Research Article

Adaptive Sliding Mode Control of Uncertain High-Order Nonholonomic Systems with Unknown Control Coefficients

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This paper investigates the global stabilization problem for a class of high-order nonholonomic systems with unknown control coefficients and uncertain nonlinearities. An adaptive sliding mode control (SMC) law based on a constructive manipulation is proposed by adding a power integrator technique. A switching control strategy is employed in the control scheme to overcome the uncontrollability problem associated with the nonholonomic systems. The designed sliding mode controller could guarantee the attractiveness of the sliding surface \( S = 0 \) and achieve the asymptotical convergence of the state as well as the boundedness of the estimated parameters. A simulation example is provided to demonstrate the effectiveness of the proposed scheme.

1. Introduction

Nonholonomic control system as a particular class of nonlinear systems represents a wide class of mechanical systems with nonholonomic (nonintegrable) constraints. The stabilization control for nonholonomic control systems is a formidable problem in the nonlinear control area [1], because the nonholonomic systems cannot be asymptotically stabilized by means of known linear and nonlinear control methods. The difficulty of controlling this class of systems lies in the fact that nonholonomic systems do not satisfy Brockett's necessary conditions for stability as shown in [2]. In the past two decades, many interesting approaches have been proposed to overcome the stabilization obstruction associated with nonholonomic systems, including the smooth time-varying feedback, discontinuous feedback, and nonsmooth time-varying homogeneous feedback; see [1] and references therein.

Variable structure control (VSC) has been shown to be robust in the presence of system variations and external disturbances. During the past few years, the VSC strategy has been also applied to the nonholonomic system control; see [3–9]. It is noted in [5, 6]; a combined adaptive/variable structure control approach was presented for a class of uncertain nonlinear systems. The proposed method not only ensures the convergence to the sliding surface \( S = 0, \dot{S} = 0 \), but also retains the asymptotical stability of the classical backstepping procedure. On the basis of the previously proposed control scheme, the so-called second order sliding mode control was exploited for nonholonomic systems in [7]. The work [8] further extended this result to a class of nonholonomic ones with unknown parameters and uncertain nonlinear drifts. In [9], the adaptive SMC problem is studied for a class of perturbed nonholonomic systems which can be transformed into the chained form with uncertain nonlinear drifts.

It should be noted that the results listed previously are all focused on the nonholonomic systems with the affine control variables. High-order nonholonomic systems which include the standard chained form systems as a special case present a new challenge for nonlinear feedback control, since this class of nonholonomic control systems is neither stabilizable by time-invariant continuous state feedback nor affine in the control inputs [10]. By means of adding a power integrator developed in [11], the work [12] first investigated a class of high-order nonholonomic systems in the so-called power chained form. As the further development of this approach, [13] studied a class of uncertain nonholonomic control systems with nonlinear drifts. The recent work [14] removed the assumption of the control gain signs. Reference [15] proposed an adaptive stabilization scheme for a class of high-order
chained nonholonomic systems without nonlinear drifts in the case of unknown control coefficients.

Motivated by the recent progress in the feedback design for nonholonomic systems, this paper will investigate the global stabilization problem for a class of high order nonholonomic systems with unknown control coefficients and uncertain nonlinearities. A combined backstepping and adaptive SMC methodology developed in [6, 16] will be applied to the control design procedure, and adding a power integrator technique is used to deal with the nonaffine control inputs. The tuning function technique presented in [17] is also introduced. We employ a switching control strategy to overcome the stabilization burden associated with the nonholonomic systems.

The paper is organized as follows. Section 2 presents the problem statement. Section 3 gives the SMC design scheme for \( x_0(t_0) \neq 0 \). The switching control strategy and the simulation example are shown in Sections 4 and 5, respectively. Section 6 gives some concluding remarks.

2. Problem Statement

In this paper, we consider the following class of high-order nonholonomic systems:

\[
\dot{x}_0 = d_0(t) u_{0}^p, \\
\dot{x}_1 = d_1(t) x_0^p u_0^q + \phi_1(x_0, x_1), \\
\vdots \\
\dot{x}_n = d_{n-1}(t) x_{n-1}^p u_{n-1}^q + \phi_{n-1}(x_0, x_1, \ldots, x_{n-1}), \\
\dot{x}_n = \beta(t) u^n + \phi_n(x_0, x_n),
\]

where \((x_0, x_1, \ldots, x_n)^T \in \mathbb{R}^{n+1}\) are the states, \(u_0\) and \(u\) are two control inputs, \(d_i(t) (i = 0, \ldots, n-1)\), \(\beta(t)\) are nonzero functions, and \(\phi_i : \mathbb{R}^{n+1} \to \mathbb{R}\) are smooth functions satisfying \(\phi_i(0, \ldots, 0) = 0\) \((i = 1, \ldots, n)\). The functions \(d_i(t) (i = 0, 1, \ldots, n-1)\), \(\beta(t)\) and \(\phi_i(x_0, x_1, \ldots, x_i)\) \((i = 1, \ldots, n)\) represent the control coefficients and the uncertain nonlinearities, respectively. It is further assumed that \(\beta(t)\) is bounded for \(t \geq 0\), \(p_i \geq 1\) \((i = 0, \ldots, n)\) are odd integers, and \(q_k\) \((k = 1, \ldots, n-1)\) are positive integers.

In the rest of this paper, an adaptive sliding mode controller \(u\) will be first designed for system (1) such that, given any initial state \((x_0(0), x(0)) \in \Omega_0 = \{(x_0, x) | x_0 \neq 0\}\), the closed-loop system is asymptotically stabilized. Then, a switching control strategy is proposed, which guarantees that all the signals are bounded for the initial conditions \((x_0(0), x(0)) \in \mathbb{R}^{n+1}\).

