Research Article

Biodiesel Production Process Optimization from Sugar Apple Seed Oil (Annona squamosa) and Its Characterization

Siddalingappa R. Hotti1 and Omprakash D. Hebbal2

1Department of Automobile Engineering, PDA College of Engineering, Gulbarga Karnataka 585102, India
2Department of Mechanical Engineering, PDA College of Engineering, Gulbarga Karnataka 585102, India

Correspondence should be addressed to Siddalingappa R. Hotti; hottisr@gmail.com

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This paper presents the production of biodiesel from nonedible, renewable sugar apple seed oil and its characterization. The studies were carried out on transesterification of oil with methanol and sodium hydroxide as catalyst for the production of biodiesel. The process parameters such as catalyst concentration, reaction time, and reaction temperature were optimized for the production of sugar apple biodiesel (SABD). The biodiesel yield of 95.15% was noticed at optimal process parameters. The fuel properties of biodiesel produced were found to be close to that of diesel fuel and also they meet the specifications of ASTM standards.

1. Introduction

Energy is the critical input factor for the socioeconomic development and welfare of human being of any country. Fossil fuels are the major sources for the energy demand since their exploration. India is highly dependent on crude oil; net import of crude oil during 2011-12 is 171.73 million metric tons [1]. Due to limited reserves of fossil fuels, environmental degradation, and volatility in fuel prices, there is a growing need for energy security and protection of the environment. Country like India with an agricultural background has wasteland of about 55.27 million hectares [2], which can be utilized for growing plants/crops, which produce nonedible oil in appreciable quantity. Thus indigenously produced bio-diesel, which is defined as the mono-alkyl esters of vegetable oils or animal fats, obtained by transesterifying oil or fat with an alcohol [3], is considered one of the options to substitute the petroleum fuels.

Many researchers have produced the biodiesel from nonedible oil, which include Jatropha (Jatropha curcas) oil [4–8], Karanja or Honge (Pongamia pinnata/glabra) seed oil [7, 9–12], Polanga (Calophyllum inophyllum) seed oil [13], rubber (Hevea brasiliensis) seed oil [14, 15], mahua (Madhuca indica) oil [16], tobacco (Nicotiana tabacum) seed oil [17], bitter almond (Prunus dulcis) oil [18], castor (Ricinus communis) seed oil [19, 20], okra (Hibiscus esculentus) seed oil [21], Kusum (Schleichera trijuga) oil [22], Simarouba (Simarouba glauca) [23], milo (Thespesia populnea) seed oil [24, 25], milk thistle (Silybum marianum) seed oil [26], and wild safflower (Carthamus oxyacantha Bieb) seed oil [27]. In the production process of biodiesel, the effects of process parameters such as alcohol to oil molar ratio, catalyst concentration, reaction time, and reaction temperature have been studied and optimized. The fuel properties of produced biodiesel have been investigated and compared with the standard specifications for assessing their feasibility to substitute the petroleum fuels. However there are many other nonedible oils for which process parameters are not being optimized. One among them is sugar apple (Annona squamosa) seed oil.

Annona squamosa, the sugar apple, sweetsop, or sugar-pineapple, is a species in the Annonaceae family. Sugar apple is grown in lowland tropical climates worldwide, including southern Mexico, the Antilles, and Central and South America, Tropical Africa, Australia, Indonesia, Polynesia,
Table 1: Fatty acid composition of sugar apple seed oil.

<table>
<thead>
<tr>
<th>Fatty acid composition</th>
<th>Weight %</th>
</tr>
</thead>
<tbody>
<tr>
<td>Lauric acid (C12:0)</td>
<td>0.08</td>
</tr>
<tr>
<td>Palmitic acid (C16:0)</td>
<td>17.79</td>
</tr>
<tr>
<td>Stearic acid (C18:0)</td>
<td>4.29</td>
</tr>
<tr>
<td>Oleic acid (C18:1)</td>
<td>39.72</td>
</tr>
<tr>
<td>Linoleic acid (C18:2)</td>
<td>29.13</td>
</tr>
<tr>
<td>Linolenic acid (C18:3)</td>
<td>1.37</td>
</tr>
<tr>
<td>Arachidonic acid (C20:4)</td>
<td>1.06</td>
</tr>
<tr>
<td>Behenic acid (C22:0)</td>
<td>2.01</td>
</tr>
</tbody>
</table>

Source: [29].

