

Research Article

A Simple Formula for Local Burnup and Isotope Distributions Based on Approximately Constant Relative Reaction Rate

Cenxi Yuan, Xuming Wang, and Shengli Chen

Sino-French Institute of Nuclear Engineering and Technology, Sun Yat-sen University, Zhuhai, Guangdong 519082, China

Correspondence should be addressed to Cenxi Yuan; yuanxc@mail.sysu.edu.cn

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A simple and analytical formula is suggested to solve the problems of the local burnup and the isotope distributions. The present method considers two extreme conditions of neutrons penetrating the fuel rod. Based on these considerations, the formula is obtained to calculate the reaction rates of ^{235}U , ^{238}U , and ^{239}Pu and straightforward the local burnup and the isotope distributions. Starting from an initial burnup level, the parameters of the formula are fitted to the reaction rates given by a Monte Carlo (MC) calculation. Then the present formula independently gives very similar results to the MC calculation from the starting to high burnup level but takes just a few minutes. The relative reaction rates are found to be almost independent of the radius (except (n, γ) of ^{238}U) and the burnup, providing a solid background for the present formula. A more realistic examination is also performed when the fuel rods locate in an assembly. A combination of the present formula and the MC calculation is expected to have a nice balance between the numerical accuracy and time consumption.

1. Introduction

To increase the efficiency of the fuel, one possible way is to increase the burnup of the fuel before discharge. The local burnup on the edge of the UO_2 fuel rod is much higher than the average burnup. Thus it is of great importance to investigate the properties of the rim of the fuel rod when considering the increment of the average burnup. Many investigations show that the mechanical structure close to the surface is rather different from that at the center of the fuel rod. In the high burnup range, a microstructure change was found on the rim of the fuel rod through transmission electron microscopy [1]. One explanation of the formation of the high burnup structure supposed that the bubbles in high burnup region are nucleated and stabilized by fission fragments, which depends on the fission rate [2]. The small pores at the high burnup region are calculated to be highly overpressurized [3]. Recently, the UO_2 fuel in both light and heavy water reactor is investigated to understand the high burnup structure of the fuel [4, 5].

In a thermal reactor, the neutrons generated from fission need to be slowed down in the moderator to be able to induce

the next fission. When the low energy neutrons go from the moderator to the fuel rod, they are firstly absorbed by the fuel close to the surface. In general, the reaction rate is higher in the rim when induced by slowed neutrons, such as the (n, f) reaction of ^{235}U and ^{239}Pu induced mainly by the thermal neutron. In contrast, the (n, γ) reaction of ^{238}U is mainly induced by the resonance neutrons. The local burnup phenomenon is mainly caused by the (n, γ) reaction of ^{238}U , which has large cross section for resonance neutrons, especially some high peaks of cross section at certain energies. Such reaction produces much more ^{239}Pu near the surface of the fuel rod, thus giving origin to the increased local burnup. As a consequence of the different reaction rates along the radial direction, the U and Pu isotopes also have different radial distributions. In a fast reactor, the Pu isotopes are redistributed along the radial direction [6]. A large local burnup is not expected because the neutrons do not need to be slowed down in the moderator.

In nuclear science, theoretical models are very important and powerful to solve various problems. Our previous works have shown that the mass, levels, electromagnetic moments

and transitions, and other properties of the nuclei can be described with high precision in the frame of the nuclear shell model even for very unstable nuclei, such as ^{22}C and ^{21}Al [7–9]. In nuclear reactor, the simulation is even more important because the experimental data are relatively difficult to be obtained, sometimes with high risk. For the present problem, various models can be used to calculate the local burnup and the isotope distributions along the radial direction. The TRANSURANUS model is very successful in the description of the local burnup and related properties in various reactors including light and heavy water reactors [10–12]. In TRANSURANUS model, a fixed neutron flux is assumed except for the absorption reaction of ^{238}U and ^{240}Pu [12], while the RAPID model considers detailed properties of the neutron flux at each burnup [13]. Recently, an empirical formulation is suggested to describe the local burnup and high burnup properties based on DIONISIO code [14–16].

Here we suggest an analytical and simple formula to calculate local burnup and isotope distributions based on the constant relative reaction rates at the different radius (except for ^{238}U) and burnup. The present method considers the radial distribution of the neutron flux through two extreme conditions. The parameters are fitted to the reaction rates of the starting burnup level. From this level, the present method is shown to have independent and similar results to the Monte Carlo (MC) simulation, but just a few minutes is needed because of its simplicity.

2. The Description of the Model

The rate of certain reaction type (x) between neutrons and a given nuclide (A) at an average burnup (bu) can be written as a function of the radius (r) and the energy of neutron (E):

$$R(r, A, x) = \int_E N(r, A) \phi(r, E) \sigma(A, x, E) dE, \quad (1)$$

where $N(r, A)$ is the concentration of the nuclide A at the radial position r , $\phi(r, E)$ is the neutron flux at the energy E and the radius r , and $\sigma(A, x, E)$ is the microscopic cross section between neutron and A for reaction type x at the energy E . The (n, f) and (n, γ) reactions are assumed to be the two more important reaction types in the fuel rod. In the present work, the main purpose is to examine the validity of the present model. Thus only ^{235}U , ^{238}U , and ^{239}Pu isotopes are considered to constrain the model testing to a simple case.

In the present study, (1) is assumed to be two terms for (n, f) and (n, γ) of ^{235}U and ^{239}Pu , and (n, f) of ^{238}U :

$$R(r) = N(r) [c_1 + c_2 e^{b_1(r-r_0)}], \quad (2)$$

and three terms for (n, γ) of ^{238}U :

$$R(r) = N(r) [c_3 + c_4 e^{b_1(r-r_0)} + c_5 e^{b_2(r-r_0)}], \quad (3)$$

where the coefficients c are specified for each nuclide and the reaction type. The coefficient b_1 is expected to be the same for all three nuclides. The coefficient b_2 in (n, γ) of ^{238}U is much larger than b_1 .

