis shows two stages of weight loss due to dehydration-dehydroxylation processes. In addition, the results of the characterizations and catalytic tests carried out for the Fe/Cr-pillared bentonites synthesized by means of ultrasound treatment displayed similar physicochemical characteristics and smaller phenol conversion than the Fe/Cr-pillared bentonite synthesized by the conventional method in this study.

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References


