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Research Article

Effect of a High Magnetic Field on Eutectoid Point Shift and Texture Evolution in 0.81C-Fe Steel

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A 12 T magnetic field has been applied to the annealing process of a 0.81%C-Fe (wt.%). It is found that the magnetic field shifts the eutectoid carbon content from 0.77 wt.% to 0.83 wt.%. The statistical thermodynamic calculations were performed to calculate the eutectoid temperature change by the magnetic field. Calculation shows that the increase of the eutectoid temperature by a 12 T field is 29°C. Synchrotron radiation measurements were performed to measure the pole figures of the samples and were analyzed by *MAUD* to determine the bulk texture of the ferrite phase in the field-treated and non-field-treated samples. Results show that although there is no specific preferred orientation appearing by applying the magnetic field, slight enhancement of (001) fiber component occurs in both the sample normal direction (ND) and the transverse direction (TD). This effect might be related to the magnetic dipolar interaction between Fe atoms in the transverse field direction.

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1. INTRODUCTION

Study of the effect of a high magnetic field on diffusional phase transformation in steels has attracted attention in recent years. So far most efforts have been made on revealing the effect of a magnetic field on phase transformation behaviors and microstructural characters in hypoeutectoid steels [1-8]. Results have shown that the magnetic field applied can increase the austenite-to-ferrite transformation temperature [1–3], accelerate the transformation process [5-7], and change the morphology and grain boundary character distribution of the product phases [5, 8]. In this work, a quasi-eutectoid steel, 0.81C-Fe, was selected and heat-treated without and with a 12 T magnetic field. The shift of the eutectoid point by the application of a high magnetic field was experimentally investigated and theoretically calculated. The influence of the magnetic field applied on the evolution of the texture of ferrite has been investigated by means of synchrotron radiation measurements.

2. EXPERIMENTAL

The material used in this study was a plain eutectoid steel with chemical composition (wt.%) 0.81%C, 0.22%Si, 0.20%Mn, 0.05%Cr, 0.014Cu, 0.019%P, 0.003%S, and bal. Fe. It was prepared by induction casting. The cast rod was twice forged in the longitudinal direction followed by the radial direction, in the temperature range $1100-868^{\circ}$ C to homogenize and refine the microstructure. Samples of dimensions $30 \text{ mm} \times 10 \text{ mm} \times 2 \text{ mm}$ were cut from the hot forged bar. They were austenitized at 830° C for 50 minutes and cooled at a rate of 2, 5, 10, and 23° C/min without and with a 12-Tesla high magnetic field. During the heat treatment, the samples were placed in the central (zero magnetic force) region (200 mm long in the field direction).

The transformed microstructure is observed with an Olympus BX61 microscope equipped with a digital camera and the analysis software package for materials science. The crystal structures of proeutectoid ferrite and proeutectoid cementite are confirmed by the indexing of the EBSD Kikuchi

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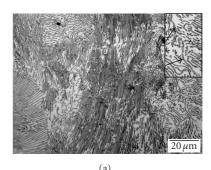
patterns acquired with a Jeol JSM 6500F FEG-SEM equipped with the HKL Channel 5 EBSD system. The area percentages of bulk ferrite appearing in the magnetic field-treated samples and the lamellar spacing of pearlite in both the field-and the non-field-treated samples were measured. The measurement was performed in 20 images of each sample to obtain a statistical representation of the results. As the lamellar spacing in each micrograph varies due to both the changing of formation temperature and the angles at which the lamellae intersect the sample-sectioning plane, the smallest lamellar spacing in each micrograph was measured. This smallest lamellar spacing obtained is related either to the pearlite formed at the very end of the transformation or to the angle, close to right angle, at which lamellae intersect the sample plane.

Synchrotron radiation measurements were performed at the Hamburg Synchrotron Radiation Laboratory (HA-SYLAB), German Electron Synchrotron (DESY), Hamburg, Germany, to measure the incomplete pole figures of the samples cooled at 2°C/min without and with a 12-Tesla high magnetic field. The measurements were carried out in transmission mode with a monochromatic synchrotron beam [9] of wavelength 0.164 Å (75.59 keV). The collimator was set to an area of 1×1 mm. The first slit was set to 1×1 mm and the second was set to 2×2 mm. During the measurement, the sample was rotated from -80° to $+80^{\circ}$ around the ω axis with a step size of 2°/step and a measurement time of 4 s/step. Data were recorded with an area detector (34.5 cm in diameter) placed behind the sample, at a distance of 115.5 cm. The data were analyzed with MAUD ("Materials Analysis Using Diffraction" program package by Lutterotti et al., University of Trento [10, 11]) and represented in inverse pole figures.