The following discussion concentrates on the explanations of the above assumptions of the reaction rates. In a thermal reactor, two kinds of the neutron reactions are most important: the scattering reaction in the moderator and the absorption reaction in the fuel rod. When the slowed down neutrons penetrate into the fuel rod, we mainly concentrate on the neutron flux at the thermal and resonance region which are important to the absorption reaction in the fuel rod. The average energy of fission neutron is around 2 MeV, which is much larger than that of the thermal and resonance neutron. Thus no multiplication of the neutron flux is considered at the energy of thermal and resonance region in the following discussion. Two extreme conditions can be considered for certain energy of the neutron. The first one is that the neutrons are strongly absorbed by the fuel, which indicates that the mean free path (MFP) of the absorption, $\lambda(a, E) = 1/\Sigma_a(E) = 1/(\Sigma_{a,5}(E) + \Sigma_{a,8}(E) + \Sigma_{a,9}(E))$, is much smaller than the size of the fuel rod at the energy E . The second one is that few neutrons are absorbed in the fuel at the energy E .

For the first extreme condition, one can further simplify that the velocities of the neutrons are all perpendicular to the surface of the fuel rod. Such assumption is acceptable because the velocity is almost symmetric around the radial directions in the real case. Then the transportation of the neutrons at certain energy E is the solution of the Boltzmann equation in the cylindrical coordinate without the terms of the scattering and the source. The radial part of the equation is as follows:

$$-\frac{1}{r} \frac{\partial r \phi(r, E)}{\partial r} + \Sigma_a(E) \phi(r, E) = 0, \quad (4)$$

where the negative sign comes from the opposite direction between the velocity and the radial vector, and the solution is as follows:

$$\phi(r, E) = \frac{r_0}{r} \phi(r_0, E) e^{(r-r_0)/\lambda(E)}, \quad (5)$$

where r_0 is the radius of the fuel rod. Because of the assumption of the strong absorption, the neutron flux is meaningful near the surface of the fuel rod. The divergence at $r = 0$ should not be considered. Because $\lambda(a, E)$ is much smaller than the size of the fuel rod, r_0 , the neutron flux decreases very quickly to zero at small $(r - r_0)$. The neutron flux $\phi(r, E)$ is approximately $\phi(r_0, E) e^{(r-r_0)/\lambda(E)}$ near the surface and zero at the other radial region. The reaction rate per nucleus $R(r, A, x, E)/N(r, A)$ is proportional to $e^{(r-r_0)/\lambda(a, E)}$, resulting in the third term in (3). One example of such situation corresponds to the (n, γ) reaction of ^{238}U at certain energy. The magnitude of the atomic concentration of ^{238}U is around $10^{22}/\text{cm}^3$ in the fuel rod. For (n, γ) reaction of ^{238}U , some peaks of cross section at the resonance region can achieve 10^4 barns [17], resulting in $\lambda(a, E) = 1/\sigma_{a,8}(E)N_8$ at the magnitude of 10^{-2} cm, which is much smaller than the size of the fuel rod.

For the second extreme condition, $\lambda(a, E)$ is much larger than the size of the fuel rod r_0 . $\phi(r, E)$ is almost unchanged in the fuel rod and $R(r, A, x, E)/N(r, A)$ is also approximately constant, resulting in the first term in (2) and (3).

The magnitude of the concentrations of ^{235}U and ^{235}Pu is around or less than $10^{20}/\text{cm}^3$ in the fuel rod. If $\sigma_{a,5;9}(E)$ and $\sigma_{a,8}(E)$ are much smaller than 10^4 barns and 10^2 barns, respectively, then $\lambda(a, E)$ is much larger than r_0 .

For the situations between these two limits, the second term in (2) and (3) is assumed with b_1 the same magnitude of $1/r_0$. Please note that the above discussion is restricted in the fuel rod. If the neutrons go out of the fuel rod, they may be slowed and reenter the fuel rod with a different energy.

In principle, c , b in (2) and (3) can be calculated through the cross section data and the neutron flux at r_0 . But in some energy regions, the cross sections change dramatically, and hence it is difficult to obtain the coefficients. Spatially Dependent Dancoff Method can be used to calculate the cross sections in the resonance region [18]. In the present work, these coefficients are fitted using a MC calculation. An initial burnup level bu_1 is assumed and with it a MC calculation is done for one fuel rod to calculate the reaction rates at different radial positions. The coefficients are then fitted to these reaction rates and used to calculate the burnup levels after bu_1 . After bu_1 , the MC calculation and the present formula are performed independently for all burnup levels, bu_2 , bu_3 , and so on. The concentrations can be calculated through

$$\begin{aligned} N_5(r, \text{bu}_{i+1}) &= N_5(r, \text{bu}_i) - (R_{5,f}(r) + R_{5,\gamma}(r)) T, \\ N_8(r, \text{bu}_{i+1}) &= N_8(r, \text{bu}_i) - (R_{8,f}(r) + R_{8,\gamma}(r)) T, \\ N_9(r, \text{bu}_{i+1}) &= N_9(r, \text{bu}_i) + (R_{8,\gamma}(r) - R_{9,f}(r)) T, \end{aligned} \quad (6)$$

by assuming that the reaction rates do not change during time T . The time duration T corresponds to the burnup change between two levels:

$$\Delta\text{bu} = \frac{QT \int_0^{r_0} [R_{5,f}(r) + R_{8,f}(r) + R_{9,f}(r)] 2\pi r dr}{M_{0\text{U}}(\pi r_0^2)}, \quad (7)$$

where Q is the average energy released by fission and $M_{0\text{U}}(\pi r_0^2)$ is the initial mass of U isotopes in volume πr_0^2 . One can transform