To this end, we make the following assumptions regarding system (1).

Assumption 1. For each \(\phi_i (i = 1, \ldots, n-1)\) in (1), there exist known smooth functions \(\phi_i\) satisfying

\[
\phi_i (x_0, x_1, \ldots, x_i) \leq |x_1| + \cdots + |x_i| \phi_i (x_0, x_1, \ldots, x_i),
\]

Assumption 2. For each \(0 \leq i \leq n-1\), the sign of \(d_i(t)\) is positive, and there are unknown positive constants \(\theta_1\) and \(\theta_2\) such that

\[
\theta_1 \leq d_i(t) \leq \theta_2, \quad \forall t \geq 0.
\]

Assumption 3. There is a known smooth function \(\psi(x_0, x)\) such that \(|\phi_i(x_0, x)| \leq \psi(x_0, x)\), for all \((x_0, x) \in \mathbb{R}^{n+1}\).

Next, we introduce a lemma which is crucial in establishing the main results of this paper.

Lemma 4 (Young’s Inequality). If the constants \(p, q > 1\) and satisfy \((p-1)(q-1) = 1\), then for all \(\varepsilon > 0\) and \((x, y) \in \mathbb{R}^2\), there holds

\[
xy \leq \frac{\varepsilon^p}{p} |x|^p + \frac{1}{q\varepsilon^q} |y|^q.
\]

3. SMC Applied to Backstepping Design

In this part, we firstly assume that \(x_0(t_0) \neq 0\) for the system (1). The case of \(x_0(t_0) = 0\) will be discussed in the subsequent section.

For \(x_0(t_0) \neq 0\), take \(u_0\) as follows:

\[
u_0 = -x_0.
\]

Choose the Lyapunov function \(V_0(x_0) = (1/2)x_0^2\), then the time derivative of \(V_0(x_0)\) along the first equation of (1) satisfies

\[
\dot{V}_0 = -d_0(t) x_0^{p+1} \leq -\theta_1 x_0^{p+1} \leq 0.
\]

Considering \(p_0\) is an odd integer, it can be concluded that \(x_0\)-subsystem is asymptotically stable. In addition, \(x_0(t, x_0(t_0))\) cannot converge to zero in finite time if \(x_0(t_0) \neq 0\).

In order to carry out the control design, we introduce the following input-state scaling discontinuous transformation defined by

\[
\begin{align*}
z_1 &= \frac{x_1}{u_0}, \\
z_2 &= \frac{x_2}{u_0}, \\
& \vdots \\
z_n &= \frac{x_n}{u_0},
\end{align*}
\]

with \(r_i = q_i + p_i r_{i+1}, r_n = 0, i = 1, \ldots, n-1\).

Under the control law (5) and the transformation (7), the \(x\)-subsystem can be transformed into

\[
\begin{align*}
\dot{z}_1 &= d_1(t) z_1^{p_1} + d_0(t) r_1 x_0^{p_0-1} z_1 + \phi_1(x_0, z_1), \\
\vdots \\
\dot{z}_{n-1} &= d_{n-1}(t) z_{n-1}^{p_{n-1}} + d_0(t) r_{n-1} x_0^{p_0-1} z_{n-1} + \phi_{n-1}(x_0, z_1, \ldots, z_{n-1}), \\
\dot{z}_n &= \beta(t) u^n + \phi_n(x_0, z),
\end{align*}
\]

where \(\phi_i(x_0, z_1, \ldots, z_i) = \phi_i(x_0, x_1, \ldots, x_i)/u_0^i, i = 1, \ldots, n.\)
To invoke the backstepping method, we define the error variables $\xi_1, \ldots, \xi_n$ as follows:

$$
\xi_1 = z_1,
$$

$$
\xi_2 = z_2^{p_1} - \alpha_1^{p_1},
$$

$$
\vdots
$$

$$
\xi_n = z_n^{p_n} - \alpha_n^{p_n},
$$

(9)

where $\alpha_1, \ldots, \alpha_{n-1}$ are the virtual controllers and given by

$$
\alpha_i^{p_i-r_i} (x_0, z_1, \ldots, z_i, \Theta) = -\xi_i \beta_i (x_0, z_1, \ldots, z_i, \Theta),
$$

(10)

where $\beta_i(x_0, z_1, \ldots, z_i, \Theta) > 0$ ($i = 1, \ldots, n-1$) are some smooth functions and $\Theta$ is the estimation of unknown parameter $\Theta = (1 + \theta_2^r)^{1/2}$.

**Lemma 5.** For every $1 \leq i \leq n - 1$, there are smooth nonnegative functions $\overline{\phi}_i(x_0, z_1, \ldots, z_i)$ satisfying

$$
\overline{\phi}_i(x_0, z_1, \ldots, z_i) \leq (z_1^2 + \cdots + z_i^2) \overline{\phi}_i(x_0, z_1, \ldots, z_i).
$$

(11)

**Proof.** According to Assumption 1, it can be derived that

$$
||x_i||^r \leq \sum_{k=1}^{n-i} (z_{i+k}^2 + \cdots + z_{n-1}^2) \overline{\phi}_i(x_0, x_1, \ldots, x_{i+1})
$$

(12)

In view of $r_k \geq r_k$ ($k = 1, \ldots, i-1$), one gets (II) with $\overline{\phi}_i = (1 + |u_0|^{r-r_i}) \overline{\phi}_i$.