3. RESULTS AND DISCUSSION

3.1. The eutectoid point shift under a 12 T magnetic field

Figure 1 shows the microstructures of samples cooled at 2°C/min without (a) and with (b) a 12T magnetic field. Besides the main constituent of lamellar pearlite, the striking difference between the two micrographs is that in the non-field-treated specimen we observed a slight amount of proeutectoid cementite (arrowed in the zoom image in the top right corner of Figure 1(a)), which characterizes the hypereutectoid microstructure, while in the field-treated specimen we find some bulk ferrite between pearlite colonies (white areas circled in Figure 1(b)) that is the typical component of hypoeutectoid microstructure, instead of proeutectoid cementite. The crystal structures of proeutectoid cementite and the proeutectoid ferrite observed with the optical microscope were further confirmed by the indexing of their Kikuchi patterns by EBSD technique. The average area percentages of the bulk ferrite measured in the field-treated specimens at various cooling rates are shown in Table 1. It is seen that the amount of the bulk ferrite decreases with the increase of the cooling rate. This is the normal influence of the cooling rate on proeutectoid transformation. The presence of the bulk ferrite in the field-treated specimens sug-



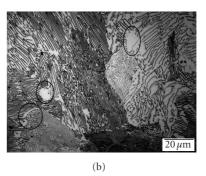


FIGURE 1: Optical micrographs of specimens austenitized at 830°C for 50 minutes and cooled at 2°C/min without (a) and with (b) a 12 T magnetic field (the field direction is horizontal). The zoom image in the right-hand corner of (a) shows the secondary cementite, as indicated by the arrow. The magnification is 1.5 times that of the main image. The circles in (b) mark out the proeutectoid ferrite between pearlite colonies.

gests that the magnetic field shifts the eutectoid point of the Fe-C binary system beyond the carbon content of the tested material (0.81%wt.C). Using the lever law, the carbon contents of the new eutectoid point under various cooling rates were calculated and displayed also in Table 1. As the carbon content of the equilibrium eutectoid point is obtained under equilibrium transformation condition, that is, under extreme slow cooling condition, the variation of the eutectoid carbon content with cooling rate is plotted in Figure 2 and extrapolated to zero cooling rate to obtain the equilibrium eutectoid carbon content. The extrapolated equilibrium eutectoid carbon content is 0.8287%(wt.). This value is noticeably different from that calculated in [3] (0.795 wt.%).

The lamellar spacing of samples fully austenitized and cooled at various cooling rates (2, 5, 10, and 23°C/min) without and with a 12 T magnetic field was also measured and is shown in Figure 3. It is seen that, at all the cooling rates tested, the lamellar spacing obtained is larger with the magnetic field than without. As the austenite to pearlite transformation is diffusional and involves the formation of the carbon-depleted ferrite and carbon-rich cementite, the lamellar spacing of pearlite depends on the diffusion length of carbon atoms that is temperature related. Therefore, the larger spacing corresponds to the higher formation temperature. This lamellar spacing increase resulting from the magnetic field applied evidences that the magnetic field also shifts

Y. D. Zhang et al.

Table 1: Average area percentages of the bulk ferrite and the standard deviation in 0.81C-Fe specimens austenitized at 830°C for 50 minutes and cooled at various cooling rates with a 12 T magnetic field, and the calculated eutectoid carbon content by using lever law and the standard deviation.

Cooling rate (°C/min)	Area percentage of ferrite (%)	Eutectoid carbon content (wt.%)
2	2.153 ± 0.850	0.827 ± 0.0070
5	1.905 ± 0.857	0.825 ± 0.0071
10	1.519 ± 0.372	0.822 ± 0.0030
23	1.277 ± 0.452	0.820 ± 0.0037

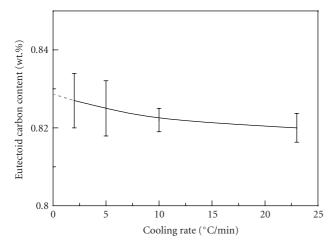


FIGURE 2: Eutectoid carbon content change with cooling rate. Black solid line: from the measured result. Gray line: extrapolation to the slow cooling rates following the changing tendency.

the eutectoid point to the high temperature side. As it is almost impossible to measure—in temperature scale—the eutectoid point shift in situ under a high magnetic field, its determination through theoretical calculation may be useful.