$$\begin{aligned} \Delta N_5(r) &= \frac{M_{0\text{U}}(\pi r_0^2)}{Q} \\ &\cdot \frac{-(R_{5,f}(r) + R_{5,\gamma}(r))}{\int_0^{r_0} [R_{5,f}(r) + R_{8,f}(r) + R_{9,f}(r)] 2\pi r dr} \Delta\text{bu}, \\ \Delta N_8(r) &= \frac{M_{0\text{U}}(\pi r_0^2)}{Q} \\ &\cdot \frac{-(R_{8,f}(r) + R_{8,\gamma}(r))}{\int_0^{r_0} [R_{5,f}(r) + R_{8,f}(r) + R_{9,f}(r)] 2\pi r dr} \Delta\text{bu}, \end{aligned}$$

$$\begin{aligned} \Delta N_9(r) &= \frac{M_{0\text{U}}(\pi r_0^2)}{Q} \\ &\cdot \frac{(R_{8,\gamma}(r) - R_{9,f}(r))}{\int_0^{r_0} [R_{5,f}(r) + R_{8,f}(r) + R_{9,f}(r)] 2\pi r dr} \Delta\text{bu}. \end{aligned} \quad (8)$$

In MC calculation, the reaction rates in the above equations are simulated with the concentration of all three isotopes at each burnup level. The present formula calculates all reaction rates through the coefficient fitted to the reaction rate at bu_1 . The $R_{9,\gamma}(r)$ reaction rate is neglected in the above equations in both MC and analytical calculation because the present model does not include ^{240}Pu . It is acceptable as the present work concentrates on the examination of the formula not on a real burnup problem. The next section shows that the present formula can obtain results for bu_n quite close to those obtained with the MC calculation.

The above equation looks similar to the formula in TRANSURANUS model [10, 12], in which the relationship between $N(r)$ and bu can be generally written as

$$\frac{dN_j(r)}{d\text{bu}} = -\sigma_{a,j} N_j(r) f_j(r) A + \sigma_{c,j-1} N_{j-1}(r) f_{j-1} A, \quad (9)$$

where j is one kind of nuclide. For $^{235,238}\text{U}$, there are no second terms. For ^{236}U , ^{237}Np , and $^{238,239,240,241,242}\text{Pu}$, $j-1$ are $^{235,236}\text{U}$, ^{237}Np , ^{238}U , and $^{239,240,241}\text{Pu}$, respectively. σ_a and σ_c are the one-group effective cross sections for the total neutron absorption and neutron captured, respectively. The cross sections are obtained differently for UO_2 and MOX fuel because of the very different initial concentrations in each fuel and the corresponding different neutron spectrum. A is a conversion constant. $f(r)$ is the radial form factor, which is $1 + p_1 \exp(-p_2(r_0 - r)^{p_3})$ for ^{238}U and ^{240}Pu and unit for all other nuclides. $f(r)$ comes from the resonance absorption and the parameters are determined by comparison with measurements [10, 12]. The local burnup and isotope distributions can be calculated through (9). More details can be found in [10, 12]. The present work does not consider unit $f(r)$ (actually the different radial neutron flux) for all nuclei.

3. Calculations and Discussions

In the present work, the continuous energy Monte Carlo code TRIPOLI-4 [19] is used for the MC calculations as the starting point of the analytical formula and the reference after calculations. The geometry of the fuel rod in the present investigation is set to be $r_0 = 0.4127$ cm, with cladding between 0.4127 and 0.4744 cm. The moderator is in an outside box with the length 1.2647 cm. All neutrons are reflected back when colliding with the six surfaces of the box. The fuel rod is divided to seven parts in the MC simulation, with the dividing point located at $r/r_0 = 1/2, 3/4, 7/8, 15/16, 31/32, 63/64$. The corresponding center r'/r_0 of each part is listed in Table 1. For a normal UO_2 fuel, there is no Pu isotopes at the beginning. It is reasonable to start the present calculation at a certain burnup bu_1 with Pu

TABLE 1: Relative radius, atomic concentrations, and relative reaction rates of each nucleus. The atomic concentrations are given in cm^{-3} , and all the other quantities are dimensionless.

r'/r_0	N_5	N_8	N_9	$R'_{5,f}$	$R'_{8,f}$	$R'_{9,f}$	$R'_{5,\gamma}$	$R'_{8,\gamma}$
1/4	6.65×10^{20}	2.17×10^{22}	3.69×10^{19}	1.00	0.0025	2.50	0.23	0.0183
5/8	6.63×10^{20}	2.17×10^{22}	3.91×10^{19}	1.02	0.0024	2.49	0.23	0.0189
13/16	6.61×10^{20}	2.17×10^{22}	4.33×10^{19}	1.05	0.0024	2.49	0.23	0.0203
29/32	6.59×10^{20}	2.17×10^{22}	5.01×10^{19}	1.07	0.0023	2.48	0.23	0.0230
61/64	6.58×10^{20}	2.17×10^{22}	6.26×10^{19}	1.08	0.0023	2.47	0.23	0.0283
125/128	6.58×10^{20}	2.16×10^{22}	8.49×10^{19}	1.09	0.0022	2.47	0.23	0.0368
127/128	6.57×10^{20}	2.16×10^{22}	1.26×10^{20}	1.10	0.0022	2.47	0.23	0.0552

included. The MC calculation is done with 3.3% enrichment ^{235}U fuel in the fuel cell to obtain (n, f) and (n, γ) reaction rates of ^{235}U and ^{238}U . With the reaction rates, the number of ^{235}U , ^{238}U , and ^{239}Pu in a certain burnup can be calculated by assuming that the reaction rates do not change in this period. The concentration of ^{235}U , ^{238}U , and ^{239}Pu at $\text{bu}_1 = 3.4 \text{ MWd/kgU}$ is given in Table 1 as the starting point of the following calculations.

