Research Article

Numerical Study of Characteristic Equations of Thermoelastic Waves Propagating in a Uniaxial Prestressed Isotropic Plate

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Thermoelastic waves propagating in an isotropic thin plate exerted by a uniaxial tensile stress are represented in this work. Characteristic equation of guided thermoelastic waves is formulated based on the theory of acoustoelasticity and classical thermoelasticity. Curve-tracing method for complex root finding is used to determine the attenuation, which is the imaginary part of the complex-value wavenumber. It is found that each plate mode of thermoelastic wave propagating in an isotropic plate with or without prestress has a minimum attenuation at a specific frequency except the $A_0$ mode. These modes are called the Lamé modes, which are the volume resonances in the thickness direction and propagate along the plate with the least energy dissipation. Frequency spectra of the phase velocity dispersion and attenuation of thermoelastic waves propagating along various orientations in the uniaxial prestressed thin plate have further been discussed.

1. Introduction

Determination of residual stresses in products is a major issue in most manufacturing industries. Both laser-induced ultrasound (LIU) [1, 2] and photoacoustics (PA) [3, 4] are the special techniques in “photothermal (PT) science” and have received intensive attention in nondestructive measurement of the residual stresses. The former determines the phase velocities from the far-field response generated by the pulsed laser, but the latter acquires the near-field response excited by the intensity-modulated CW laser. Both methods are correlative to the responses induced by “thermal acoustic waves.” Their dynamical behaviors are described based on the theory of thermoelasticity.

Research on the theory of dynamical thermoelasticity which includes the displacement and temperature coupled fields was studied and established well in a book [5]. However,
for describing the thermal transmission that propagates by means of wave with finite speed, several modified theories for the hyperbolic-type energy equation have been proposed. Differing from the classical theory of thermoelasticity, these theories are called the “generalized thermoelasticity” and classified as the followings: L-S theories [6] with one relaxation time, G-L theory [7] with two relaxation times, and three types of G-N theory [8–10] involved with the energy dissipation.

On the other hand, the thermoelastic waves or laser-induced ultrasonic waves have become rather important in recent decades. Generalized thermoelastic wave propagation in the homogeneous transversely isotropic and anisotropic media has been analyzed [11, 12]. Afterward, based on four assumptions of the classical L-S, G-L, and G-N theories, Sharma et al. [13] investigated the thermoelastic wave propagation in a homogeneous isotropic plate, and showed the wavenumber spectra of the symmetric and antisymmetric modes for the insulated and isothermal boundary conditions. Verma and Hasebe [14, 15] and Verma [16] studied the wave propagation in the infinite homogeneous isotropic and orthotropic plates as well as the anisotropic layered media using the generalized thermoelasticity with relaxation times. Salnikov and Scott [17] developed the asymptotic models of long-wave low-frequency and short-wave approximations to analyze the dispersion relations of thermoelastic waves in an infinite homogeneous isotropic plate subject to either isothermal or thermally insulated traction-free boundary conditions.

This work presents an emerging method that unifies the advantages of LIU and PA without loss of generality for anisotropic inspection, which is of significance in the residual stress measurement. The classical theory of thermoelasticity [5] and the acoustoelasticity [18] are employed to model the thermoelastic waves propagating in a copper foil under distinct uniaxial stress state. The characteristic equations of phase velocity dispersion and attenuation are derived, and the spectra for each plate mode are determined numerically. Except for the fundamental antisymmetric \((A_0)\) mode, each thermoelastic plate mode has a unique characteristic in its attenuation spectrum, in which a minimum value occurs at a specific frequency: guided thermoelastic waves induced at these specific frequencies can propagate farther away because of smaller attenuation.

2. Theoretical Formulation

2.1. Constitutive Relations

The thermoelastic effect in a stressed flat plate is formulated within the framework of the natural, initial, and final states, shown in Figure 1, originally proposed in [18] for the formulation of acoustoelasticity. Assume that there is no temperature change between the natural and initial states, that is, \(\Theta_0 = \Theta_i\). The stress component \(T_{IJ}\) and the increment of entropy \(\Xi\) satisfy the following constitutive relations:

\[
T_{IJ} = \bar{c}_{IJKL} u_{K,L} + \bar{\lambda}_{IJ} \Delta \Theta, \tag{2.1a}
\]

\[
\Xi = \bar{\lambda}_{K,L} u_{K,L} + \bar{\alpha} \Delta \Theta, \tag{2.1b}
\]

where \(I, J, K, L = 1, 2, 3\). The physical field variables \(u_{K,L}\) and \(\Delta \Theta\) indicate the strain changes and temperature rise caused by the external disturbance applied to the initial state. The material constants \(\bar{c}_{IJKL}, \bar{\lambda}_{IJ},\) and \(\bar{\alpha}\) denote the effective elastic constants, thermoelastic
coupling coefficients, and thermal constant influenced by the initial strains \( u'_{K,L'} \), respectively. They are defined by

\[
\begin{align*}
\bar{c}_{IJKL} &= (1 - e'_{NN})c_{IJKL} + c'_{IJKLMN}u'_{M,N} + c_{O|KLO}u'_{I,O} + c_{I|LOL}u'_{O,K} + c_{IJKO}u'_{L,O}, \\
\bar{\lambda}_{IJ} &= (1 - e'_{NN})\lambda_{IJ} + \lambda_{OJ}u'_{I,O} + \lambda_{IO}u'_{O,J}, \\
\bar{\alpha} &= (1 - e'_{NN})\alpha,
\end{align*}
\]

where \( \alpha \equiv \rho_C / \Theta_0 \) and \( e'_{NN} \equiv u'_{1,1} + u'_{2,2} + u'_{3,3} \) denotes the cubic dilatation. The terms \( c_{IJKL}, c'_{IJKLMN}, \lambda_{IJ}, \alpha, \rho_C, \rho_0, \) and \( \Theta_0 \) are the second- and third-order elastic constants, thermoelastic coupling coefficients, thermal constant, heat capacity, mass density, and temperature measured in the natural state. The relation between the initial strains \( u'_{K,L} \) and the initial (residual) stresses \( T'_{IJ} \) is given by \( T'_{IJ} = c_{IJKL} u'_{K,L} \).