In what follows, we give the SMC control design procedure using the recursive method.

**Step 1.** Choose the candidate Lyapunov function $V_1 = (n/2\theta_1) x_0^{p_1} + (1/2) \Theta^2$ for this step, where $\Theta = \Theta - \hat{\Theta}$ is the parameter estimation error, and $\gamma_i > 0$ is the design gain. Then, along the trajectories of system (8), we have

$$
V_1 = -(n-i+1) x_0^{p_1} - n-i + \sum_{k=1}^{n-i} (z_k^2 + d_0(t) r_1 x_0^{p_0} - \alpha_{i+1}^{p_{i+1}})
$$

(13)

Choose the virtual control

$$
\alpha_1^{p_1} (x_0, z_1, \Theta) = -\xi_1 \rho_1 (x_0, z_1) \sqrt{1 + \Theta^2}
$$

(14)

and one gets

$$
V_1 \leq -(n-i+1) x_0^{p_1} - n-i + \sum_{k=1}^{n-i} (z_k^2 + d_0(t) r_1 x_0^{p_0} - \alpha_{i+1}^{p_{i+1}})
$$

(15)

(16)

**Step 2** ($2 \leq i < n$). Suppose that at **Step $i-1$**, there is a positive definite and proper Lyapunov function $V_{i-1}$ satisfying

$$
V_{i-1} \leq -(n-i+2) x_0^{p_i+1} - \sum_{k=1}^{n-i} \frac{1}{\gamma_i} z_k^2 + d_0(t) x_0^{p_0} - \alpha_{i+1}^{p_{i+1}}
$$

(17)

Let

$$
V_i = V_{i-1} + W_i
$$

(18)
Then \( V_i \) is a \( C^2 \), positive definite and proper function such that
\[
\dot{V}_i = V_{i-1} + \frac{\partial W_i}{\partial x_0} \dot{x}_0 + \sum_{k=1}^{i-1} \frac{\partial W_i}{\partial z_k} \dot{z}_k + \frac{\partial W_i}{\partial \Theta} \dot{\Theta}
\]
\[
\leq -(n - i + 2) x_{0}^{p_{0}+1} - n - i + 1 \sum_{k=1}^{i-1} \xi_k^2 + \frac{i-1}{\theta_1} \sum_{k=1}^{i-1} \xi_k^2
\]
\[- \sum_{k=1}^{i-1} \xi_k^2 + d_{i-1}(t) \xi_k^{2-(1/p_i-\cdot-p_{i-1})} (z_{i-1} - \alpha_{i-1}^{p_{i-1}})
\]
\[+ \frac{\partial W_i}{\partial z_0} \dot{x}_0 + \sum_{k=1}^{i-1} \frac{\partial W_i}{\partial z_k} \dot{z}_k
\]
\[+ \xi_k^{2-(1/p_i-\cdot-p_{i-1})} (\phi_i + d_0(t) r_i x_0^{p_{i-1}} z_i)
\]
\[
+ d_i(t) \xi_k^{2-(1/p_i-\cdot-p_{i-1})} z_{i-1}^{p_{i-1}}
\]
\[
+ \left( \tau_{i-1} - \frac{\partial}{\partial \Theta} \right) \left( \frac{\partial}{\partial \Theta} \frac{\partial W_i}{\partial z_0} \dot{x}_0 - \sum_{k=1}^{i-1} \frac{\partial W_i}{\partial z_k} \dot{z}_k + \frac{\partial W_i}{\partial \Theta} \dot{\Theta} \right)
\]
(19)

With the help of Young’s Inequality, we can obtain
\[
d_{i-1}(t) \xi_k^{2-(1/p_i-\cdot-p_{i-1})} (z_{i-1} - \alpha_{i-1}^{p_{i-1}})
\leq 2^{1-(1/p_i-\cdot-p_{i-1})} \theta_2 \xi_k^{2-(1/p_i-\cdot-p_{i-2})} |s_k|^{1/p_i-\cdot-p_{i-2}}
\leq \frac{1}{4 \theta_1} \xi_k^2 + \xi_k^{2+(p_i-\cdot-p_{i-1})-3} \frac{p_{i-1}^{p_{i-1}-1}}{p_{i-1} \cdot \cdot \cdot p_{i-2}}
\times \left( \frac{4 p_{i-1} \cdot \cdot \cdot p_{i-2} - 2}{p_{i-1} \cdot \cdot \cdot p_{i-2}} \right) \frac{p_{i-1}^{p_{i-1}-1}}{p_{i-1} \cdot \cdot \cdot p_{i-2} - 1} \frac{p_{i-1}^{p_{i-1}-1}}{p_{i-1} \cdot \cdot \cdot p_{i-2}}
\leq \frac{1}{4 \theta_1} \xi_k^2 + \theta_i \xi_k^{2+(p_i-\cdot-p_{i-1})-3} \left( \frac{4 p_{i-1} \cdot \cdot \cdot p_{i-2} - 2}{p_{i-1} \cdot \cdot \cdot p_{i-2}} \right) \frac{p_{i-1}^{p_{i-1}-1}}{p_{i-1} \cdot \cdot \cdot p_{i-2}}
\leq \frac{1}{4 \theta_1} \xi_k^2 + \theta_i \xi_k^{2+(p_i-\cdot-p_{i-1})-3} \left( \frac{4 p_{i-1} \cdot \cdot \cdot p_{i-2} - 2}{p_{i-1} \cdot \cdot \cdot p_{i-2}} \right) \frac{p_{i-1}^{p_{i-1}-1}}{p_{i-1} \cdot \cdot \cdot p_{i-2}}
\]
(20)

where \( \phi_{i1} \) and \( \phi_{ij} \) (\( i = 2, \ldots, n; j = 1, \ldots, 5 \)) given later are smooth nonnegative functions.