The (n, f) and (n, γ) reaction rates of ^{235}U , ^{238}U , and ^{239}Pu can be simulated by using concentrations listed in Table 1. The corresponding relative reaction rates defined below are also listed in Table 1:

$$\begin{aligned}
 R'_{5,f}(r) &= \frac{R_{5,f}(r)/N_5(r)}{R_{5,f}(r=r_0/4)/N_5(r=r_0/4)}, \\
 R'_{8,f}(r) &= \frac{R_{8,f}(r)/N_8(r)}{R_{5,f}(r)/N_5(r)}, \\
 R'_{9,f}(r) &= \frac{R_{9,f}(r)/N_9(r)}{R_{5,f}(r)/N_5(r)}, \\
 R'_{5,\gamma}(r) &= \frac{R_{5,\gamma}(r)}{R_{5,f}(r)}, \\
 R'_{8,\gamma}(r) &= \frac{R_{8,\gamma}(r)/N_8(r)}{R_{5,f}(r)/N_5(r)}.
 \end{aligned} \tag{10}$$

The above equations firstly scale the reaction rate by the corresponding concentration, because the concentration is different at different radial position. The scaling cancels such difference in consideration of reaction rate. The reaction rates are then calculated relative to that of (n, f) reaction of ^{235}U . We find that the radial distribution of these relative reaction rates is almost constant except (n, γ) reaction of ^{238}U . Thus all the reaction rates except that of (n, γ) of ^{238}U can be treated in (2) with the same coefficients. The radial distributions of these reaction rates are fitted as

$$\begin{aligned}
 R_{5,f}(r) &= cN_5(r) f(r), \\
 R_{8,f}(r) &= 0.0024cN_8(r) f(r), \\
 R_{9,f}(r) &= 2.49cN_9(r) f(r),
 \end{aligned}$$

$$R_{5,\gamma}(r) = 0.23cN_5(r) f(r),$$

$$f(r) = 0.99 + 0.11e^{3.3(r/r_0-1)},$$

$$R_{8,\gamma}(r) = 0.0183cN_8(r)$$

$$\cdot \left[0.97 + 0.42e^{3.3(r/r_0-1)} + 2.85e^{50(r/r_0-1)} \right],$$

(11)

where c is the reaction rate per nucleus of (n, f) of ^{235}U at $r = r_0/4$ and canceled in (8). Please note that the same b_1 in (2) and (3) is used for all nuclei. From bu_2 , MC and analytical calculations are independent. It is straightforward to see the advantage of transforming the burnup problem to the reaction rate problem in the present work. The reaction rate actually is the most direct quantity to obtain the burnup and the concentration. In many models, the reaction rate must be obtained after solving the neutron flux problem. The present work treats the neutron flux problem in a simple way in Section 2 and considers the relative reaction rate. The validity of these considerations will be discussed later.

In the following discussion Δbu is set to be 2.85 MWd/kgU and the total burnup is calculated to $\text{bu}_{15} = 43.30 \text{ MWd/kgU}$. The local burnup from two calculations is presented in Figure 1. The analytical calculations can give almost the same results as MC calculations. The detailed data of the three burnup levels in Table 2 shows that the average errors are less than 1%.

The radial distributions of U and Pu isotopes at three burnup levels are presented in Table 3. bu_2 is the first burnup level that MC calculation and present formula are performed independently. The error between two methods at this level reflects how exactly (11) fits to the MC reaction rates. The concentration of ^{235}U changes around 10% from bu_1 (in Table 1) to bu_2 (in Table 3). The average error 0.05% indicates that the present formula well describes the isotope distribution of ^{235}U at the burnup level. The average error of the isotope distribution of ^{239}Pu is around 1%. It is partially from the large change of the concentration from bu_1 to bu_2 and partially from the coefficient of the (n, f) reaction rate for ^{239}Pu in (11). The coefficient in Table 1 is decreasing from 2.50 to 2.47. The use of 2.49 in (11) contributes to the 1% error between MC calculation and the present formula at bu_2 .

At the burnup levels bu_8 and bu_{14} , the errors become larger, indicating that the reaction rates in (11) change slightly

TABLE 2: The comparison of the local burnup (unit in MWd/kgU) at three levels given by the present formula (AN) and MC calculations.

r'/r_0	$bu_{2,MC}$	$bu_{2,AN}$	$bu_{8,MC}$	$bu_{8,AN}$	$bu_{14,MC}$	$bu_{14,AN}$
1/4	5.96	5.94	21.48	21.33	36.57	36.30
5/8	6.11	6.09	22.11	22.09	37.69	37.80
13/16	6.29	6.29	23.05	23.11	39.53	39.75
29/32	6.48	6.49	24.40	24.22	42.42	41.83
61/64	6.72	6.74	26.62	26.37	47.48	46.55
125/128	7.06	7.08	30.13	30.38	55.50	55.91
127/128	7.68	7.72	37.20	37.31	71.75	71.64
Average errors		0.32%		0.55%		0.84%

TABLE 3: The comparison of the concentrations (unit in cm^{-3}) at three burnup levels given by the present formula (AN) and MC calculations.