2.2. Governing Equations

The elastic wave propagation in a medium under residual stress must satisfy the equations of motion in the initial state of the form

\[
(T'_{IJ} + T'_{JK}u_{I,K})_{,J} + \rho_i b_I = \rho_i \ddot{u}_I,
\]

where \( \rho_i \) is the mass density in the initial state and is defined by \( \rho_i = (1 - e'_{NN})\rho_0 \). The term \( \rho_i b_I \) is the body force applied to the initial state. Further, the balance of entropy and Fourier heat transfer equation in the initial state are of the form

\[
\begin{align*}
-q_{IJ} + \rho_i h &= \Theta_i \Xi, \\
q_I &= -k_{II} \Delta \Theta_I,
\end{align*}
\]
where $\Theta_i (= \Theta_0)$, $\rho_i h$, and $q_i$ are the temperature, distributed body heat source, and surface heat flux in the initial state, respectively. $k_{ij}$ is the effective thermal conductivity influenced by the initial strains $u_{k,l}^i$ and can be written as

$$k_{ij} = \left(1 - e_i^{NN}\right) k_{ij} + k_{ij}^0 \lambda_{j,ij} + k_{ij}^0 \lambda_{j,ij},$$  

(2.5)

where $k_{ij}$ is the thermal conductivity measured in the natural state. Substituting (2.1a), (2.1b) into (2.3), (2.4a), (2.4b) subsequently yields the partial differential equations of thermoelastic waves as follows:

$$\left(\tilde{c}_{ijkL} + \delta_{ik} T_{jL}^i\right) u_{k,lj} - \tilde{k}_{ij} \Delta \Theta_{ijkl} + \rho_i \lambda_{l} = \rho_i \dot{u}_l,$$

$$k_{jL} \Delta \Theta_{jL} - \Theta_i \tilde{k}_{kL} \dot{u}_{k,l} + \rho_i h = \Theta_i \tilde{h} \Delta \Theta.$$  

(2.6)

### 2.3. Thin Isotropic Plate Subjected to a Uniaxial Prestress in the $X_1$-Direction

In this study, an isotropic thin plate in the natural state is considered. Referring the schematic diagram shown in Figure 2, the residual stresses $T_{ij}^i$ are assumed to be homogeneous. Only normal stress is applied in the $X_1$-direction, and shear stress components vanish, that is, $T_{22}^i = T_{33}^i = T_{ij}^i = 0 \ (i \neq j)$. According to the relation $T_{ij}^i = c_{ijkl} u_{k,l}^i$, the initial strains $u_{k,l}^i$ and the associated cubic dilatation $e_i^{NN}$ of the isotropic plate are given as follows:

$$u_{1,1}^i = \frac{(c_{11} + c_{12}) T_{11}^i}{(c_{11} - c_{12})(c_{11} + 2c_{12})},$$

$$u_{2,2}^i = u_{3,3}^i = \frac{-c_{12} T_{11}^i}{(c_{11} - c_{12})(c_{11} + 2c_{12})},$$

$$u_{2,3}^i = u_{3,2}^i = u_{3,3}^i = u_{2,3}^i = u_{2,2}^i = u_{3,1}^i = u_{1,2}^i = 0,$$

$$e_i^{NN} = \frac{T_{11}^i}{c_{11} + 2c_{12}}.$$  

(2.7)
The existing effective material constants \(\varepsilon_{PQ}, \theta_{P},\) and \(\kappa_{P}\) \((P, Q = 1, 2, \ldots, 6)\) in the initial state appeared in (2.2a), (2.2b), and (2.5) are derived as follows:

\[
\begin{align*}
\{\bar{c}_{11}, \bar{c}_{22}, \bar{c}_{33}\}^T &= \left[\left(1 - \varepsilon_{N,N}^{1}\right)c_{11} + \varepsilon_{112}^{1}e_{N,N}^{1}\right]\{1, 1, 1\}^T \\
+ (4c_{11} + \varepsilon_{112}^{2} - \varepsilon_{112}^{1})\left\{u_{1,1}^{i}, u_{2,2}^{i}, u_{3,3}^{i}\right\}^T, \\
\{\bar{c}_{23}, \bar{c}_{13}, \bar{c}_{12}\}^T &= \left[\left(1 - \varepsilon_{N,N}^{2}\right)c_{12} + (2c_{12} + \varepsilon_{112}^{2})e_{N,N}^{1}\right]\{1, 1, 1\}^T \\
- (2c_{12} + \varepsilon_{112}^{1} - \varepsilon_{112}^{2})\left\{u_{1,1}^{i}, u_{2,2}^{i}, u_{3,3}^{i}\right\}^T, \\
\{\bar{c}_{44}, \bar{c}_{55}, \bar{c}_{66}\}^T &= \left[\left(1 - \varepsilon_{N,N}^{3}\right)c_{44} + (2c_{44} + \varepsilon_{155}^{4})e_{N,N}^{1}\right]\{1, 1, 1\}^T \\
- (2c_{44} + \varepsilon_{155}^{3} - \varepsilon_{155}^{4})\left\{u_{1,1}^{i}, u_{2,2}^{i}, u_{3,3}^{i}\right\}^T, \\
\{\bar{\lambda}_{1}, \bar{\lambda}_{2}, \bar{\lambda}_{3}\}^T &= \left(1 - \varepsilon_{N,N}^{4}\right)\lambda\{1, 1, 1\}^T + 2\lambda\left\{u_{1,1}^{i}, u_{2,2}^{i}, u_{3,3}^{i}\right\}^T, \\
\{\bar{k}_{1}, \bar{k}_{2}, \bar{k}_{3}\}^T &= \left(1 - \varepsilon_{N,N}^{5}\right)k\{1, 1, 1\}^T + 2k\left\{u_{1,1}^{i}, u_{2,2}^{i}, u_{3,3}^{i}\right\}^T.
\end{align*}
\]