From (18), we get
\[
\frac{\partial W_i}{\partial x_0} \dot{x}_0
\]
\[= \left( \frac{2 - \frac{1}{p_{i-1}}}{p_{i-1}} \right) d_0(t) x_0^{p_{i-1}-p_{i-1} p_{i-1}}
\times \left( \frac{4 p_{i-1} \cdot \cdot \cdot p_{i-2} - 2}{p_{i-1} \cdot \cdot \cdot p_{i-2}} \right) \frac{p_{i-1}^{p_{i-1}-1}}{p_{i-1} \cdot \cdot \cdot p_{i-2}}
\times \left( \frac{4 p_{i-1} \cdot \cdot \cdot p_{i-2} - 2}{p_{i-1} \cdot \cdot \cdot p_{i-2}} \right) \frac{p_{i-1}^{p_{i-1}-1}}{p_{i-1} \cdot \cdot \cdot p_{i-2}}
\]
\[\leq \left( \frac{4 - \frac{2}{p_{i-1}}}{p_{i-1}} \right) \frac{\partial x_0^{p_{i-1}-p_{i-1}}}{\partial x_0}
\]
\[
\begin{align*}
&\leq \left(4 - \frac{2}{p_1 \cdots p_{i-1}}\right) |\xi_i| \\
&\times \sum_{k=1}^{i-1} p_1 \cdots p_{k-1} \beta_k \\
&\times \left( \theta_2 z_k^{p_{i-k}} + \theta_2 (1 + r_k x_0^{p_{i-k}}) z_k^{p_{i-k}} + (|\xi_i|^{p_{i-k}} - \cdots + |\xi_{i-1}|^{p_{i-k}}) \right) \\
&\quad + k \left| \xi_k \right| z_k^{p_{i-k}} \\
&\quad + \left(4 - \frac{2}{p_1 \cdots p_{i-1}}\right) \left| \xi_i \right| \left( \sum_{k=1}^{i-1} \left| \xi_i \right| \left( \sum_{l=1}^{i} \frac{\partial \beta_l}{\partial z_k} \left| \dot{z}_{i-l} \right| \right) \right) \\
&\leq \left(4 - \frac{2}{p_1 \cdots p_{i-1}}\right) |\xi_i| \\
&\times \left( \theta_2 |\xi_{i-1}| + \theta_2 (\beta_k + 1 + r_k x_0^{p_{i-k}}) |\xi_k| \right) \\
&\quad + \theta_2 (1 + r_k x_0^{p_{i-k}}) \beta_k - 1 |\xi_{k-1}| \\
&\quad + \sum_{l=1}^{i-1} 2^{p_{i-k-1} - 1} \left( |\xi_l|^{p_{i-k-1}} + |\xi_{l-1}\beta_{i-1}|^{p_{i-k-1}} \right) \\
&\quad \times \bar{\varphi}_l + k \left| \xi_k \right| \left( |\xi_k| + \beta_k + 1 |\xi_{k-1}| \right) \bar{\varphi}_k \\
&\quad + \left(4 - \frac{2}{p_1 \cdots p_{i-1}}\right) \left| \xi_i \right| \left( \sum_{k=1}^{i-1} \left| \xi_i \right| \left( \sum_{l=1}^{i} \frac{\partial \beta_l}{\partial z_k} \left| \dot{z}_{i-l} \right| \right) \right) \\
&\leq \frac{1}{4 \theta_1} \sum_{k=1}^{i-1} \xi_k^2 + \xi_i^2 \sum_{k=1}^{i-1} \frac{1}{4 \theta_1} \left(4 - \frac{2}{p_1 \cdots p_{i-1}}\right) \left| \xi_i \right| \\
&\times \sum_{k=1}^{i-1} (p_1 \cdots p_{k-1} \beta_k)^2 \\
&\quad \times \left( \theta_2 \left(2 + 2 \beta_k + 2 r_k x_0^{p_{i-k}} \right)^2 \right) \\
&\quad + \left( \beta_k + r_k x_0^{p_{i-k}} \right)^2 \beta_k \right) \\
&\quad + 2 \sum_{l=1}^{i-1} \left( 2^{p_{i-k-1} - 1} - 2^{\bar{\varphi}_k} \right) \left\{ \xi_k^{2p_{i-k-1} - 1} - 2^{p_{i-k-1} - 1} \right\} \\
&\quad \times \beta_k^2 + \beta_{i-1} \left( \beta_{i-1} \xi^2 \right) \\
&\quad + 2k^2 \left( \bar{\varphi}_l + \beta_k^2 \bar{\varphi}_{k+1} \right) \\
&\quad + \left( \beta_k + r_k x_0^{p_{i-k}} \right)^2 \beta_k \right) \\
&\quad + 2k^2 \left( \bar{\varphi}_l + \beta_k^2 \bar{\varphi}_{k+1} \right) \\
&\quad + \left(4 - \frac{2}{p_1 \cdots p_{i-1}}\right) \sum_{k=1}^{i-1} k \left( \frac{\partial \beta_k}{\partial z_l} \left| \dot{z}_{i-l} \right| \right)^2 \bar{\varphi}_l.
\end{align*}
\]
\[ V_i = - (n - i + 1) x_0^{p_{i+1}} - \frac{n - i + 1}{\theta_1} \sum_{k=1}^{i-1} \beta_k^2 + \theta_1 \Theta x_i^2 \left( n - i + 2 + \theta_1 + 3 \right) + \theta_3 + \theta_4 \]
\[ + d_j(t) (\tau_i^{2-1/p_i-1})^2 \rho_{i+1} \]
\[ + \left( \tau_{i-1} - \frac{\Theta}{\theta_1} \right) \left( \frac{\theta_1}{\tau_i} - \sum_{k=2}^{i-1} \frac{\partial W_k}{\partial \Theta} \right) + \frac{\partial W_i}{\partial \Theta} \].