Let us remind that the eutectoid point of Fe-C system is the intersection of the Ae₃ line (austenite/ferrite γ/α equilibrium boundary) and the Ae_{cm} line (austenite/cementite γ /cem equilibrium line). By using the well-established statistical thermodynamic models, the Ae₃ and Ae_{cm} lines can be calculated, so the eutectoid composition and temperature can be determined. It is known that the driving force for austenite to proeutectoid ferrite transformation, $\Delta G^{\gamma-\alpha+\gamma}$, is directly related to the equilibrium position (composition and temperature) of Ae₃ line and is expressed as follows:

$$\Delta G^{\gamma \to \alpha + \gamma} = RT \left[x^{\gamma} \ln \frac{a_{\rm C}^{\gamma / \alpha}}{a_{\rm C}^{\gamma}} + (1 - x^{\gamma}) \ln \frac{a_{\rm Fe}^{\gamma / \alpha}}{a_{\rm Fe}^{\gamma}} \right], \tag{1}$$

where x^{γ} is the mole fraction of carbon in the initial austenite, R is the gas constant, T is absolute temperature, $a_j^{\gamma/\alpha}$ is the activity of C or Fe in austenite on the γ/α boundary, and a_j^{γ} is the activity of C or Fe in the initial austenite. By definition, the driving force of a phase transformation is the

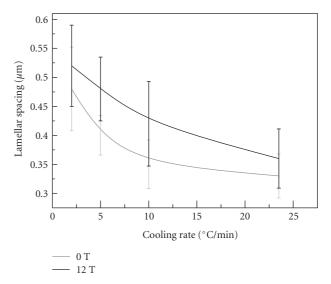


FIGURE 3: Average lamellar spacing of specimens austenitized at 830°C for 50 minutes and cooled at a rate of 2, 5, 10, and 23°C/min without and with a 12 T magnetic field.

Gibbs free energy difference between the product and parent phase. It is known that a magnetic field lowers the Gibbs free energy of a magnetized phase [5-7] according to its magnetization. The amount lowered is $\int_0^M \vec{B} \cdot d \vec{M}$ for ferromagnetic phase [12] and $(1/2\mu_0)\chi B^2$ for paramagnetic phase [12], where $B = B_0 + \mu_0 M$, B_0 is the magnetic induction of the applied field, μ_0 is the permeability of free space, M is the magnetization, and χ is the magnetic susceptibility. As ferrite (or cementite) and austenite have different magnetization under the same magnetic field, their Gibbs free energy changes by the magnetic field are different. In this way, the phase equilibrium between the parent and the product phase is altered. Assume that under the magnetic field, the γ/α (or y/cem) boundary $x^{y/i}$ (mole fraction of carbon in austenite on Ae₃ or Ae_{cm} line) moves to ${}^{M}x^{\gamma/i}$. The activity of C or Fe in austenite at the new γ/α (or γ /cem) boundary is ${}^{M}a_{i}^{\gamma/i}$, thus the total driving force under the magnetic field for the austenite-to-proeutectoid ferrite transformation can be expressed as

$$\Delta G^{\gamma \to \alpha + \gamma} + {}^{M}\Delta G^{\gamma \to \alpha + \gamma} = RT \left[x^{\gamma} \ln \frac{{}^{M} a_{C}^{\gamma/\alpha}}{a_{C}^{\gamma}} + (1 - x^{\gamma}) \ln \frac{{}^{M} a_{Fe}^{\gamma/\alpha}}{a_{Fe}^{\gamma}} \right]. \tag{2}$$

Substituting (1) into (2) and letting x^{γ} take the equilibrium carbon content at the γ/α boundary $x^{\gamma/\alpha}$, we obtain

$${}^{M}\Delta G^{\gamma-\alpha+\gamma} = RT \left[x^{\gamma/\alpha} \ln \frac{{}^{M} a_{\rm C}^{\gamma/\alpha}}{a_{\rm C}^{\gamma/\alpha}} + (1 - x^{\gamma/\alpha}) \ln \frac{{}^{M} a_{\rm Fe}^{\gamma/\alpha}}{a_{\rm Fe}^{\gamma/\alpha}} \right]. \tag{3}$$