According to (2.7) and (2.8), the special relations \(\bar{c}_{22} = \bar{c}_{33}, \bar{c}_{13} = \bar{c}_{12}, \bar{c}_{55} = \bar{c}_{66}, \bar{\lambda}_{2} = \bar{\lambda}_{3},\) and \(\bar{k}_{2} = \bar{k}_{3}\) are obtained. Rewriting (2.6) leads to the thermoelastic governing equations involving the effect of uniaxial prestress \(T_{11}\) as follows:

\[
\begin{align*}
\left(\bar{c}_{11}^{i}u_{1,1}^{i} + \bar{c}_{66}u_{1,22} + \bar{c}_{55}u_{1,33}\right) + (\bar{c}_{12} + \bar{c}_{66})u_{2,12} + (\bar{c}_{13} + \bar{c}_{55})u_{3,13} - \bar{\lambda}_{1}\Delta\Theta_{1} + \rho_{i}b_{1} &= \rho_{i}u_{1}^{i}, \\
\left(\bar{c}_{66}^{i}u_{2,11} + \bar{c}_{22}u_{2,22} + \bar{c}_{44}u_{2,33}\right) + (\bar{c}_{12} + \bar{c}_{66})u_{1,12} + (\bar{c}_{23} + \bar{c}_{44})u_{3,23} - \bar{\lambda}_{2}\Delta\Theta_{2} + \rho_{i}b_{2} &= \rho_{i}u_{2}^{i}, \\
\left(\bar{c}_{55}^{i}u_{3,11} + \bar{c}_{44}u_{3,22} + \bar{c}_{33}u_{3,33}\right) + (\bar{c}_{13} + \bar{c}_{55})u_{1,13} + (\bar{c}_{23} + \bar{c}_{44})u_{2,23} - \bar{\lambda}_{3}\Delta\Theta_{3} + \rho_{i}b_{3} &= \rho_{i}u_{3}^{i}, \\
\left(\bar{k}_{1}\Delta\Theta_{11} + \bar{k}_{2}\Delta\Theta_{22} + \bar{k}_{3}\Delta\Theta_{33}\right) - (\bar{\Theta}_{1}\bar{\lambda}_{1}u_{1,1}^{i} + \bar{\Theta}_{1}\bar{\lambda}_{2}u_{2,2}^{i} + \bar{\Theta}_{1}\bar{\lambda}_{3}u_{3,3}^{i}) + \rho_{i}h &= \bar{\Theta}_{1}\bar{\rho}\Delta\Theta;
\end{align*}
\]

where \(\bar{c}_{11}^{i} = \bar{c}_{11} + T_{11}^{i}, \bar{c}_{55}^{i} = \bar{c}_{55} + T_{11}^{i},\) and \(\bar{c}_{66}^{i} = \bar{c}_{66} + T_{11}^{i}.

### 2.4. Thermoelastic Waves Propagating along Any Direction from the \(X_{1}\)-Axis

The schematic diagram of a thin plate exerted by normal stress in the \(X_{1}\)-direction with the Cartesian coordinates is shown in Figure 2, in which the \(X_{3}\)-axis is the thickness direction and the \(X_{1}\)- and \(X_{2}\)-axes both extend to infinity. This plate occupies the region \(-h/2 \leq X_{3} \leq h/2,\) where \(h\) is the thickness. In the absence of both \(\rho_{i}b_{1}\) and \(\rho_{i}h\) in (2.9), all field quantities are
assumed to have a plane wave harmonic function $e^{i(\xi_i X_i + \zeta X_3 - \omega t)}$ based on the partial wave expansion (PWE) method. Then, the solutions of $u_I (I = 1, 2, 3)$ and $\Delta \Theta$ are represented as

$$
\begin{align*}
\quad u_I &= A_I e^{i(\xi_i X_i + \zeta X_3 - \omega t)}, \\
\Delta \Theta &= A_4 e^{i(\xi X_i + \zeta X_3 - \omega t)},
\end{align*}
$$

where $A_I$ and $A_4$ indicate the amplitudes of $u_I$ and $\Delta \Theta$, respectively. The term $\xi_f (f = 1, 2)$ denotes the wave vector of guided wave in the $X_1 X_2$-plane and $\zeta$ denotes the angular wavenumber in the thickness ($X_3$-) direction. The components of wave vector $\xi_f$ are defined by $\xi_1 = \xi \cos \theta$ and $\xi_2 = \xi \sin \theta$, where $\theta$ denotes the included angle of the arrowhead $n$ and the $X_1$-axis as shown in Figure 2. The parameters $\xi$ and $\omega$ are the angular wavenumber and angular frequency defined as $2\pi$ times the wavenumber $k$ and the frequency $f$, which are the reciprocal of the wavelength and period, respectively.