Denote
\[ \rho_i(x_0, z_1, \ldots, z_i, \Theta) = n - i + 2 + \theta_1 + \theta_3 + \theta_4, \]
\[ \tau_i = \tau_{i-1} + y_i \xi_i^2 \rho_i(x_0, z_1, \ldots, z_i, \Theta). \]

Substituting (26) into (25), we have
\[ V_i \leq - (n - i + 1) x_0^{p_{i+1}} - \frac{n - i + 1}{\theta_1} \sum_{k=1}^{i-1} \xi_k^2 
\[ + \frac{3}{4 \theta_1} \sum_{k=1}^{i-1} \xi_k^2 + \theta_1 \Theta x_i^2 \left( n - i + 2 + \theta_1 + \theta_2 \right) + \theta_3 + \theta_4 \]
\[ + d_j(t) (\tau_i^{2-1/p_i-1})^2 \rho_{i+1} \]
\[ + \left( \tau_{i-1} - \frac{\Theta}{\theta_1} \right) \left( \frac{\theta_1}{\tau_i} - \sum_{k=2}^{i-1} \frac{\partial W_k}{\partial \Theta} \right) + \frac{\partial W_i}{\partial \Theta} \].

According to (26), there holds
\[ \sum_{k=2}^{i-1} \frac{\partial W_k}{\partial \Theta} \left( \tau_{i-1} - \tau_i \right) + \frac{\partial W_i}{\partial \Theta} \tau_i \]
\[ \leq \sum_{k=2}^{i-1} y_i \left( 4 - \frac{2}{\beta_{k-1} p_{k-1}} \right) \frac{\partial \rho_{k-1}}{\partial \Theta} \left[ \beta_k \xi_k^2 \rho_k \right] 
\[ + y_i \left( 4 - \frac{2}{\beta_{k-1} p_{k-1}} \right) \frac{\partial \rho_{k-1}}{\partial \Theta} \left[ \beta_k \xi_k^2 \rho_k \right] \]
\[ \leq \frac{1}{4 \theta_1} \sum_{k=1}^{i-1} \xi_k^2 + \frac{1}{\theta_1} \xi_i^2 \]
\[ + \frac{3}{4 \theta_1} \sum_{k=1}^{i-1} \xi_k^2 + \theta_1 \Theta x_i^2 \left( n - i + 2 + \theta_1 + \theta_2 \right) + \theta_3 + \theta_4 \]
\[ + d_j(t) (\tau_i^{2-1/p_i-1})^2 \rho_{i+1} \]
\[ + \left( \tau_{i-1} - \frac{\Theta}{\theta_1} \right) \left( \frac{\theta_1}{\tau_i} - \sum_{k=2}^{i-1} \frac{\partial W_k}{\partial \Theta} \right) + \frac{\partial W_i}{\partial \Theta} \].

Substituting (20)–(24) into (19), we have
\[ V_i \leq - (n - i + 1) x_0^{p_{i+1}} - \frac{n - i + 1}{\theta_1} \sum_{k=1}^{i-1} \xi_k^2 + \theta_1 \Theta x_i^2 \left( n - i + 2 + \theta_1 + \theta_2 \right) + \theta_3 + \theta_4 \]
\[ + d_j(t) (\tau_i^{2-1/p_i-1})^2 \rho_{i+1} \]
\[ + \left( \tau_{i-1} - \frac{\Theta}{\theta_1} \right) \left( \frac{\theta_1}{\tau_i} - \sum_{k=2}^{i-1} \frac{\partial W_k}{\partial \Theta} \right) + \frac{\partial W_i}{\partial \Theta} .
\]
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\[ \frac{1}{4\theta_1} \sum_{k=1}^{i-1} \xi_k^2 + \frac{1}{\theta_1} \xi_i^2 + \theta_1 \xi_i^2 \varepsilon_0 \left( x_0, z_1, \ldots, z_p, \bar{\Theta} \right). \]

As a result, (27) can be further transformed into

\[ \dot{V}_i \leq -(n - i + 1) \alpha_{i-1}^0 - \frac{n - i}{\theta_1} \sum_{k=1}^{i} \xi_k^2 \]

\[ - \sum_{k=1}^{i} \xi_k^2 + d_i \left( t \right) \xi_i^{2(1/p_i - 1)} z_{i+1}^2 \]

\[ + \theta_1 \xi_i^2 \left( \rho_\Theta + \varepsilon_0 \right) + \left( \tau_i - \bar{\Theta} \right) \left( \frac{\partial W_k}{\partial \Theta} - \sum_{k=2}^{i} \frac{\partial W_k}{\partial \Theta} \right). \]

