Research Article

Fault Forecasting of a Machining Center Tool Magazine Based on Health Assessment

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A tool magazine is one of the key functional components of machining centers with frequent faults. The reliability level of a tool magazine directly affects the reliability level of the machining center. After establishing a reliability test bench and a prognostic and health management system for a tool magazine, a novel fault-forecasting method for machining center tool magazines based on health assessment is proposed. First, the health status of each tool magazine subcomponent is determined using the grey clustering method. Second, the weight of each tool magazine subcomponent is determined using an entropy weight method. Third, the health status of the tool magazine is evaluated via fuzzy comprehensive evaluation. If the tool magazine exhibits an unhealthy status, then the subcomponent with the worst health status is selected for fault forecasting. In addition, standardized treatment, stationarity test, and differential processing are conducted separately on the raw performance indicator data of the worst subcomponent. Finally, the performance indicators of the worst subcomponent are forecasted with the constructed autoregressive moving average model. Using tool-falling failure as an example, the forecasted and experimental tool-pulling forces are compared and analyzed, and the prediction accuracy of the proposed method is verified.

1. Introduction

The numerical control (NC) machine tool is the material and technical basis of a modern manufacturing system; it is a “working machine” with high-tech content. At present, NC machine tools have made remarkable progress in terms of accuracy, speed, large-scale production, multiaxis linkage, and composite functions. However, their reliability level is one bottleneck that restricts their ability to reach the advanced international level. A tool magazine is one of the key functional components of NC machine tools with frequent faults that seriously affect its processing efficiency, resulting in considerable maintenance costs and downtime losses. Prognostic and health management (PHM) uses various algorithms and models to identify the mapping relationship between fault symptoms and causes, deduces the cause and location of faults, traces fault symptoms, predicts possible faults, points out the development trends and consequences of faults, predicts the residual life of components, and formulates the best maintenance and guarantee scheme. Therefore, PHM technology for tool magazines is helpful for improving their reliability, safety, and adaptability.

PHM technology has been gradually applied to engineering since the 1970s. The US military used PHM technology to build a health management system for F-35 Joint Strike Fighter [1]. Lee et al. [2] discussed the implementations of machine health management within a smart factory in terms of data connectivity, communications, cyber-physical systems, and virtual factories. Tsui et al. [3] provided a concise review of mainstream methods in aspects of the PHM framework with a focus on data-driven approaches. Lee et al. [4] provided a comprehensive review of PHM design for a rotary machinery system. Khan and Yairi [5] presented a systematic review of artificial intelligence-based PHM. He et al. [6] addressed the development and application of PHM technologies to a screw-tightening machine. Zheng et al. [7] designed a PHM system for NC machines to improve the reliability and availability of NC.
machine tools. Javed et al. [8] built a model with summation wavelet extreme learning machine, to perform tasks, such as the wear estimation of a cutting tool from a machining center and the long-term prediction of a bearing from a machining center.


In fault prediction, Aggoune et al. [25] proposed a fault detection method based on nonlinear autoregressive moving average (ARMA) with an exogenous input model and Hellinger distance for a distillation unit. Wu et al. [26] used a fractal autoregressive integrated moving average (ARIMA) model to predict the skip-over of a machinery. Jurjevic et al. [27] used an ARIMA method for the early fault detection of a pulverised coal preparation system. Cai et al. [28] used an adaptive residual grey model and an improved ARMA model to predict gyroscope drift. Kim et al. [29] presented a forecasting approach based on generalised linear ARMA models and integer-valued generalised autoregressive conditional heteroscedastic models. Xiao et al. [30] used a multistep ARMA model to detect sensor and processed faults with good accuracy under different scenarios. Wang et al. [31] used an ARIMA model and a hidden Markov model to predict the reliability of a vertical roller mill. Aghdam and Cigeroglu [32] used a nonstationary functional series time-dependent ARMA model for forecasting tool nonstationary signals. At present, most fault-forecasting methods are based on the ARMA model and its variants. Compared with the ARMA model, the ARIMA model first performs differential processing on nonstationary time series and then establishes the ARMA model. The primary objects of fault forecasting are rotary parts, and the monitored signals are mostly vibration signals. Existing methods do not fully consider the physical meaning and degradation of the performance indicators of each subcomponent. Therefore, the generalization of these methods is weak, and their prediction accuracy is poor.