Figure 1: Sugar apple (Annona squamosa) fruits and seeds.

The emphasis of present work is to produce biodiesel from Annona squamosa seed oil by transesterification process and to study the effect of process parameters such as alcohol to oil molar ratio, reaction time, and reaction temperature on the yield of biodiesel. Further the physicochemical properties of produced biodiesel are investigated and compared with diesel and standard specifications of biodiesel to assess its feasibility to replace the petroleum fuel.

2. Materials and Method

2.1. Oil Extraction. The seeds were collected from the different households as one discards the seeds after consuming the fruit. The collected seeds were dried and crushed in a mechanical expeller. For complete extraction of oil the seeds were passed four times through the expeller. The neat oil is allowed to settle for 48 hours and after that oil is stored in an airtight container to avoid oxidation.

2.2. Fatty Acid Composition of Sugar Apple Seed Oil. The vegetable oil extracted from a plant is composed of triglyceride, which is an ester derived from three fatty acids and one glycerol. The fatty acid composition of sugar apple seed oil (SASO) is given in Table 1.

2.3. Transesterification Reaction. The transesterification reaction was carried out in a laboratory scale batch reactor equipped with thermometer and condenser; the heating and stirring were done with a hot plate magnetic stirrer system. In each set of experiment 50 g of oil was heated to the predefined temperature and after attainment of predefined temperature the mixture of catalyst and methanol was transferred to reactor and all the predefined sets of transesterification reaction conditions were measured from this point for each set of experiment. The transesterification reaction mechanism is as shown in Figure 2. Stoichiometrically 3:1 molar ratio of alcohol to oil is needed for completion of transesterification reaction, but many researchers reported that biodiesel yield is maximum with excess molar ratio of alcohol to oil. Hence in the present investigation, in each set of experiment, 6:1 molar ratio of alcohol to oil and constant stirrer speed were maintained.

After the completion of predefined set of transesterification reaction conditions the reaction mixture was transferred into a separating funnel left for 60 minutes to separate into biodiesel and glycerol. The lower layer of glycerol was removed and the upper layer of crude biodiesel is washed several times with hot water at 50°C to remove the impurities,
such as residual catalyst, methanol, soap, and glycerol. The removal of impurities was confirmed by measuring the pH of water. The biodiesel was dried by heating it to a temperature of 110°C and allowed overnight for evaporation and cooling. The final product was weighed to determine the biodiesel yield.

2.4. Analytical and Test Methods. The mean molecular weight, saponification number (SN), iodine value (IV), and cetane number (CN) were determined from the fatty acid composition of oil using (1), (2), (3), and (4); respectively [18, 31]:

\[
MW_{oil} = 3 \times \sum (MW_i \times x_i) + 38, \quad (1)
\]

where \(MW_{oil}\) stands for molecular weight of SASO and SABD and \(MW_i\) and \(x_i\) stand for molecular weight and mass fraction of \(i^{th}\) fatty acid; respectively,

\[
SN = \sum \left( 560 \times \frac{A_i}{MW_i} \right), \quad (2)
\]

\[
IV = \sum \left( 254 \times D \times \frac{A_i}{MW_i} \right), \quad (3)
\]

\[
CN = 46.3 + \frac{5458}{SN} - 0.225 \times IV, \quad (4)
\]

where \(A_i\) is the percentage, \(D\) is the number of double bonds, and \(MW_i\) is the molecular mass of each component.

The fuel properties of sugar apple seed oil (SASO) and sugar apple biodiesel (SABD) were determined as per the ASTM standards as given in Table 2.

In this paper the biodiesel yield was calculated using

\[
\text{Biodiesel yield} = \frac{m_{\text{biodiesel}}}{m_{\text{oil}}} \times 100, \quad (5)
\]

where \(m_{\text{biodiesel}}\) is the weight of SABD after purification and \(m_{\text{oil}}\) is the weight of SASO.

### 3. Results and Discussion

#### 3.1. Oil Content of Sugar Apple Seeds

The oil extracted from the mechanical expeller was weighed after filtering; it was found that the sugar apple seeds contain moderate quantity of oil, 24.5 w/w % oil, and thus it can be suitable feedstock for the production of biodiesel.