Choose the ith virtual control law

\[ \alpha_i^{p_i - p_i} \left( x_0, z_1, \ldots, z_i, \bar{\Theta} \right) \]

\[ = -\xi_i \left( \rho_\Theta \left( x_0, z_1, \ldots, z_i, \bar{\Theta} \right) \right) v_1 + \varepsilon_0 \left( x_0, z_1, \ldots, z_i, \bar{\Theta} \right) \]

and then

\[ \dot{V}_i \leq -(n - i + 1) \alpha_{i-1}^0 - \frac{n - i}{\theta_1} \sum_{k=1}^{i} \xi_k^2 \]

\[ - \sum_{k=1}^{i} \xi_k^2 + d_i \left( t \right) \xi_i^{2(1/p_i - 1)} z_{i+1}^2 \]

\[ + \left( \tau_i - \bar{\Theta} \right) \left( \frac{\partial W_k}{\partial \Theta} - \sum_{k=2}^{i} \frac{\partial W_k}{\partial \Theta} \right). \]

Step n. Let

\[ V_n = V_{n-1} + \int_{x_{n-1}}^{x_n} \left( s^{p_{n-1} - p_{n-1}} - \alpha_{n-1}^{p_{n-1} - p_{n-1}} \right)^{2(1/p_{n-1} - p_{n-1})} ds \]

\[ + \frac{1}{2\gamma_2}, \]

where

\[ \dot{V}_{n-1} \leq -2 x_{n-1}^{p_{n-1} - 1} - \frac{n}{\theta_1} \sum_{k=1}^{n-1} \xi_k^2 \]

\[ - \sum_{k=1}^{n-1} \xi_k^2 + d_{n-1} \left( t \right) \xi_{n-1}^{2(1/p_{n-1} - 1)} \left( z_{n-1}^{p_{n-1} - 1} - \alpha_{n-1}^{p_{n-1} - 1} \right) \]

\[ + \left( \tau_{n-1} - \bar{\Theta} \right) \left( \frac{\partial W_k}{\partial \Theta} - \sum_{k=2}^{n-1} \frac{\partial W_k}{\partial \Theta} \right). \]

\[ y_2 > 0 \text{ is an arbitrary constant, } \bar{\Lambda} = \Lambda - \bar{\Lambda} \text{ with } \bar{\Lambda} \text{ is the estimate of the unknown constant } \Lambda = \max\{\theta_2, \theta_1^{2(p_2 - p_1 - p_{n-1})} \}. \]

Choose the parameter update law as

\[ \dot{\lambda} = r_{n-1} = \sum_{k=1}^{n-1} y_1^2 p_k, \]

and then

\[ V_n = V_{n-1} + \frac{\partial W_n}{\partial x_0} + \sum_{k=1}^{n-1} \frac{\partial W_n}{\partial z_k} + \frac{\partial W_n}{\partial z_n} \]

\[ + \frac{\partial W_n}{\partial \Theta} + \frac{1}{\gamma_2} \bar{\Lambda} \]

\[ \leq -2 x_{n-1}^{p_{n-1} - 1} - \frac{n}{\theta_1} \sum_{k=1}^{n-1} \xi_k^2 \]

\[ - \sum_{k=1}^{n-1} \xi_k^2 + d_{n-1} \left( t \right) \xi_{n-1}^{2(1/p_{n-1} - 1)} \left( z_{n-1}^{p_{n-1} - 1} - \alpha_{n-1}^{p_{n-1} - 1} \right) \]

\[ + \frac{\partial W_n}{\partial x_0} + \sum_{k=1}^{n-1} \frac{\partial W_n}{\partial z_k} + \frac{\partial W_n}{\partial \Theta} \left( z_{n-1}^{2(1/p_{n-1} - 1)} - \alpha_{n-1}^{p_{n-1} - 1} \right) \]

\[ + d_{n-1} \left( t \right) \xi_{n-1}^{2(1/p_{n-1} - 1)} d_{n-1} + \frac{\partial W_n}{\partial \Theta} + \frac{1}{\gamma_2} \bar{\Lambda} \]

\[ \leq \frac{1}{4} \xi_{n-1}^2 + \xi_{n-1}^2 \frac{2^{2(p_{n-1} - 1)}}{p_1 \cdots p_{n-2}} \]

\[ \times \left( \frac{4 p_1 \cdots p_{n-2} - 2}{p_1 \cdots p_{n-2}} \right)^{2(p_{n-1} - 1)} \frac{\partial \alpha_{n-1}^{p_{n-1} - 1}}{p_1 \cdots p_{n-2}} \]

\[ \leq \frac{1}{4} \xi_{n-1}^2 + \Lambda \xi_{n-1}^2 \left( z_{n-1}^{2(1/p_{n-1} - 1)} - \alpha_{n-1}^{p_{n-1} - 1} \right) \]

\[ \leq \frac{1}{4} \xi_{n-1}^2 + \Lambda \xi_{n-1}^2 \left( x_0, z, \bar{\Theta} \right). \]

By Lemma 4, it can be concluded that

\[ \frac{\partial W_n}{\partial x_0} \leq x_{n-1}^{p_{n-1} - 1} \]

\[ + \xi_{n-1}^2 \left( \frac{4}{p_1 \cdots p_{n-1}} \right) \frac{\partial \alpha_{n-1}^{p_{n-1} - 1}}{p_{n-1} - 1} \]

\[ \leq x_{n-1}^{p_{n-1} - 1} + \Lambda \xi_{n-1}^2 \left( x_0, z, \bar{\Theta} \right). \]