Substitution of (2.10) into (2.9) is followed by the thermoelastic Christoffel equations for the coupled P, SV, SH, and thermal waves in the matrix form:

$$
\begin{bmatrix}
\xi^2 a_{11} + c_{11} & c_{12} & \xi b_{13} & c_{14} \\
 c_{21} & \xi^2 a_{22} + c_{22} & \xi b_{23} & c_{24} \\
 \xi b_{31} & \xi b_{32} & \xi^2 a_{33} + c_{33} & \xi b_{34} \\
 c_{41} & c_{42} & \xi b_{43} & \xi^2 a_{44} + c_{44}
\end{bmatrix}
\begin{bmatrix}
A_1 \\
A_2 \\
A_3 \\
A_4
\end{bmatrix}
= \begin{bmatrix}
0 \\
0 \\
0 \\
0
\end{bmatrix},
$$

(2.11)

where the unknown terms are defined as follows:

$$
\begin{align*}
a_{11} &= \bar{c}_{55}, & c_{11} &= \frac{\xi^2 - \xi_1^2}{\xi_1^4} + \frac{\xi^2 - \xi_6^2}{\xi_6^4} - \omega^2 \rho, \\
a_{22} &= \bar{c}_{44}, & c_{22} &= \frac{\xi^2 - \xi_1^2}{\xi_1^4} + \frac{\xi^2 - \xi_6^2}{\xi_6^4} - \omega^2 \rho, \\
a_{33} &= \bar{c}_{33}, & c_{33} &= \frac{\xi^2 - \xi_1^2}{\xi_1^4} + \frac{\xi^2 - \xi_6^2}{\xi_6^4} - \omega^2 \rho, \\
a_{44} &= \bar{k}_3, & c_{44} &= \frac{\xi^2 - \xi_1^2}{\xi_1^4} + \frac{\xi^2 - \xi_6^2}{\xi_6^4} - \omega^2 \rho, \\
c_{12} &= c_{21} = \xi_1 \xi_2 (\bar{c}_{12} + \bar{c}_{66}), & c_{14} &= i \xi_1 \bar{\lambda}_1, & c_{41} &= \omega \Theta_i \bar{\lambda}_1, \\
b_{13} &= b_{31} = \xi_1 (\bar{c}_{13} + \bar{c}_{55}), & c_{24} &= i \xi_2 \bar{\lambda}_2, & c_{42} &= \omega \Theta_i \bar{\lambda}_2, \\
b_{23} &= b_{32} = \xi_2 (\bar{c}_{23} + \bar{c}_{44}), & b_{34} &= i \bar{\lambda}_3, & b_{43} &= \omega \Theta_i \bar{\lambda}_3.
\end{align*}
\quad
$$

(2.12)

According to the existence of a nontrivial solution in (2.11), the determinate vanishes and the eigenvalues $\pm \xi_k (k = 1, 2, 3, 4)$ must satisfy the quartic equation of $\xi^2$ as follows:

$$
a_8 \xi^8 + a_6 \xi^6 + a_4 \xi^4 + a_2 \xi^2 + a_0 = 0,
$$

(2.13)

where the coefficients $a_8, a_6, a_4, a_2,$ and $a_0$ can be obtained and sorted by employing the software MAPLE for symbolic computation. The quartic equation (2.13) can be directly
solved by quartic formula and eight complex roots $\pm \zeta_k$ ($k = 1, 2, 3, 4$) are subsequently obtained. For the definiteness of a single-value function, a constraint for root $\zeta_k$ is selected as $\text{Im}(\zeta_k) \geq 0$ to avoid the exponential increasing. The symbol “+” corresponds to the downgoing waves propagating along the positive $X_3$-direction. On the other hand, the symbol “−” denotes those upgoing waves traveling toward the negative $X_3$-direction. The eigenvector components $(A_1^\pm, A_2^\pm, A_3^\pm, A_4^\pm)^{(k)}$ with respect to $\pm \zeta_k$ satisfy the proportional relation,

$$(A_1^\pm, A_2^\pm, A_3^\pm, A_4^\pm)^{(k)} = (p_{1k}^+, p_{2k}^+, p_{3k}^+, p_{4k}^+)^{(k)} \times C_k^+,$$  

(2.14)

where $C_k^+$ denotes the unknown amplitudes and the proportional factors $(p_{1k}^+, p_{2k}^+, p_{3k}^+, p_{4k}^+) \in C$ are the determinants of corresponding submatrices (or minors) in (2.11) of the form.

$$p_{1k}^+ = \zeta_k \bigg[ c_{11} b_{43} \left( \zeta_k^2 a_{22} + c_{22} \right) + c_{12} b_{23} \left( \zeta_k^2 a_{44} + c_{44} \right) + c_{24} c_{42} b_{13} - b_{13} \left( \zeta_k^2 a_{22} + c_{22} \right) \left( \zeta_k^2 a_{44} + c_{44} \right) - c_{14} c_{42} b_{23} - c_{12} c_{24} b_{43} \bigg],$$

$$p_{2k}^+ = \zeta_k \bigg[ c_{24} b_{43} \left( \zeta_k^2 a_{11} + c_{11} \right) + c_{21} b_{13} \left( \zeta_k^2 a_{44} + c_{44} \right) + c_{14} c_{41} b_{23} - b_{23} \left( \zeta_k^2 a_{11} + c_{11} \right) \left( \zeta_k^2 a_{44} + c_{44} \right) - c_{24} c_{41} b_{13} - c_{12} c_{24} b_{43} \bigg],$$