r'/r_0	$N_{5,MC}$	$N_{8,MC}$	$N_{9,MC}$	$N_{5,AN}$	$N_{8,AN}$	$N_{9,AN}$
	bu_2					
1/4	$6.01E + 20$	$2.17E + 22$	$6.13E + 19$	$6.00E + 20$	$2.17E + 22$	$6.09E + 19$
5/8	$5.98E + 20$	$2.17E + 22$	$6.46E + 19$	$5.98E + 20$	$2.16E + 22$	$6.43E + 19$
13/16	$5.94E + 20$	$2.16E + 22$	$7.09E + 19$	$5.94E + 20$	$2.16E + 22$	$7.08E + 19$
29/32	$5.91E + 20$	$2.16E + 22$	$8.13E + 19$	$5.91E + 20$	$2.16E + 22$	$8.16E + 19$
61/64	$5.89E + 20$	$2.16E + 22$	$1.01E + 20$	$5.89E + 20$	$2.16E + 22$	$1.02E + 20$
125/128	$5.88E + 20$	$2.16E + 22$	$1.31E + 20$	$5.88E + 20$	$2.16E + 22$	$1.35E + 20$
127/128	$5.87E + 20$	$2.15E + 22$	$1.98E + 20$	$5.87E + 20$	$2.15E + 22$	$2.02E + 20$
Average errors				0.05%	0.06%	1.06%
	bu_8					
1/4	$3.20E + 20$	$2.14E + 22$	$1.42E + 20$	$3.24E + 20$	$2.14E + 22$	$1.33E + 20$
5/8	$3.14E + 20$	$2.14E + 22$	$1.49E + 20$	$3.18E + 20$	$2.14E + 22$	$1.42E + 20$
13/16	$3.07E + 20$	$2.14E + 22$	$1.61E + 20$	$3.10E + 20$	$2.14E + 22$	$1.53E + 20$
29/32	$3.01E + 20$	$2.13E + 22$	$1.84E + 20$	$3.04E + 20$	$2.14E + 22$	$1.65E + 20$
61/64	$2.98E + 20$	$2.13E + 22$	$2.26E + 20$	$3.01E + 20$	$2.13E + 22$	$2.02E + 20$
125/128	$2.96E + 20$	$2.11E + 22$	$2.93E + 20$	$2.99E + 20$	$2.11E + 22$	$2.78E + 20$
127/128	$2.94E + 20$	$2.08E + 22$	$4.36E + 20$	$2.97E + 20$	$2.09E + 22$	$4.06E + 20$
Average errors				1.07%	0.03%	7.03%
	bu_{14}					
1/4	$1.53E + 20$	$2.12E + 22$	$1.65E + 20$	$1.60E + 20$	$2.12E + 22$	$1.52E + 20$
5/8	$1.48E + 20$	$2.12E + 22$	$1.70E + 20$	$1.54E + 20$	$2.12E + 22$	$1.61E + 20$
13/16	$1.42E + 20$	$2.11E + 22$	$1.83E + 20$	$1.47E + 20$	$2.11E + 22$	$1.72E + 20$
29/32	$1.38E + 20$	$2.10E + 22$	$2.07E + 20$	$1.42E + 20$	$2.11E + 22$	$1.85E + 20$
61/64	$1.35E + 20$	$2.09E + 22$	$2.54E + 20$	$1.39E + 20$	$2.09E + 22$	$2.23E + 20$
125/128	$1.33E + 20$	$2.06E + 22$	$3.27E + 20$	$1.37E + 20$	$2.06E + 22$	$3.07E + 20$
127/128	$1.32E + 20$	$2.01E + 22$	$4.79E + 20$	$1.36E + 20$	$2.01E + 22$	$4.43E + 20$
Average errors				3.36%	0.07%	7.89%

during burnup. The details will be discussed later. It can be seen that the radial distribution of N_9 does not change much after a few periods because the production and reaction rates find a balance at such distribution. Both the comparisons of the local burnup and the isotope distributions imply that the present simple and analytical formula can give very nice description if a starting point is given.

As the present model is constrained in a single rod, it is worth examining its validity in a more realistic case, such as in an assembly. Figure 2 shows the model of an assembly which has the same size for each fuel rod as the previous single one. There are 24 positions for the control rods and one position in the center for the detectors. In the present calculation,

the control rods are not inserted and the rod for detectors is filled with water. The reaction rates of the fuel rods in the assembly are simulated by setting all fuel rods in the same concentrations as the single rod at a certain burnup level. The single rod model is compared with four selected fuel rods in the assembly, marked in Figure 2.

The relative reaction rates, defined by (11), in the single rod and four rods in the assembly are compared at the burnup level bu_2 in Table 4. The relative reaction rates of all the five rods are generally similar, especially for the important (n, f) reactions of ^{235}U and ^{239}Pu . The relative reaction rate of (n, γ) reaction of ^{238}U in the single rod is a few percent less than those in the four rods in the assembly. A slight modification

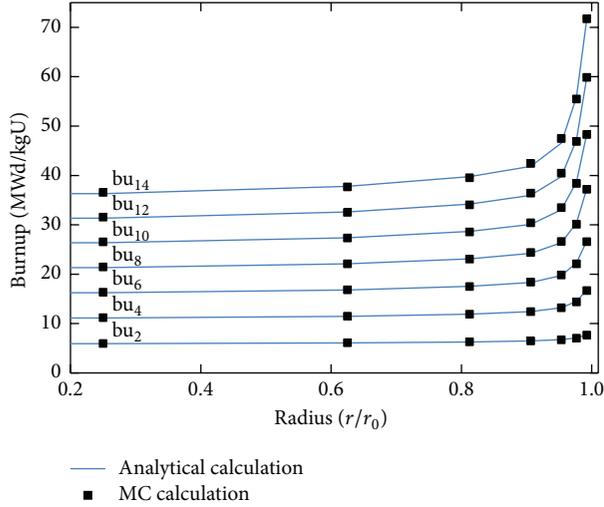


FIGURE 1: The comparison of the local burnup given by the present formula and MC calculations.