As for γ /cem boundary ${}^M x^{\gamma/Fe_3C}$, it can be obtained according to the way to obtain x^{γ/Fe_3C} in [13] as follows:

$$\Delta G^{\text{Fe}_3\text{C}} + {}^{M}\Delta G^{\text{Fe}_3\text{C}-\gamma} = RT \ln^{M} a_{\text{C}}^{\gamma/\text{Fe}_3\text{C}} + 3RT \ln^{M} a_{\text{Fe}}^{\gamma/\text{Fe}_3\text{C}}, \tag{4}$$

where $\Delta G^{\text{Fe}_3\text{C}} = 39828 - 193.296T + 22.345T \ln T$ [14], the Gibbs free energy change of the formation of 1 mol cementite from 3 mol of γ -Fe and 1 mol of graphite, and ${}^M\Delta G^{\text{Fe}_3\text{C}-\gamma}$ is magnetic Gibbs free energy difference between cementite and austenite that is determined by the magnetic susceptibility difference between the two phases. From the quasi-chemical model [15–17], the general expression of the activity of carbon and iron in austenite is

$$\ln a_{\rm C}^{\gamma} = 5\ln \frac{1 - 2x^{\gamma}}{x^{\gamma}} + \frac{6w_{\gamma}}{RT} + 6\ln \left(\frac{\delta_{\gamma} - 1 + 3x^{\gamma}}{\delta_{\gamma} + 1 - 3x^{\gamma}}\right) + \frac{\Delta \overline{H}_{\gamma} - \Delta \overline{S}_{\gamma}^{xs} T}{RT},$$

$$\ln a_{\text{Fe}}^{\gamma} = 5 \ln \frac{1 - x^{\gamma}}{1 - 2x^{\gamma}} + 6 \ln \left[\frac{1 - 2J_{\gamma} + (4J_{\gamma} - 1)x^{\gamma} - \delta_{\gamma}}{2J_{\gamma}(2x^{\gamma} - 1)} \right], \tag{5}$$

where $\delta_{\gamma} = \left[1 - 2(1 + 2J_{\gamma})x^{\gamma} + (1 + 8J_{\gamma})(x^{\gamma})^{2}\right]^{1/2}$ and $J_{\gamma} = 1 - \exp(-w_{\gamma}/RT)$, w_{γ} is the pairwise interaction energy of carbon in austenite, $\Delta \overline{H}_{\gamma}$ and $\Delta \overline{S}_{\gamma}^{xs}$ are the relative partial enthalpy and nonconfigurational entropy of austenite. We finally take $w_v = 5880$ J/mol, $\Delta \overline{H}_v = 44400$, and $\Delta \overline{S}_v^{xs} = 17.2$ from Shiflet et al. [18] (after trying various sets of data from published literature and verifying with the Fe-C diagram without a magnetic field). By using a model based on the itinerant electron theory as implemented by Sakoh and Shimizu [19], a density functional-based method in conjunction with statistical approximations [20] and the Weiss molecular field model for ferromagnetism [21], the temperature variations of susceptibilities of austenite and cementite and the magnetization of ferrite can be calculated, and thus ${}^{M}\Delta G^{\gamma-\alpha+\gamma}$ and $^{M}\Delta G^{\text{cem}-\gamma}$ can be obtained. Substituting (5) into (3) and (4) and using the Newton-Raphson iterative algorithm, part of the phase diagram of Fe-C binary system without and with a 12 T magnetic field was calculated and is shown in Figure 4. For comparison and completion, the y/α and y/cem equilibrium lines without magnetic field are also calculated by using related equations [13] and the α/γ equilibrium lines without and with magnetic field are also calculated by using the related equations [13] and data [22] and are shown in the same figure. It is seen that the influence of the magnetic field is mainly on Ae₃ line. The calculated eutectoid carbon content and temperature without and with a 12 T magnetic field is 0.779 wt.%C; 725.71°C and 0.847 wt.%C; 754.68°C. The calculated eutectoid carbon contents without and with the magnetic field are quite close to the values determined from the experimental results. This agreement shows that the eutectoid temperature increase calculated by this method is reliable. In the case of a 12 T magnetic field, the eutectoid temperature shift is 28.97°C. Equations (3) and (4) together with (5) offer a practical and accurate method to determine the new phase equilibrium boundary lines and the eutectoid shift under the influence of a magnetic field.