$$p_{3k}^+ = \zeta_k \bigg[ c_{12} b_{23} \left( \zeta_k^2 a_{11} + c_{11} \right) + c_{41} b_{13} \left( \zeta_k^2 a_{22} + c_{22} \right) + c_{12} c_{21} b_{43} - b_{13} \left( \zeta_k^2 a_{11} + c_{11} \right) \left( \zeta_k^2 a_{22} + c_{22} \right) - c_{42} c_{41} b_{13} - c_{12} c_{24} b_{23} \bigg],$$

$$p_{4k}^+ = \zeta_k \bigg[ c_{12} b_{23} \left( \zeta_k^2 a_{11} + c_{11} \right) + c_{41} b_{13} \left( \zeta_k^2 a_{22} + c_{22} \right) + c_{12} c_{21} b_{43} - b_{13} \left( \zeta_k^2 a_{11} + c_{11} \right) \left( \zeta_k^2 a_{22} + c_{22} \right) - c_{42} c_{41} b_{13} - c_{12} c_{24} b_{23} \bigg],$$

(2.15)

Applying (2.1a) and (2.4b), the solutions of traction $t_I$ ($\equiv T_{3I}$, $I = 1, 2, 3$) and heat influx $q_{in}$ ($\equiv - q_3$) along the positive $X_3$-direction can be represented in the form of

$$t_I = T_{3I} = B_I e^{i\xi X_3} e^{i(\xi I X_I - \omega t)},$$

$$q_{in} = - q_3 = B_4 e^{i\xi X_3} e^{i(\xi I X_I - \omega t)},$$

(2.16)

where $B_I$ and $B_4$ indicate the amplitudes of $T_{3I}$ and $-q_3$, respectively. Following the above procedure in a similar manner, the components $(B_1^\pm, B_2^\pm, B_3^\pm, B_4^\pm)^{(k)}$ with respect to $\pm \zeta_k$ also satisfy the proportional relation,

$$(B_1^\pm, B_2^\pm, B_3^\pm, B_4^\pm)^{(k)} = (q_{1k}^\pm, q_{2k}^\pm, q_{3k}^\pm, q_{4k}^\pm)^{(k)} \times C_k^+,$$

(2.17)
where the proportional factors \( q_{1k}^+, q_{2k}^+, q_{3k}^+, q_{4k}^+ \) are given by

\[
q_{1k}^+ = i\vec{c}_{35} (\hat{\xi}_k p_{1k}^+ + \hat{\eta}_l p_{3k}^+), \quad q_{2k}^+ = i\vec{c}_{44} (\hat{\xi}_k p_{2k}^+ + \hat{\eta}_l p_{3k}^+),
\]

\[
q_{3k}^+ = i \left( \bar{c}_{13} \hat{\xi}_k p_{1k}^+ + \bar{c}_{23} \hat{\xi}_k p_{2k}^+ + \bar{c}_{33} \hat{\xi}_k p_{3k}^+ + i\bar{\xi}_3 p_{4k}^+ \right), \quad q_{4k}^+ = i \bar{\xi}_3 \hat{\xi}_k p_{4k}^+,
\]

Hence, applying the matrix technique [19] used in analysis for the layered structure, a combination of (2.10) and (2.16) yields

\[
\begin{bmatrix}
    U(X_j, X_3, t) \\
    T(X_j, X_3, t)
\end{bmatrix} = \begin{bmatrix}
    P^+ & P^- \\
    Q^+ & Q^-
\end{bmatrix} \begin{bmatrix}
    \mathbf{D}^+(X_3) & 0 \\
    0 & \mathbf{D}^-(X_3)
\end{bmatrix} \begin{bmatrix}
    \mathbf{C}^+ \\
    \mathbf{C}^-
\end{bmatrix} \epsilon^i (\zeta_j \lambda_j - \omega t),
\]

(2.19)

where \( U = \{ u_t, u_x, u_y, \Delta \Theta \}^T \) and \( T = \{ T_{31}, T_{32}, T_{33}, -q_3 \}^T \). The submatrices \( P^\pm \) and \( Q^\pm \) are the \( 4 \times 4 \) matrices with elements \( p_{ik} \) and \( q_{ik} \) as given in (2.15) and (2.18), respectively. The diagonal matrix \( \mathbf{D}^\pm(X_3) \) has a rank 4 with plane wave forms \( e^{ik\hat{\xi}X_3} \). The uncertain \( 4 \times 1 \) vector \( \mathbf{C}^\pm \) with elements \( C^\pm_k \) can be determined by the boundary conditions.

2.5. Characteristic Equation of Guided Thermoelastic Waves

Thermoelastic waves propagating in a thin plate are dispersive because of the geometric constraints on the upper and bottom boundaries. In addition, they are dissipative due to transformation between strain and thermal energies. Assume that the upper and bottom surfaces \( (X_3 = \pm h/2) \) are both traction-free and adiabatic conditions, that is, \( T_{3I} = q_3 = 0 \) \( (I = 1, 2, 3) \). Applying the above boundary conditions to (2.19), the characteristic equations for the symmetric and antisymmetric modes of thermoelastic waves, indicated by the superscript “S” and “A”, are derived in the form

\[
\Omega^{S,A}(\omega, \xi) \quad \text{or} \quad \Omega^{S,A}(f, k) \equiv \det \begin{pmatrix}
    S_A & S_A & S_A & S_A \\
    q_{11} & q_{12} & q_{13} & q_{14} \\
    q_{21} & q_{22} & q_{23} & q_{24} \\
    q_{31} & q_{32} & q_{33} & q_{34} \\
    q_{41} & q_{42} & q_{43} & q_{44}
\end{pmatrix},
\]