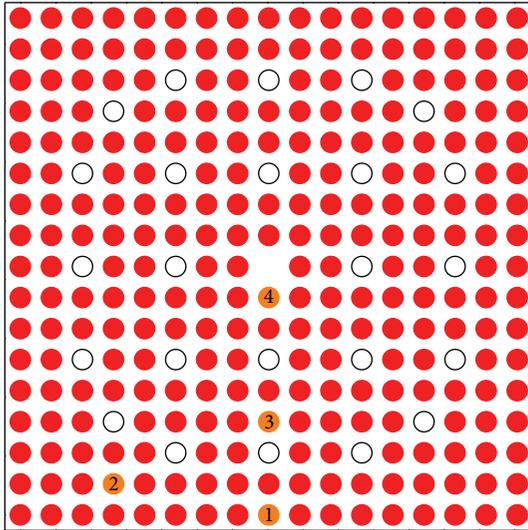


FIGURE 2: The model of an assembly, with filled and empty circle for fuel and control rods, respectively. Four selected rods are marked.

can be applied for (11) to fit to the fuel rods in the assembly. In the case of assembly, it is clear to see that the relative reaction rates are almost constant for all the four fuel rods, while the reaction rates are a little different depending on the position of the fuel rods, seen from $R_{5,f}(\text{rod } i)/R_{5,f}(\text{rod } 1)$ in Table 4.

Table 5 presents the comparison of the relative reaction rates between the single rod and rod 1 in the assembly at the burnup levels bu_9 and bu_{15} . As relative reaction rates in the four rods in the assembly are similar to each other, only the data of rod 1 are shown in Table 5. At both bu_9 and bu_{15} , the (n, f) reactions of ^{235}U and ^{239}Pu are similar in both rods, while the relative reaction rate of (n, γ) of reaction ^{238}U in the single rod is a few percent larger than that in rod 1. The situations are similar to that at bu_2 . The comparisons in Tables 4 and 5 imply that the single rod model is a nice estimation of the fuel rods in the assembly.

TABLE 4: The comparison of the relative reaction rates for a single fuel rod and four selected fuel rods in an assembly at bu_2 .

r'/r_0	$R'_{5,f}$	$R'_{8,f}$	$R'_{9,f}$	$R'_{5,\gamma}$	$R'_{8,\gamma}$	$R_{5,f}(\text{rod } i)/R_{5,f}(\text{rod } 1)$
Single						
1/4	1.00	0.0026	2.43	0.23	0.0186	
5/8	1.02	0.0025	2.43	0.23	0.0192	
13/16	1.05	0.0024	2.43	0.23	0.0206	
29/32	1.07	0.0024	2.42	0.23	0.0235	
61/64	1.08	0.0023	2.42	0.23	0.0289	
125/128	1.09	0.0023	2.42	0.23	0.0376	
127/128	1.09	0.0023	2.42	0.23	0.0561	
Rod 1						
1/4	1.00	0.0025	2.44	0.23	0.0178	
5/8	1.02	0.0024	2.43	0.23	0.0185	
13/16	1.05	0.0023	2.42	0.23	0.0197	
29/32	1.07	0.0023	2.42	0.23	0.0222	
61/64	1.08	0.0022	2.42	0.23	0.0269	
125/128	1.09	0.0022	2.42	0.23	0.0352	
127/128	1.10	0.0022	2.42	0.23	0.0521	
Rod 2						
1/4	1.00	0.0025	2.42	0.23	0.0179	0.99
5/8	1.02	0.0024	2.42	0.23	0.0184	0.99
13/16	1.05	0.0023	2.41	0.23	0.0197	1.00
29/32	1.07	0.0023	2.40	0.23	0.0225	1.00
61/64	1.09	0.0022	2.40	0.23	0.0277	1.00
125/128	1.09	0.0022	2.40	0.23	0.0355	1.00
127/128	1.10	0.0022	2.40	0.23	0.0538	1.00
Rod 3						
1/4	1.00	0.0023	2.43	0.23	0.0173	1.05
5/8	1.02	0.0023	2.43	0.23	0.0178	1.05
13/16	1.05	0.0022	2.42	0.22	0.0191	1.06
29/32	1.07	0.0021	2.41	0.22	0.0220	1.06
61/64	1.09	0.0021	2.41	0.22	0.0271	1.06
125/128	1.09	0.0021	2.41	0.22	0.0358	1.06
127/128	1.10	0.0021	2.41	0.22	0.0533	1.06
Rod 4						
1/4	1.00	0.0023	2.42	0.22	0.0170	1.08
5/8	1.03	0.0022	2.42	0.22	0.0175	1.09
13/16	1.05	0.0021	2.41	0.22	0.0190	1.09
29/32	1.07	0.0021	2.40	0.22	0.0216	1.09
61/64	1.08	0.0020	2.40	0.22	0.0268	1.09
125/128	1.09	0.0020	2.40	0.22	0.0349	1.09
127/128	1.10	0.0020	2.39	0.22	0.0526	1.09

It is worth considering why such simple formula (11) works. Take $R'_{9,f}(r)$, for example,

$$R'_{9,f}(r) = \frac{R_{9,f}(r)/N_9(r)}{R_{5,f}(r)/N_5(r)} = \frac{\int_E \phi(r, E) \sigma(9, E) dE}{\int_E \phi(r, E) \sigma(5, E) dE}, \quad (12)$$

which is the ratio of the one-group effective cross section. An approximately constant $R'_{9,f}(r)$ indicates constant neutron dynamics for the ratio between the fission reaction of ^{239}Pu

TABLE 5: The comparison of the relative reaction rates for a single fuel rod and the fuel rod in an assembly at bu_9 and bu_{15} .