#### 3.2. Fatty Acid Composition Analysis

Generally three main types of fatty acids are present in triglyceride and they are saturated, monounsaturated, and polyunsaturated. The quality of biodiesel will be affected by the fatty acid composition of oil, preferably the vegetable oil should have low saturated and low polyunsaturated fatty acid composition, and the composition of monounsaturated fatty acid should be high. Table 1 shows the fatty acid composition of SASO and it contains predominant amount of monounsaturated fatty acid composition, that is, 39.72%, followed by 31.56% of polyunsaturated fatty acid and 24.07% of saturated fatty acids. The major fatty acids present in the SASO were oleic acid, 39.72%, linoleic acid, 29.13%, palmitic acid, 17.79%, and stearic acid, 4.29%. Thus the SASO can be classified as oleic-linoleic oil.

#### 3.3. Physicochemical Properties of SASO and SABD

The physical and chemical properties of SASO and SABD were determined as per the ASTM standard test procedures and tabulated in Table 3. The iodine value of SASO is 118 mgI₂/g, as the iodine value is higher, which indicates the unsaturation of SASO. The heating of these higher fatty acids results in polymerization of glycerides, which necessitates the limitation of unsaturated fatty acids; otherwise, it leads to formation of deposits and deterioration of lubricating oil. The saponification of SASO was 192, which indicates that the SASO is normal triglyceride and useful in production of soaps. The FFA (free fatty acid) content of oil is 0.965%, as it is less than the biodiesel that can be produced using single stage transesterification process, that is, by base-catalyzed transesterification process. The flash points of SASO, SABD, and diesel were 235, 161, and 54 degrees Celsius, respectively. The flash points of SASO and SABD are found to be much higher in comparison with diesel, which helps in safe storage and transportation. The densities of SASO and SABD were higher than that of diesel, which may be due to the presence of higher molecular weight triglycerides. The kinematic viscosity of SASO was found to be 42.63 mm²/s, which is much higher than that of diesel; hence the direct use of SASO may lead to poor combustion, untimely wear of fuel pumps, and injector. The viscosity of SASO was reduced by converting it to biodiesel and it was found to be 5.90 mm²/s, which is within the limits of standard specification for biodiesel fuel. Calorific values of SASO, SABD, and diesel were found to be 37.95, 40.48, and 43.00 MJ/kg, respectively. The calorific values of studied oil and biodiesel are found to be lower than that of diesel, which may be due to the difference in chemical composition or presence of oxygen molecule in molecular structure of oil. The other parameters, that is, cetane number, calculated cetane index, sulfated ash, carbon residue, copper strip corrosion, and distillation temperature, were found to be within the limits of standard specifications for biodiesel fuel.
Table 3: Physiochemical properties of SASO and SBD in comparison with commercially available diesel and ASTM standard specifications for biodiesel fuel.

<table>
<thead>
<tr>
<th>Property</th>
<th>SASO</th>
<th>SABD</th>
<th>Commercially available diesel</th>
<th>Standards specifications for biodiesel fuel, ASTM D6751-09a</th>
</tr>
</thead>
<tbody>
<tr>
<td>Iodine value (mg I₂/g)</td>
<td>118</td>
<td>—</td>
<td>—</td>
<td>—</td>
</tr>
<tr>
<td>Saponification number</td>
<td>192</td>
<td>—</td>
<td>—</td>
<td>—</td>
</tr>
<tr>
<td>Acid number (mg KOH/g)</td>
<td>1.93</td>
<td>0.34</td>
<td>—</td>
<td>0.50 max</td>
</tr>
<tr>
<td>Flash point (°C)</td>
<td>235</td>
<td>161</td>
<td>54</td>
<td>130 min</td>
</tr>
<tr>
<td>Density (kg/m³)</td>
<td>910</td>
<td>865</td>
<td>830</td>
<td>870–900</td>
</tr>
<tr>
<td>Kinematic viscosity (mm²/s) at 40°C</td>
<td>42.63</td>
<td>5.90</td>
<td>2.4</td>
<td>1.9–6.0</td>
</tr>
<tr>
<td>Calorific value (MJ/kg)</td>
<td>37.95</td>
<td>40.48</td>
<td>43.00</td>
<td>—</td>
</tr>
<tr>
<td>Cetane number</td>
<td>47.93</td>
<td>—</td>
<td>—</td>
<td>47 min</td>
</tr>
<tr>
<td>Calculated cetane index</td>
<td>—</td>
<td>53.57</td>
<td>50.98</td>
<td>47 min</td>
</tr>
<tr>
<td>Sulfated ash (w/w, %)</td>
<td>—</td>
<td>0.0015</td>
<td>—</td>
<td>0.020 max</td>
</tr>
<tr>
<td>Carbon residue (w/w, %)</td>
<td>0.697</td>
<td>0.033</td>
<td>—</td>
<td>0.050 max</td>
</tr>
<tr>
<td>Copper strip corrosion</td>
<td>—</td>
<td>3 h, 50°C/1a</td>
<td>—</td>
<td>No. 3 max</td>
</tr>
<tr>
<td>Distillation temperature, 90% recovered (°C)</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>IBP</td>
<td>338</td>
<td>161</td>
<td>360 max</td>
<td></td>
</tr>
<tr>
<td>10%</td>
<td>340</td>
<td>202</td>
<td></td>
<td></td>
</tr>
<tr>
<td>20%</td>
<td>342</td>
<td>215</td>
<td></td>
<td></td>
</tr>
<tr>
<td>50%</td>
<td>348</td>
<td>254</td>
<td></td>
<td></td>
</tr>
<tr>
<td>90%</td>
<td>356</td>
<td>348</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Molecular weight (g/mol)</td>
<td>872.50</td>
<td>—</td>
<td>—</td>
<td></td>
</tr>
</tbody>
</table>