3.2. Texture evolution under the effect of the applied magnetic field

Figure 5 shows the inverse pole figures of the samples heat-treated at slow cooling rate (2°C/min) without and with the

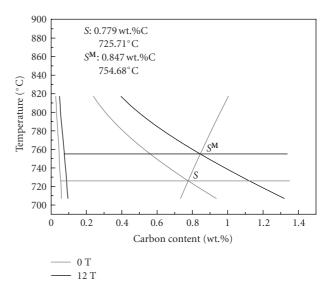


FIGURE 4: The calculated Fe-C phase diagram without and with a 12 T magnetic field.

12 T magnetic field and the corresponding sample coordinate system. Despite the textures are relatively weak, it is clearly seen that under the magnetic field there is slight enhancement of (001) fiber component in both the sample normal direction (ND) and the widthwise or transverse direction (TD), as seen in Figure 5(b). This result corroborates earlier results we found in a medium carbon plain steel heat-treated under a 12 T magnetic field [8]. Actually in the present case, both ND and TD are transverse field directions. It is known that each Fe atom carries a magnetic moment. Under the applied magnetic field, these moments tend to align along the field direction. Then, there exists the dipolar interaction between neighboring Fe atoms. They attract each other along the field direction but repel each other along the transverse field directions (ND and TD in the present study). Correlatively, the distance between neighboring atoms tends to decrease along FD and increase along ND and TD to minimize the total energy of the system. For ferrite, the carbon atoms are located in the octahedral interstices, as shown in Figure 6 [8]. The interstices are flat in the (001) direction. The occupation of the carbon atom in this interstice exerts an expansion stress on its neighboring iron atoms along the (001) direction. This gives rise to the lattice distortion and creates distortion energy. If such a (001) direction of a grain was parallel to the transverse field direction (ND or TD), the lattice distortion energy would be reduced through increasing the atomic spacing in such (001) direction by the magnetic field. Therefore, the nucleation and growth of the grains having such (001) parallel to the ND and TD are energetically favored by the magnetic field. In this way, the (001) component is enhanced in the transverse field directions (ND and TD).

4. SUMMARY

The eutectoid carbon content and temperature of Fe-C binary system under a magnetic field have been examined

Y. D. Zhang et al.

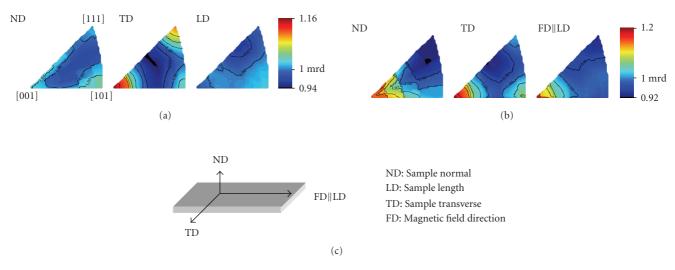


FIGURE 5: Inverse pole figures of the samples austenitized at 830°C for 50 minutes and cooled at a rate of 2°C/min without (a) and with a 12 T magnetic field (b), and the corresponding sample coordinate system. Note: mrd in the figure means "multiples of random distribution" also called trd "times random distribution".

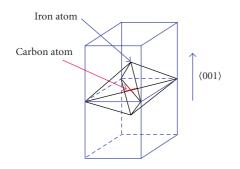


FIGURE 6: Schematic illustration of an octahedral interstice occupied by a carbon atom in bcc Fe [8].

quantitatively for the first time in the present work. The appearance of the proeutectoid ferrite confirms the shift of eutectoid carbon content. Under a 12 T magnetic field, it shifts from 0.77 wt.%C to 0.8287 wt.%C (determined from the experimental data). The increase of the pearlite lamellar spacing by the magnetic field qualitatively evidences the increase of the eutectoid temperature. By making use of the quasichemical model to calculate the corresponding activities of Fe and carbon in the related phases and considering the magnetic field influence through magnetic Gibbs free energy determined by the magnetization of the corresponding phases, the new phase equilibrium is calculated. Calculation shows that the increase of the eutectoid temperature by a 12 T field is 28.97°C.

In addition, the magnetic field enhances the (001) texture component along the sample normal and transverse directions that are both transverse field directions. This results from the dipolar interaction of the magnetic moments carried by the Fe atoms. The repelling interaction between Fe atoms in the transverse direction increases the atomic spacing that mitigates the lattice distortion induced by the solution of carbon atoms in the transverse field direction.

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