r'/r_0	$R'_{5,f}$	$R'_{8,f}$	$R'_{9,f}$	$R'_{5,\gamma}$	$R'_{8,\gamma}$
bu ₉ single					
1/4	1.00	0.0025	2.23	0.23	0.0183
5/8	1.02	0.0025	2.24	0.23	0.0190
13/16	1.04	0.0024	2.25	0.23	0.0205
29/32	1.06	0.0023	2.26	0.23	0.0233
61/64	1.07	0.0023	2.26	0.23	0.0287
125/128	1.08	0.0023	2.27	0.23	0.0374
127/128	1.08	0.0023	2.27	0.23	0.0559
bu ₉ rod 1					
1/4	1.00	0.0024	2.23	0.23	0.0175
5/8	1.02	0.0024	2.24	0.23	0.0182
13/16	1.04	0.0023	2.25	0.23	0.0197
29/32	1.06	0.0022	2.26	0.23	0.0222
61/64	1.07	0.0022	2.26	0.23	0.0272
125/128	1.07	0.0022	2.27	0.23	0.0354
127/128	1.08	0.0022	2.28	0.23	0.0523
bu ₁₅ single					
1/4	1.00	0.0022	2.18	0.23	0.0168
5/8	1.02	0.0022	2.19	0.23	0.0174
13/16	1.04	0.0021	2.20	0.22	0.0188
29/32	1.05	0.0021	2.21	0.22	0.0214
61/64	1.06	0.0021	2.22	0.22	0.0265
125/128	1.06	0.0020	2.22	0.23	0.0346
127/128	1.07	0.0020	2.23	0.23	0.0510
bu ₁₅ rod 1					
1/4	1.00	0.0021	2.18	0.22	0.0161
5/8	1.02	0.0021	2.19	0.22	0.0166
13/16	1.04	0.0020	2.20	0.22	0.0178
29/32	1.05	0.0020	2.20	0.22	0.0203
61/64	1.06	0.0020	2.22	0.22	0.0251
125/128	1.06	0.0020	2.21	0.22	0.0327
127/128	1.07	0.0019	2.22	0.22	0.0486

and ^{235}U along the radial direction. Although the one-group effective cross section changes as the function of r , the ratio of the one-group effective cross section of each reaction included in the present study remains almost the same except the (n, γ) reaction of ^{238}U . One of the advantages of the present method is the consideration of the reaction rate compared with the previous methods [12–14]. Because the local burnup and the isotope distributions do not directly depend on the neutron flux but on the reaction rate, it is an alternative method which considers the properties of the latter one. The TRANSURANUS model considers the constant neutron flux and the one-group effective cross sections during Δbu . The assumption in the present model is actually the constant ratio of the one-group effective cross sections, which is relatively easy to be achieved.

From Tables 1, 4, and 5, it is seen that the relative reaction rates change not much along the radial direction and among burnup levels. It should be mentioned that the relative (n, γ) reaction rates of ^{239}Pu are also close to constant. It is

neglected in the present calculation because it links to other Pu isotopes which are not included in the present study. If the error of a few percent is acceptable, (11) can be performed independently until bu_{15} because the relative reaction rates are almost independent of both radius (except the (n, γ) reaction of ^{238}U) and burnup. More exact investigations need to consider that the relative reaction rates are not exactly constant as the burnup increases. Like $R'_{9,f}$ decreases from 2.49 in bu_2 to 2.25 in bu_9 , seen from Tables 4 and 5. This is why the difference of isotope distributions between the MC and the present calculations becomes larger as the increment of the burnup. One can use the present formula to obtain the concentration at a certain burnup level, such as bu_4 , resimulate the reactions with the concentrations through MC, and refit the coefficients in (11).

The present calculation is limited to ^{235}U , ^{238}U , and ^{239}Pu to examine their validity in a simple case. It is expected that it can be expanded to more complicated case, such as the consideration of other Pu isotopes and other nuclides which played important role in the reactor, such as the minor actinide and the poisons. In that case, a starting point is also needed to obtain the parameters in (11). In addition, the present calculation constrains Δbu to compare with the MC calculations. In principle, the change of bu , Δbu , can be rather small which results in bu being a continuous variable of the reaction rates depending on the burnup and radius. In the case of small Δbu , the assumption of constant reaction rates in (8) is more reasonable.

For a more exact study, the present method can be used together with the MC calculation. For example, starting from bu_1 , the reaction rates and the concentrations can be calculated with rather small Δbu up to bu_2 . The output is used for the next MC calculation. If Δbu is rather small, pure MC calculation is very time consuming from bu_1 to bu_2 . But with the supplement of the present work, more exact and relatively quick results are expected.

In practice, one can use the reaction rates in (11) with the concentrations at bu_1 to calculate $\Delta N(r)$ in (8) with small Δbu , such as 0.01 MWd/kgU. The next step is to use the new concentrations to calculate the reaction rates in (11) and then the next $\Delta N(r)$ through (8). After 285 steps, the concentrations at bu_2 are obtained and can be used for the next MC calculation. It is actually the Euler method with very small steps, which is expected to be more exact. In (8), the reaction rates (actually the neutron flux and the concentrations) are assumed to be constant during Δbu . But both the neutron flux and the concentrations change when the burnup changes. For detail, the concentration is in the reaction rate in the numerator of (8). The effect of the neutron flux in (8) is reflected by the integral of the reaction rates (the total fission reaction rate) in the denominator. At the different burnup level, the total fission rate and its distribution in each isotope are different, which corresponds to the different neutron flux. If the calculation between bu_1 and bu_2 is separated to many small steps, the neutron flux and concentrations are reconsidered for each step.

The present method is also helpful for solving the properties of the fuel rods at the different positions in an assembly or

an reactor core. As discussed before, the relative reaction rates are almost constant in the fuel rod at the different position in the assembly. Only one factor is needed to describe the reaction rates in each fuel rod. One can simulate at an initial level through the MC method to obtain the factors for each fuel rod and investigate the evolution of the local burnup and isotope distributions for all fuel rods at certain average burnup level.