The current study builds a reliability test bench and a PHM system for tool magazines. The health status of each tool magazine subcomponent is evaluated using grey clustering and an entropy weight method. Meanwhile, the health status of a tool magazine is evaluated using a fuzzy comprehensive evaluation method. When a tool magazine exhibits an unhealthy status, fault forecasting is performed on the subcomponent with the worst health status. Using tool-failing failure as an example, we forecast the changing trend of the tool-pulling force.

2. Relevant Theory and Methodology

2.1. Grey Clustering Theory. Grey clustering theory is a method for integrating several performance indicators that cannot be directly classified into several grey categories by the whitening weight function of grey relational objects. For example, m objects and n performance indicators should be clustered, and k different grey categories are present. $X_{ij}$ ($i = 1, 2, \ldots, m; j = 1, 2, \ldots, n$) is the evaluation value of the i-th clustering object on the j-th clustering index. Grey clustering refers to classifying the i-th object into the s-th ($s = \{1, \ldots, k\}$) grey category. The whitening weight function
of the $s$-th grey category and the $j$-th performance indicator is recorded as $f^s_j(\ast)$. The whitening weight functions include whitening weight function of a typical measure, whitening weight function of a lower limit measure, whitening weight function of an upper limit measure, and whitening weight function of a moderate measure. $\beta^s_i$ is the grey clustering coefficient of the $i$-th clustering object relative to the $s$-th grey class:

$$\beta^s_i = \sum_{j=1}^{n} f^s_j(X_{ij}) \cdot \omega_j,$$

$$\sum_{j=1}^{n} \omega_j = 1,$$ (1)

where $\omega_j$ represents the weight of the $j$-th performance indicator and $s$-th grey class. The clustering coefficient vector of the $i$-th clustering object is shown in the following equation:

$$\beta_i = [\beta^1_i, \beta^2_i, ..., \beta^n_i] = \left[ \sum_{j=1}^{n} f^1_j(X_{ij}) \cdot \omega_j, ..., \sum_{j=1}^{n} f^n_j(X_{ij}) \cdot \omega_j \right],$$

$$\max_{1 \leq i \leq N} \{\beta^s_i\} = \beta^{s^*}_i,$$ (2)

where $\beta^{s^*}_i$ denotes that the $i$-th cluster object belongs to the $s^*$-th grey class.

2.2. Entropy Weight Method. Suppose $m$ objects and $n$ performance indicators exist. The original data matrix $X = (X_{ij})$, $X_{ij} \geq 0$, $i = 1, 2, ..., m$; $j = 1, 2, ..., n$. Matrix $X$ is normalized to obtain matrix $P$:

$$\omega_j = \frac{(1 - E_j)}{(n - \sum_{j=1}^{n} E_j)},$$ (4)

where $\omega_j$ represents the weight of the $j$-th performance indicator. $E_j$ represents the entropy of the $j$-th performance indicator.

2.3. ARMA Model. ARMA is a stochastic time series model. As shown in equation (5), time series $\{X_t\}$ exhibits the characteristics of a stable, zero-mean, and normal distribution, and then it can be fitted by the ARMA model:

$$X_t = \sum_{i=1}^{m} \phi_i X_{t-i} - \sum_{j=1}^{n} \theta_j t_{t-j} + \tau_t,$$ (5)

where $m$ denotes the autoregressive order, $n$ denotes the moving average order, $\phi_i$ is the autoregressive coefficient, $\theta_j$ is the moving average coefficient and sequence, and $\{\tau_t\}$ is white noise.

2.4. Determination of ARMA Model Order. The purpose of determining model order is to identify which model should be selected for fault prediction from the autoregressive (AR), moving average (MA), and ARMA models. In general, the order of a model is determined by observing the ACF and partial ACF (PACF) of a sequence. Table 1 shows the relationship between model order, ACF, and PACF.

The order of the ARMA model determined by ACF and PACF should be optimised. The general optimisation criteria include the Akaike information criterion and the Bayesian information criterion.