(37)
With the same strategy as previously, it follows mentioned that

\[
\sum_{k=1}^{n-1} \frac{\partial W_n}{\partial z_k} \leq \frac{1}{4} \sum_{k=1}^{n-1} \xi_k^2 + \xi_n^2 \left( 4 - \frac{2}{p_1 \cdots p_{n-1}} \right) \left( \sum_{k=1}^{n-1} (p_1 \cdots p_{k-1}) \beta_k^2 \right) \cdot \left( 2(2 + 2 \beta_k + 2r_k x_0^{p-k-1})^2 + (\beta_k + r_k x_0^{p-k-1})^2 \right) + 2 \sum_{l=k+1}^{n-1} \left( 2^2 p_{n-1}^{2(p-n+1)} - 2^2 \varphi_k^2 \varphi_{k+l}^2 + 2^2 p_{n-1}^{2(p-n+1)} - 2^2 \varphi_k^2 \varphi_{k+l}^2 \right) + 2k^2 \left( \varphi_k^2 + \varphi_{k+l}^2 \right) + \xi_n^2 \left( 4 - \frac{2}{p_1 \cdots p_{n-1}} \right) \left( \sum_{k=1}^{n-1} (\partial z_k) \right)^2 \leq \frac{1}{4} \sum_{k=1}^{n-1} \xi_k^2 + \Lambda \xi_n^2 \left( 4 - \frac{2}{p_1 \cdots p_{n-1}} \right)^2 \left( \sum_{k=1}^{n-1} (p_1 \cdots p_{k-1}) \beta_k^2 \right) \cdot \left( 2(2 + 2 \beta_k + 2r_k x_0^{p-k-1})^2 + (\beta_k + r_k x_0^{p-k-1})^2 \right) + 2 \sum_{l=k+1}^{n-1} \left( 2^2 p_{n-1}^{2(p-n+1)} - 2^2 \varphi_k^2 \varphi_{k+l}^2 + 2^2 p_{n-1}^{2(p-n+1)} - 2^2 \varphi_k^2 \varphi_{k+l}^2 \right) + 2k^2 \left( \varphi_k^2 + \varphi_{k+l}^2 \right) + \sum_{k=1}^{n-1} \sum_{l=1}^{k} \left( \frac{\partial z_k}{\partial z_l} \right)^2 \xi_l^2 \leq \frac{1}{4} \sum_{k=1}^{n-1} \xi_k^2 + \Lambda \xi_n^2 \left( x_0, z, \tilde{\Theta} \right). \tag{38} \]

In terms of (34), it can be seen that

\[
\frac{\partial W_n}{\partial \tilde{\Theta}} \leq \gamma_n \left( 4 - \frac{2}{p_1 \cdots p_{n-1}} \right) \left| \frac{\partial \alpha_n^{p-n-1}}{\partial \Theta} \right| \left( \sum_{k=1}^{n-1} \xi_k^2 \right) \leq \frac{1}{4} \sum_{k=1}^{n-1} \xi_k^2 + \xi_n^2 \left( x_0, z, \tilde{\Theta} \right). \tag{39} \]

Substituting (36)–(39) into (35), we have

\[
V_n \leq -x_0^{p+1} - \frac{1}{\theta_1} \sum_{k=1}^{n-1} \xi_k^2 + \alpha_n^{2(p-n-1)} \left( \theta_1 + \theta_2 + \theta_3 \right) + \xi_n^2 \left( x \right) \leq \frac{\gamma_n^2}{2} \left( 1 + \frac{1}{p_1 \cdots p_{n-1}} \right) \left( x \right) + \beta \left( t \right) \xi_n^2 \left( x \right) + \frac{1}{\gamma_2} \left( x \right), \tag{40} \]

where \( \theta_1, \theta_2, \theta_3 \) are suitable positive constants. Denote

\[
\rho_n \left( x_0, z, \tilde{\Theta} \right) = \theta_1 + \theta_2 + \theta_3 + \theta_4, \quad \omega = \gamma_2 \xi_n^2 \left( x_0, z, \tilde{\Theta} \right). \tag{41} \]

As a result, (40) can be further transformed into

\[
V_n \leq -x_0^{p+1} - \frac{1}{\theta_1} \sum_{k=1}^{n-1} \xi_k^2 + \beta \left( t \right) \xi_n^2 \left( x_0, z, \tilde{\Theta} \right) + \frac{1}{\gamma_2} \left( x \right), \tag{42} \]

Inspired by [6, 16], the error variable \( \xi_n = \xi_n^{p-n-1} - \alpha_n^{p-n-1} \) can be viewed as an adaptive sliding surface in the \( x \)-coordinate. Denote the sliding manifold by \( S = \xi_n \), then the adaptive sliding mode control and the parameter update law can be chosen as

\[
u_n = -\frac{1}{\beta} \left( \xi_n^{p-n-1} \right) \times \left( \rho_n \left( x_0, z, \tilde{\Theta} \right) \sqrt{1 + \tilde{\Lambda}^2} + \theta_5 \left( x_0, z, \tilde{\Theta} \right) \right) + \frac{1}{\gamma_2} \left( x \right) \tag{43} \]

\[
\tilde{\Lambda} = \omega, \tag{44} \]

where \( k > 0 \) is a constant and \( \text{sgn}(\cdot) \) is the sign function. Accordingly, we obtain

\[
V_n \leq -x_0^{p+1} - \frac{1}{\theta_1} \sum_{k=1}^{n-1} \xi_k^2 - k \left| S \right|^{2(1/p-n-1)} \cdot \left( x \right). \tag{45} \]

Since \( V_n \) is a positive definite and proper Lyapunov function, (45) guarantees the convergence of the system
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trajectory to the origin of the sliding surface \( S = \xi_n \) in finite
time. In addition, the convergence properties of the states
and the parameter estimate remain unchanged with respect
to those of the standard backstepping design procedure.
That is, the states \((x_0(t), x(t))\) of system (1) converge to zero
asymptotically and the parameter estimates \( \hat{\Theta}(t), \hat{\Lambda}(t) \) are bounded.