4. Summary

In conclusion, an analytical and simple formula is suggested to calculate the reaction rates as well as the burnup and the isotope distributions as the function of radius. The parameters of the formula are fitted to the reaction rates of a given burnup level. Starting from the same burnup level, the present formula can give very nice description compared with a MC calculation from the code TRIPOLI-4. The reaction rates depend on the concentrations and the neutron flux, which both vary along the radial direction and at the different burnup levels. The present work finds almost constant relative reaction rates on these two degrees of freedom (except the (n, γ) reaction of ^{238}U on the degree of freedom of the radius), which provides a solid physical explanation on the simple formula used to calculate the local burnup and the isotope distributions.

Conflict of Interests

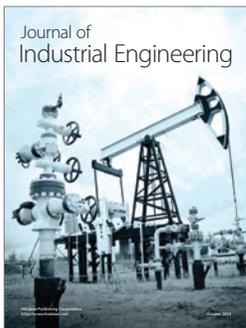
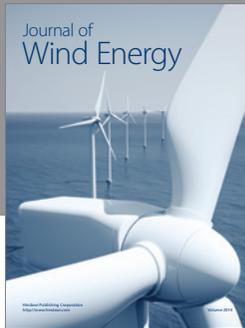
The authors declare that there is no conflict of interests regarding the publication of this paper.

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References

- [1] K. Nogita and K. Une, "Irradiation-induced recrystallization in high burnup UO_2 fuel," *Journal of Nuclear Materials*, vol. 226, no. 3, pp. 302–310, 1995.
- [2] C. B. Lee and Y. H. Jung, "An attempt to explain the high burnup structure formation mechanism in UO_2 fuel," *Journal of Nuclear Materials*, vol. 279, no. 2-3, pp. 207–215, 2000.
- [3] Y.-H. Koo, B.-H. Lee, J.-S. Cheon, and D.-S. Sohn, "Pore pressure and swelling in the rim region of LWR high burnup UO_2 fuel," *Journal of Nuclear Materials*, vol. 295, no. 2-3, pp. 213–220, 2001.
- [4] J. Noirot, L. Desgranges, and J. Lamontagne, "Detailed characterisations of high burn-up structures in oxide fuels," *Journal of Nuclear Materials*, vol. 372, no. 2-3, pp. 318–339, 2008.
- [5] M. Amaya, J. Nakamura, and T. Fuketa, "The effects of irradiation condition and microstructural change on lattice parameter, crystal lattice strain and crystallite size in high burnup UO_2 pellet," *Journal of Nuclear Materials*, vol. 392, no. 3, pp. 439–446, 2009.
- [6] V. Di Marcello, A. Schubert, J. van de Laar, and P. V. Uffelen, "Extension of the TRANSURANUS plutonium redistribution model for fast reactor performance analysis," *Nuclear Engineering and Design*, vol. 248, pp. 149–155, 2012.
- [7] C. X. Yuan, C. Qi, and F. R. Xu, "Shell evolution in neutron-rich carbon isotopes: unexpected enhanced role of neutron–neutron correlation," *Nuclear Physics A*, vol. 883, pp. 25–34, 2012.
- [8] C. X. Yuan, T. Suzuki, T. Otsuka, F. Xu, and N. Tsunoda, "Shell-model study of boron, carbon, nitrogen, and oxygen isotopes with a monopole-based universal interaction," *Physical Review C*, vol. 85, no. 6, Article ID 064324, 12 pages, 2012.
- [9] C. X. Yuan, C. Qi, F. Xu, T. Suzuki, and T. Otsuka, "Mirror energy difference and the structure of loosely bound proton-rich nuclei around $A = 20$," *Physical Review C*, vol. 89, no. 4, Article ID 044327, 2014.
- [10] K. Lassmann, C. O'Carroll, J. van de Laar, and C. T. Walker, "The radial distribution of plutonium in high burnup UO_2 fuels," *Journal of Nuclear Materials*, vol. 208, no. 3, pp. 223–231, 1994.
- [11] K. Lassmann, C. T. Walker, and J. van de Laar, "Extension of the TRANSURANUS burnup model to heavy water reactor conditions," *Journal of Nuclear Materials*, vol. 255, no. 2-3, pp. 222–233, 1998.
- [12] A. Schubert, P. Van Uffelena, J. van de Laara, C. T. Walkera, and W. Haeckb, "Extension of the TRANSURANUS burn-up model," *Journal of Nuclear Materials*, vol. 376, no. 1, pp. 1–10, 2008.
- [13] C. B. Lee, D. H. Kim, J. S. Song, J. G. Bang, and Y. H. Jung, "RAPID model to predict radial burnup distribution in LWR UO_2 fuel," *Journal of Nuclear Materials*, vol. 282, no. 2-3, pp. 196–204, 2000.
- [14] A. Soba, A. Denis, L. Romero, E. Villarino, and F. Sardella, "A high burnup model developed for the DIONISIO code," *Journal of Nuclear Materials*, vol. 433, no. 1–3, pp. 160–166, 2013.
- [15] A. Soba, M. Lemes, M. E. González, A. Denis, and L. Romero, "Simulation of the behaviour of nuclear fuel under high burnup conditions," *Annals of Nuclear Energy*, vol. 70, pp. 147–156, 2014.
- [16] M. Lemes, A. Soba, and A. Denis, "An empirical formulation to describe the evolution of the high burnup structure," *Journal of Nuclear Materials*, vol. 456, pp. 174–181, 2015.
- [17] <http://www.nndc.bnl.gov/exfor/endl00.jsp>.
- [18] H. Matsumoto, M. Ouisloumen, and T. Takeda, "Development of spatially dependent resonance shielding method," *Journal of Nuclear Science and Technology*, vol. 42, no. 8, pp. 688–694, 2005.
- [19] O. Petit, F. X. Hugot, Y. K. Lee, and C. Jouanne, "TRIPOLI-4 version 4 user guide," CEA-R- 6169, CEA, 2008, <http://www.nea.fr/abs/html/nea-1716.html>.



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