2.5. Model Solving and Testing. $m$ and $n$ are calculated in accordance with AIC and BIC. The results of $m$ and $n$ are expressed by $\hat{m}$ and $\hat{n}$. The unknown parameters in the model are calculated using SQP. General test methods include model goodness of fit, $F$, and residual tests. Theoretically, $\tau_t$ is a white Gaussian noise with a mean of zero. The residual of the preceding model is given by

$$\hat{\tau}_t = X_t - \sum_{i=1}^{m} \hat{\phi}_i X_{t-i} + \sum_{i=1}^{n} \hat{\theta}_i \tau_{t-i}.$$ (6)

The residual test primarily tests the randomness of a sequence and determines whether it is white noise. If the residual sequence does not satisfy randomness, then the model should be improved. The hypothesis of the test is $\{H_0: k \leq L, \rho_k = 0; H_1: k \leq L, \rho_k \neq 0\}$. If $H_0$ holds, then $\chi^2$ approximates to the $\chi^2(L-r)$ distribution, where $r$ is the number of parameters of the ARMA model. For a given saliency level $\alpha$, $H_0$ is rejected when $x^2 > x^2_{\alpha}(L-r)$; that is, $\tau_t$ is not white noise and the model test fails. When $x^2 \leq x^2_{\alpha}(L-r)$, $H_0$ is accepted; that is, $\tau_t$ is white noise, and the model test passes.

3. Fault Forecast of a Tool Magazine Based on the ARMA Model

3.1. Partition of a Tool Magazine and Determination of Performance Indicators. The research object in this work is the YP4024 tool magazine. We tracked a batch of tool magazines used by an enterprise. A reasonable division of subcomponents is the premise of PHM. In accordance with the principles of function sharing, function independence, and industry consensus, we divide the tool magazine into five subcomponents: the tool flywheel motor, the manipulator motor, the pneumatic device, the automatic tool change (ATC) system, and the cutter body and the tool case. In general, the tool flywheel motor and the manipulator motor are purchased parts. The pneumatic device, the ATC system, the cutter body, and the tool case have different functions. The ATC system primarily includes the transmission system of the manipulator and the manipulator. The failure mode is the manifestation of failure. After analyzing the collected faults, the typical failure modes of a tool magazine include tool-falling failure, jamming of tool failure, sensor failure,
3.2. Fault Forecasting of a Tool Magazine Based on Health Assessment. The fault forecasting process for tool magazines based on health assessment is shown in Figure 3. The specific steps are as follows:

Step 1: a tool magazine is divided into five different subcomponents, and the performance indicators of each subcomponent are determined.

Step 2: for every subcomponent, the weight of each performance indicator is determined using an entropy weight method, and the health status of each subcomponent is evaluated using the grey clustering method.

Step 3: the entropy weight method is used to determine the weight of each subcomponent. A fuzzy comprehensive evaluation method is used to determine the health status of the tool magazine.

Step 4: if the tool magazine exhibits an unhealthy status, we analyze failure modes related to the subcomponent with the worst health status and identify the most likely failure. Then, we determine the performance indicators corresponding to the most likely failure.

Step 5: the performance indicator data of the subcomponent with the worst health status are collected and standardized. Next, autocorrelation function (ACF) is used to test the stability of performance indicator data. If the data are nonstationary, then the data are smoothed by differential operation.

Step 6: the order of the ARMA model is determined on the basis of the ACF and PACF of the processed sequence. The order of the ARMA model is optimised through AIC and BIC. The unknown parameters in the model are calculated using sequence quadratic program (SQP). The ARMA model is tested via the residual test method. The failure of the tool magazine is forecasted on the basis of the established ARMA model.

4. Results and Discussion

4.1. Reliability Test Bench and PHM System of a Tool Magazine. The reliability test bench and PHM system of a tool magazine are established as shown in Figure 4. The reliability test bench includes a bracket, a tool magazine, various sensors, a counterweight block, and a virtual spindle. The counterweight block is used to replace the real tool. The PHM system consists of condition-monitoring, data management, health assessment, and fault-forecasting modules. The condition-monitoring module collects the performance indicator data. The data management module completes the storage and reading of the collected data. The health assessment module realizes the health assessment of the subcomponents and the tool magazine. The fault-forecasting module is used to forecast the failure of the subcomponent with the worst health status.