(2.20)

where the elements of vector \( \{ q_{1k}^S, q_{2k}^S, q_{3k}^S, q_{4k}^S \}^T \) \( (k = 1, 2, 3, 4) \) are defined as follows:

\[
q_{1k}^S = \sin(\zeta_k h/2) q_{1k}^+, \quad q_{2k}^S = \cos(\zeta_k h/2) q_{2k}^+, \quad q_{3k}^S = \cos(\zeta_k h/2) q_{3k}^+,
\]

\[
q_{4k}^S = \sin(\zeta_k h/2) q_{4k}^+, \quad q_{3k}^A = \sin(\zeta_k h/2) q_{3k}^+.
\]

(2.21)
In this study, due to energy dissipation of the propagating guided wave in the plate, the imaginary part of the complex-value wave number plays an important role. It is defined as \( k = k_r + ik_i = k_r(1 + i\gamma/2\pi) \), where \( k_i \) and \( \gamma \) are the attenuation per unit distance (Np/mm) and per wavelength (Np/\( \nu \)) respectively. The characteristic equation \( \Omega^{S,A}(f,k) \) given in (2.19) can be represented as \( \Omega^{S,A}(f,k_r,k_i) \) or \( \Omega^{S,A}(f,k_r,\gamma) \). Moreover, because of the difficulty in obtaining an exact zero solution to \( \Omega^{S,A}(f,k_r,k_i) = 0 \) numerically. Instead, minimizing \(|\Omega^{S,A}(f,k_r,k_i)|\) is the common method for finding an approximate solution. Lowe [19] developed an effective method (also called the curve tracing algorithm) to find the complex roots of the characteristic equation for acoustic guided waves. Figures 3(a) and 3(b) show the dispersion and attenuation spectra for real wavenumber \( k_r \) and imaginary wavenumber \( k_i \) with respect to frequency \( f \). There exist many roots of \((f,k_r)\) with respect to one point on the \( k_r \)-axis. Besides, the MATLAB v6.5 subroutine \texttt{fminbnd} [20] which is an algorithm by the golden section search and parabolic interpolation and the subroutine \texttt{amoeba} [21] based on the downhill simplex method are frequently used in the numerical computation.

### 3. Numerical Results and Discussion

In this study, a thin copper foil is considered as an example. The material properties [22, 23] used in numerical computation are expressed in the units of “mg”, “mm”, “\( \mu \)s”, and “k\(^\circ\)K” and listed in the first column of Table 1. Furthermore, the effective material properties under two initial states with two uniaxial prestresses 0.02\( c_{44} \) and 0.04\( c_{44} \) applied in the \( X_1 \)-direction are assembled in the second and third columns of Table 1, respectively. Obviously, according to the relations \( \bar{c}_{22} = \bar{c}_{33} \approx \bar{c}_{23} + 2\bar{c}_{44}, \bar{k}_2 = \bar{k}_3 \) in the \( X_2X_3 \)-plane, the material properties in two distinct initial states reveal the characteristic of nearly transversely isotropic. Material properties in the plane perpendicular to the direction of applied pre stressing \( T_{11} \) are quasi-isotropic.
Table 1: Material properties of the copper foil under the natural state and two initial states with two uniaxial prestresses 0.02c_{44} and 0.04c_{44} applied in the X_1-direction.

<table>
<thead>
<tr>
<th>Thickness (mm)</th>
<th>Natural state</th>
<th>Prestress $T^i_{11} = 0.02c_{44}$</th>
<th>Prestress $T^i_{11} = 0.04c_{44}$</th>
</tr>
</thead>
<tbody>
<tr>
<td>Mass density (mg/mm$^3$)</td>
<td>$\rho_0 = 8.93$</td>
<td>$\rho_i = 8.913$</td>
<td>$\rho_i = 8.895$</td>
</tr>
<tr>
<td>Elastic constants (mg/mm$^2$/s$^2$)</td>
<td>$c_{11} = 188.1$</td>
<td>$c_{11} = 183.377$</td>
<td>$c_{11} = 178.655$</td>
</tr>
<tr>
<td></td>
<td>$c_{12} = 108.9$</td>
<td>$c_{22} = c_{33} = 187.343$</td>
<td>$c_{22} = c_{33} = 186.587$</td>
</tr>
<tr>
<td></td>
<td>$c_{44} = 39.6$</td>
<td>$c_{23} = c_{32} = 111.926$</td>
<td>$c_{23} = c_{32} = 114.952$</td>
</tr>
<tr>
<td></td>
<td>$c'_{11} = -1894$</td>
<td>$c'_{12} = -754$</td>
<td>$c'_{12} = -106.094$</td>
</tr>
<tr>
<td></td>
<td>$c'_{12} = 56$</td>
<td>$c'_{44} = -401$</td>
<td>$c'_{44} = 37.704$</td>
</tr>
<tr>
<td></td>
<td>$c'_{55} = -287$</td>
<td>$c'_{46} = 57$</td>
<td>$c'_{46} = 39.636$</td>
</tr>
<tr>
<td>Temperature (K)</td>
<td>$\Theta_0 = 0.300$</td>
<td>$\Theta_i = 0.300$</td>
<td>$\Theta_i = 0.300$</td>
</tr>
<tr>
<td>Thermal constant (mg/mm$^2$/s$^2$·K$^2$)</td>
<td>$\alpha = (\rho_0 C_E)/\Theta_0 = 11.129$</td>
<td>$\alpha = 11.107$</td>
<td>$\alpha = 11.085$</td>
</tr>
<tr>
<td>Thermoelastic coupling coeff. (mg/mm$^2$/s$^2$·K$^2$)</td>
<td>$\lambda = (c_{11} + 2c_{12})\gamma = 6.697$</td>
<td>$\lambda_1 = 6.782$</td>
<td>$\lambda_1 = 6.867$</td>
</tr>
<tr>
<td></td>
<td>$\mu_{12} = \mu_{32} = 6.648$</td>
<td>$\mu_2 = \mu_3 = 6.599$</td>
<td>$\mu_2 = \mu_3 = 6.599$</td>
</tr>
<tr>
<td>Thermal conductivity (mg/mm$^2$/s$^2$·K$^2$)</td>
<td>$k = 0.398 \times 10^{-3}$</td>
<td>$k_1 = 0.403 \times 10^{-3}$</td>
<td>$k_1 = 0.408 \times 10^{-3}$</td>
</tr>
<tr>
<td></td>
<td>$k_2 = k_3 = 0.395 \times 10^{-3}$</td>
<td>$k_2 = k_3 = 0.392 \times 10^{-3}$</td>
<td>$k_2 = k_3 = 0.392 \times 10^{-3}$</td>
</tr>
</tbody>
</table>