4. Switching Control Strategy

In this section, we consider the case of \( x_0(t_0) = 0 \).
Without loss of generality, we assume that \( t_0 = 0 \).
As to the case of \( x_0(0) \neq 0 \), we have given the controller (5) and (43) for \( u_0 \) and \( u \)
of system (1), respectively. Now, we turn to how to select
control laws while \( x_0(0) = 0 \).

We consider the constant control if \(|x_0|\) is small enough.
When \( x_0(0) = 0 \), we choose \( u_0 \) as follows:
\[
    u_0(0) = u_0^*, \quad u_0^* > 0. \tag{46}
\]

In accordance with the first subsystem of (1), we know that
\[
    \dot{x}_0(0) = d_0(0) u_0^{\Theta^0}(0) = d_0(0) u_0^{\Theta^0} > 0. \tag{47}
\]

So, for any small enough constant \( c_0^* \), there exists
an instant \( t_0^* > 0 \) such that \( x_0(t_0^*) = c_0^* \).
During the finite time interval \([0, t_0^*)\), a new adaptive sliding mode control \( u = u^*(x_0, x) \)
using \( u_0 \) as defined in (46) and two new parameter
update laws can be obtained following the procedure described
in the previous section. Combining with \( x_0(t_0^*) = c_0^* \neq 0 \),
we can switch the control inputs \( u_0 \) and \( u \) into (5) and (43),
respectively.

Now we state the main result of this paper.

Theorem 6. Suppose that Assumptions 1–3 are satisfied. If the
proposed control design procedure together with the previous
switching control strategy is applied to system (1), then, for
any initial conditions in the state space \( \Omega = \{(x_0, x) \in \mathbb{R}^{n+1}\} \),
system (1) will be asymptotically stabilized at the equilibrium,
and specifically, the states are regulated to the sliding surface
\( S = 0 \) in finite time while keeping the estimated parameters
bounded.

5. Simulation Example

Consider the following example:
\[
\begin{align*}
    \dot{x}_0 &= d_0(t) u_0^3, \\
    \dot{x}_1 &= d_1(t) x_2^3 u_0^2 + \frac{1}{4} x_1, \\
    \dot{x}_0 &= u^3,
\end{align*}
\tag{48}
\]

where \( x = (x_0, x_1, x_2)^T \) is the state, \( u_0 \) and \( u \) are the control
inputs of the system, \( 0 < \theta_1 \leq \dot{d}_0(t) \leq \theta_2 \) are unknown
control coefficients with \( \theta_1 \) and \( \theta_2 \) being unknown positive
constants. It can be seen that system (48) is in the form of (1)
with \( p_0 = p_1 = p_2 = 3, q_1 = 2, \phi_2(x_0, x_1, x_2) = (1/4)x_2, \)

Denote \( \hat{\Theta} \) as the estimation of \( \Theta = (1 + \theta_2^2) \max\{1, \theta_1^{-1}\} \) and
\( \Lambda = \max\{\theta_2, \theta_2^2\} \).

Here, we just consider the case of \( x_0(0) \neq 0 \). In the first
subsystem of (48), we choose the control law
\[
    u_0 = -x_0. \tag{49}
\]

Using the developed design procedure in Section 3, we can
obtain that
\[
\begin{align*}
    u &= -\xi_2^{1/3} \left( \rho_2 \left( x_0, x_1, x_2, \hat{\Theta}, \hat{\Lambda} \right) \right)^{1/2} + k \text{sgn}(S), \\
    \hat{\Theta} &= \gamma_1 \xi_1^2 \rho_1, \\
    \hat{\Lambda} &= \gamma_2 \xi_2^3 \rho_2,
\end{align*}
\tag{50}
\]

where \( \xi_1 = x_1 / u_0^3, \rho_1 = 9/4 + 2 x_0^2, \beta_1 = \rho_1 (1 + \Theta^2)^{1/2}, \xi_2 = x_2^3 + \xi_1 \beta_2, S = \xi_2 - \rho_2 = 1 + (40/3) x_0^3 \xi_2^2 (1 + \Theta^2)^2 + 100/3 \beta_1^2 (\beta_2^2 + 4 x_0^2 + 1/16) + 10/3 \beta_1 \rho_{25} = (100/9) \gamma_1^2 \xi_1^2 \rho_1^2, k, \gamma_1 \) and \( \gamma_2 \) are
positive design parameters.

Let the unknown functions be \( d_0(t) = 1 - (1/2) \cos t, \)
\( d_1(t) = 1 + (1/4) \sin t \). The unknown constants can be
chosen as \( \theta_1 = 1/2 \) and \( \theta_2 = 3/2 \). Take \( k = \gamma_1 = \gamma_2 = 1 \).
Simulation results of the closed-loop system are shown in Figure 1
with the initial condition \((x_0(0), x_1(0), x_2(0)) = (1, 0.1, 0.25)\).

6. Conclusions

In this paper, the global stabilization problem is considered
for a class of uncertain high-order nonholonomic systems
with unknown control coefficients. By adding a power inte-
grator technique, we propose a combined adaptive/sliding
mode control scheme. To get around the stabilization burden associated with the nonholonomic control systems, a switching control strategy is exploited in this procedure. The designed adaptive sliding mode controller guarantees the global asymptotical stabilization of the closed-loop system as well as the boundedness of the parameter estimates. Moreover, the attractiveness of the sliding surface $S = 0$ in finite time is also obtained with the help of the proposed control approach.

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