3.4. Effect of Catalyst Concentration on Biodiesel Production.

The catalyst concentration is one of the most significant parameters which affects the biodiesel yield. Figure 3 shows the effect of NaOH catalyst concentration on the yield of biodiesel; during the process the other parameters are kept constant. It is observed that the biodiesel yield increases when catalyst concentration is increased from 0.25 w/w % to 0.50 w/w % and decreases when increased from 0.50 w/w % to 0.75 w/w %. The decrease in yield at 0.25 w/w % of catalyst concentration may be due to incomplete reaction and at 0.75 w/w % of catalyst concentration may be due to the fact that the higher amount of catalyst concentration favors the saponification reaction; thus further increase in catalyst concentration was not studied. From the present investigation, optimum amount of catalyst concentration was found to be 0.50 w/w % with 90.69% biodiesel yield.

3.5. Effect of Reaction Time on Biodiesel Production.

In order to study the effect of reaction time on production of biodiesel, the transesterification reaction was carried out by varying the reaction time as 45, 60, 75, and 90 minutes and by keeping other process parameters constant. Figure 4 shows the effect of reaction time on the yield of biodiesel. Varying the reaction time from 45 to 60 minutes and 60 to 75 minutes, the percentage yield of biodiesel is increased. The percentage yield of biodiesel is decreased with further increase in reaction time from 75 to 90 minutes; this may be due to formation of more amount of soap. The highest percentage yield of biodiesel was noticed when the reaction time was 75 minutes and it is found to be 95.15%.

3.6. Effect of Reaction Temperature on Biodiesel Production.

Further experiments were conducted by keeping the reaction temperature at 40, 50, 60, and 75°C in order to study the effect of reaction temperature. The catalyst concentration of 0.5 w/w % and reaction time of 75 minutes were maintained. Figure 5 shows the effect of reaction temperature on biodiesel...
yield. As the methanol boils at 65°C, varying the reaction temperature from 40 to 60°C the biodiesel yield is increased and biodiesel yield was decreased at temperature of 70°C; this may be attributed to occurrence of saponification reaction at higher temperature. The highest biodiesel yield is found to be 95.15% at 60°C.

4. Conclusions

The purpose of the present study was to evaluate the sugar apple seed oil as a potential raw material for the production of biodiesel and to assess its feasibility for the replacement of petroleum fuel. The sugar apple seed oil was converted into biodiesel successfully by transesterification process and following conclusions were drawn.

(1) The sugar apple oil was converted to biodiesel by single stage base-catalyzed transesterification process without any pretreatment as the FFA content is found to be less than 1%.

(2) The optimized process parameters are catalyst concentration of 0.5 w/w%, reaction time of 75 minutes and reaction temperature of 60°C with alcohol to oil molar ratio of 6:1, and constant stirrer speed. The biodiesel yield was found to be 95.15% at the optimized process parameters.

(3) The physical and chemical properties of biodiesel produced were found to be close to those of diesel fuel and also they meet the ASTM standard specifications for biodiesel.

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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References