$c_E = 3.74$ is the heat capacity (mg/°C·K$^2$), and $\gamma = 0.0165$ is the thermal expansion coefficient (1/K°C).

The speeds of the longitudinal (L0) and transverse (S0) waves, and Lamé mode (Lame0), and the Rayleigh wave (R0) in the natural state are, respectively, defined by

$$c_{L0} = \sqrt{c_{11}/\rho_0},$$

$$c_{S0} = \sqrt{c_{44}/\rho_0},$$

$$c_{\text{Lame0}} = \sqrt{2c_{S0}},$$

$$c_{R0} = \frac{0.87 + 1.12\nu}{1 + \nu}c_{S0},$$

where Poisson’s ratio $\nu = 0.367$ for the copper foil. The formulas given in (3.1c) and (3.1d) can be referred to the books by Graff [24] and Achenbach [25], respectively. In the absence of the thermoelastic coupling effect, the speeds of the longitudinal (L) and transverse (S) waves along the $X_1$, $X_2$, and $X_3$-directions in the initial (prestressed) state are defined as follows:

$$c_{L1}^{[100]} = \sqrt{c_{11}^{[100]}/\rho_i},$$

$$c_{S1}^{[100]} = \sqrt{c_{55}^{[100]}/\rho_i},$$

$$c_{L1}^{[010]} = \sqrt{c_{22}^{[010]}/\rho_i},$$

$$c_{S1}^{[010]} = \sqrt{c_{44}^{[010]}/\rho_i},$$

$$c_{L1}^{[001]} = \sqrt{c_{33}^{[001]}/\rho_i},$$

$$c_{S1}^{[001]} = \sqrt{c_{55}^{[001]}/\rho_i},$$

$$c_{L2}^{[100]} = \sqrt{c_{22}^{[100]}/\rho_i},$$

$$c_{S2}^{[100]} = \sqrt{c_{44}^{[100]}/\rho_i},$$

$$c_{L2}^{[010]} = \sqrt{c_{33}^{[010]}/\rho_i},$$

$$c_{S2}^{[010]} = \sqrt{c_{55}^{[010]}/\rho_i},$$

$$c_{L3}^{[100]} = \sqrt{c_{33}^{[100]}/\rho_i},$$

$$c_{S3}^{[100]} = \sqrt{c_{44}^{[100]}/\rho_i},$$

$$c_{L3}^{[010]} = \sqrt{c_{22}^{[010]}/\rho_i},$$

$$c_{S3}^{[010]} = \sqrt{c_{55}^{[010]}/\rho_i},$$

$$c_{L3}^{[001]} = \sqrt{c_{33}^{[001]}/\rho_i},$$

$$c_{S3}^{[001]} = \sqrt{c_{55}^{[001]}/\rho_i},$$

$$c_{\text{Lame0}} = \sqrt{2c_{S1}^{[001]}},$$

$$c_{R0}^{[100]} = \frac{0.87 + 1.12\nu}{1 + \nu}c_{S1}^{[001]},$$

$$c_{R0}^{[010]} = \frac{0.87 + 1.12\nu}{1 + \nu}c_{S1}^{[010]},$$

$$c_{R0}^{[001]} = \frac{0.87 + 1.12\nu}{1 + \nu}c_{S1}^{[001]}.$$
where the superscript “[IJK]” denotes the polarized direction of plane wave. Next, their corresponding differences of speeds between the natural and initial states are defined by

\[ \Delta c_{L1}^{[100]} = c_{L1}^{[100]} - c_{L0}, \quad \Delta c_{S1}^{[001]} = c_{S1}^{[001]} - c_{S0}, \quad \Delta c_{S1}^{[010]} = c_{S1}^{[010]} - c_{S0}, \]  
\[ \Delta c_{L2}^{[010]} = c_{L2}^{[010]} - c_{L0}, \quad \Delta c_{S2}^{[001]} = c_{S2}^{[001]} - c_{S0}, \quad \Delta c_{S2}^{[100]} = c_{S2}^{[100]} - c_{S0}, \]  
\[ \Delta c_{L3}^{[001]} = c_{L3}^{[001]} - c_{L0}, \quad \Delta c_{S3}^{[010]} = c_{S3}^{[010]} - c_{S0}, \quad \Delta c_{S3}^{[100]} = c_{S3}^{[100]} - c_{S0}. \]  

(3.5)

(3.6)

(3.7)