4.2. Health Assessment of a Tool Magazine. Table 2 shows the weights and normalized values of each performance indicator for several subcomponents of the tool magazine. Following the recommendation in [9], the normalized values are defined as healthy in [0.85, 0.9, -], subhealthy in [0.6, 0.7, 0.8, 0.85], degeneration in [0.4, 0.5, -], deterioration in [0.2, 0.3, -], and failure in [-, 0, 0.1, 0.2]. Table 3 provides the grey clustering coefficients and health status of each subcomponent of the tool magazine calculated on the basis of grey clustering theory. By substituting the data provided in Table 3 into the calculation formula of the entropy weight method, the weight value of each subcomponent of the tool magazine is determined as follows: \( \omega = [0.20, 0.20, 0.23, 0.09, 0.28] \). The health status of the tool magazine can be obtained by using the fuzzy comprehensive evaluation method, as shown in Table 3. The evaluation result indicates that the health status of the tool magazine is subhealthy, and the cutter body and the tool case should be inspected after shutdown. After inspection, the tool-pulling force of No. 24 tool case is relatively small, and the throttle valve in the pneumatic device that controls the flow rate of the air intake of the cylinder is loose. On the basis of the aforementioned inspection and analysis, the evaluation result is consistent with the actual state.
4.3. Fault Forecasting of a Tool Magazine. The health assessment result indicates that the failure of the cutter body and the tool case should be forecasted. The failure rate of the cutter body is extremely low, and its performance indicator is vibration of cutter head. The tool case is a consumable part. Its performance indicator is tool-pulling force. The inspection of the cutter body and the tool case reveals that the locking force of No. 24 tool case is too small. Small locking force mainly causes the tool-falling failure. The tool-falling failure can be characterized by the tool-pulling force. We select the tool-falling failure as the most likely failure and predict the most important performance indicator, namely, the tool-pulling force. A total of 10000 tool changes are executed for No. 24 tool case. The tool-pulling force is measured every 100 tool changes. A total of 100 tool-pulling force values are measured. The specific change of the tool-pulling force is shown in Figure 5.

The data in Figure 5 are standardized to calculate the ACF of the original data. As shown in Figure 6, $\hat{\rho}_L$ does not converge to 0 with an increase in $L$; thus, the original sequence is nonstationary. Given the linear trend of the original data, the first-order differential processing of the original data is performed, as shown in Figure 7.

As indicated in Figure 7, the downward trend of the raw data has been eliminated and the fluctuation of the data has been basically stabilized. Figures 8 and 9 present the ACF and PACF values of the first-order differential sequence.

Referring to Figures 8 and 9, when $L$ is 0, both PACF and ACF are 1. As $L$ increases from 1 to 4, the ACF decays rapidly, and the PACF basically exhibits an exponential decay. As $L$ increases from 5 to 20, ACF and PACF basically fluctuate slightly between $[-0.1, 0.1]$. Because of the randomness of samples, ACF and PACF do not show theoretical truncation or tailing, but a slight oscillation. The ACF and PACF of the first-order differential sequence are a four-order truncation and a tailing, respectively. Preliminary determination indicates that $m = 0$ and $n = 4$. The model is determined to be MA (4). On the basis of ACF and PACF, the order of the ARMA model is less than 4 ($m, n < 4$). AIC and BIC are calculated for the first-order differential sequence, as shown in Figures 10 and 11.

When $m = 2$ and $n = 4$, AIC and BIC are the smallest; thus, the ARMA model is ARMA (2, 4). Then, the parameter is estimated using SQP. The model parameters are $\hat{\theta} = (-2.340, 2.220, -0.862, 0.153)$ and $\hat{\varphi} = (-1.247, 1.260)$. The residual model is tested on the basis of significance level $\alpha = 0.05$. The test result is $H_0$, that is, the accuracy of the model meets the requirements. The 1st–90th tool-pulling force values are fed into the ARMA (2, 4) model to predict the 91st–100th tool-pulling force values. The parameter estimation of the ARMA model is essentially a problem of finding the minimum value of a constrained nonlinear multivariable function. The parameter estimation methods of ARMA (2, 4) model include interior point method, SQP, and active set method. As shown in Table 4, the predictions of the ARMA (2, 4) model using different parameter estimation algorithms are compared with the original data.
The original data fluctuated sharply. Each set of predictions fluctuates slowly. The mean absolute percentage error (MAPE) of the 10-step prediction of interior point method, SQP, and active set method is 2.34%, 2.26%, and 2.31%, respectively. It can be seen that the ARMA (2, 4) model with SQP has the highest prediction accuracy. The MAPE of the 10-step prediction of the ARMA (2, 4) model with SQP is within 3%. In other words, the predicted value
is likely to be 0.97 to 1.03 times the corresponding actual value. Firstly, it is generally believed that if the MAPE is less than 10%, the prediction accuracy is considered to be high. Secondly, with the increase of the number of tool changes, the tool-pulling force decreased in a fluctuation way. Refer to Figure 7, the first-order difference sequence is not a constant value, but fluctuates basically in the interval $[-30 \text{N}, 30 \text{N}]$. It can be seen that the tool-pulling force has a certain randomness. Assume that the actual value of the tool-pulling force is 600 N, its predicted value is likely to be between 580 and 620. Finally, in engineering practice, the tool case is a consumable part. In order to replace the tool case in time, the failure threshold is often set to about 1.1 times the tool-pulling force when the tool-falling failure falls. Therefore, the constructed ARMA model is suitable for predicting tool-pulling forces.

As shown in Figure 12, the 1st–100th tool-pulling force values are fed into the ARMA $(2, 4)$ model to predict the 101th–515th tool-pulling force values. In the short term, for 101th–110th tool-pulling force values, the tool-pulling force decreased in a fluctuation way. Its fluctuation became smaller and smaller. The ARMA $(2, 4)$ model has high prediction accuracy and retains small fluctuations. Given that the locking force of the tool case is less than 500 N, tool-falling failure may occur. Thus, 500 N is used as the failure threshold of tool-falling failure. Obviously, the tool-falling failure will not happen shortly. In the long run, for 111th–515th tool-pulling force values, the tool-pulling force decreases linearly. Due to the nonlinearity and non-stationarity of the degradation process of the internal parts.
of tool case and the mutual coupling between the parts, the attenuation process of tool-pulling force is actually nonlinear and nonstationary. Therefore, the deviation between the linear attenuation process predicted by the constructed static ARMA (2, 4) model and the actual nonlinear attenuation process is large. Long-term prediction is inaccurate, but it is helpful to predict tool-falling failure. After 51000 tool changes, the forecasted interval of the tool-pulling force is [500N, 545N]. Tool-falling failure may occur after 51000 tool changes.

5. Conclusions

The typical failure modes of a tool magazine are analyzed on the basis of a large number of failures. After establishing a reliability test bench and a PHM system for the tool magazine, a novel fault-forecasting method for the machining center’s tool magazine based on health assessment is proposed. This research exhibits theoretical significance and practical application value. Simultaneously, it can be applied to other key functional components of the machining center and the entire machine, promoting the intelligentisation of the machining center. The major conclusions of this study are as follows:

1. Applying the principles of function sharing, function independence, and industry consensus, the tool magazine is divided into five parts: the tool flywheel motor, the manipulator motor, the pneumatic device, the ATC system, and the cutter body and the tool case. We determine the performance indicators of each subcomponent from the FTA results. The PHM system of the tool magazine is established accordingly.

2. A health assessment method based on grey clustering, entropy weight method, and fuzzy comprehensive evaluation method is proposed. The weight of each subcomponent’s performance indicator is determined using the entropy weight method, and the health status of each subcomponent is evaluated via grey clustering. The health status of the manipulator motor, the tool flywheel motor, the cutter body and the tool case, the ATC system, and the pneumatic device are as follows: healthy, healthy, deteriorated, healthy, and degraded. The fuzzy comprehensive evaluation method is used to obtain the health status of the tool magazine as subhealthy.

3. A fault prediction method based on the ARMA model is proposed. The evaluation result of the health status indicates that failure prediction should be performed on the No. 24 tool case. A total of 10000 tool changes are implemented, and the ARMA (2, 4) model is established. The model parameters $\theta = (-2.340, 2.220, -0.862, 0.153)$ and $\varphi = (-1.247, 1.260)$. The trend of the tool-pulling force is predicted on the basis of the model, and the original data are used to verify the prediction result. The result shows that the mean absolute percentage error of 10-step prediction is within 3%. The constructed ARMA model is suitable for predicting tool-pulling forces.

Data Availability

The data used to support the findings of this study are included within the supplementary information file.

Conflicts of Interest

The authors declare that there are no conflicts of interest regarding the publication of this paper.

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Supplementary Materials

Table 1: original value of every performance indicator for every subcomponent of a tool magazine. Table 2: the 100 original tool-pulling force values. (Supplementary Materials)

References