The speeds of the Lamé modes along the \( X_1 \)- and \( X_2 \)-directions and their corresponding differences are given by

\[ c_{\text{Lame}1} = \sqrt{2} c_{S3}^{[100]}, \quad \Delta c_{\text{Lame}1} = \sqrt{2} \Delta c_{S3}^{[100]}, \]  
\[ c_{\text{Lame}2} = \sqrt{2} c_{S3}^{[010]}, \quad \Delta c_{\text{Lame}2} = \sqrt{2} \Delta c_{S3}^{[010]}, \]  

(3.8)

(3.9)

and they are related to the speeds of transverse (S) waves along the \( X_3 \)-direction according to the thickness resonance behavior of the Lamé mode. Equation (3.9) can provide an exact solution the Lamé modes because of the nearly isotropic property in the \( X_2 \)-\( X_3 \)-plane for whereas (3.8) only provided the trend of speed change for the Lamé modes owing to the orthorhombic property in the \( X_1 \)-\( X_3 \)-plane. Substituting the material properties listed in Table 1 into (3.1a)–(3.1d) to (3.9), the resultant data for the natural states and two initial states, that is, two prestresses: 0.02\( c_{44} \) and 0.04\( c_{44} \) applied in the \( X_1 \)-direction, are assembled in Table 2.

According to the results via the complex root finding, the frequency spectra of the dispersion (real wavenumber \( k_r \)) and attenuation (imaginary wavenumber \( k_i \)) for the symmetric modes (red lines) and antisymmetric modes (black lines) of a thermoelastic wave propagating in the copper foil in the natural state (without any prestress) are shown in Figures 3(a) and 3(b). The frequency spectra of the phase velocity \( c_{\text{ph}} \) and semilogarithmic plot of attenuation \( k_i \) are also shown in Figures 4(a) and 4(b), where the phase velocity \( c_{\text{ph}} \) is defined as \( f/k_r \). In Figure 4(a), the four additional blue dashed lines, labeled by “\( c_{L0} \)” “\( c_{S0} \)” “\( c_{\text{Lame0}} \)” and “\( c_{R0} \)” indicate the phase velocities of values 4.590, 2.106, 2.978, and 1.972 mm/\( \mu \)s due to (3.1a)–(3.1d). As frequency increases, both phase velocities of the \( A_0 \) and \( S_0 \) modes converge to a constant value corresponding to the Rayleigh wave speed \( c_{R0} = 1.972 \) mm/\( \mu \)s.

In Figure 4(b), the attenuation spectrum of each mode, except the \( A_0 \) mode, has a close-to-zero minimum at a specific frequency, which is called the “Lamé mode” [24]. The Lamé modes travel at a specific wave speed \( c_{\text{Lame0}} \) and can be indicated using a dimensionless parameter \( k_r h = n + 1/2 \) for the symmetric modes \( S_n(n = 0, 1, 2, \ldots) \) and \( k_r h = m \) for the antisymmetric modes \( A_m(m = 1, 2, 3, \ldots) \). Reflecting on the “\( c_{\text{Lame0}} \)”-labeled blue dashed line shown in Figure 4(a), the specific frequencies, that is, \( f = (c_{\text{Lame0}}/h) \cdot (n + 1/2) \) for the \( S_n \) modes and \( f = (c_{\text{Lame0}}/h) \cdot m \) for the \( A_m \) modes, can be also observed. The Lamé modes represent the volume resonances in the thickness direction and propagate along the plate with the close-to-zero attenuation. This means that the thermoelastic waves can propagate farther away without energy dissipation. Moreover, the attenuations of the \( A_0 \) and \( S_0 \) modes merge together at the frequency range higher than 40 MHz. The convergent value is about \( 0.5 \times 10^{-3} \) mm\(^{-1}\) at 80 MHz.

Let the copper foil be exerted by a tensile stress in the \( X_1 \)-direction. Two cases of applied stresses 0.02\( c_{44} \) and 0.04\( c_{44} \) are considered. Figures 5(a) and 5(b) show the
Table 2: Collected data of the wave speeds under the natural state and two initial states with two uniaxial prestresses 0.02c_{44} and 0.04c_{44} applied in the X_1-direction.

<table>
<thead>
<tr>
<th>Wave speed (mm/μs)</th>
<th>Longitudinal wave</th>
<th>Shear wave</th>
<th>Corresponding differences of wave speed due to (3.5)–(3.7)</th>
<th>Lamé mode</th>
</tr>
</thead>
<tbody>
<tr>
<td>Natural state</td>
<td>c_{L0} = 4.590</td>
<td>c_{S0} = 2.106</td>
<td>—</td>
<td>c_{Lame0} = 2.978</td>
</tr>
<tr>
<td>Prestress</td>
<td>c_{L1}^{[100]} = 4.546</td>
<td>c_{S1}^{[001]} = 2.130</td>
<td>Δc_{L1}^{[001]} = -0.044</td>
<td>c_{Lame1} = 2.982</td>
</tr>
<tr>
<td>T_{11} = 0.02c_{44}</td>
<td>c_{L2}^{[010]} = 4.585</td>
<td>c_{S2}^{[010]} = 2.109</td>
<td>Δc_{L2}^{[010]} = -0.005</td>
<td>Δc_{Lame1} = 0.0004</td>
</tr>
<tr>
<td></td>
<td>c_{L3}^{[001]} = 4.585</td>
<td>c_{S3}^{[001]} = 2.109</td>
<td>Δc_{L3}^{[001]} = -0.005</td>
<td>c_{Lame2} = 2.908</td>
</tr>
<tr>
<td></td>
<td>c_{L1}^{[100]} = 4.502</td>
<td>c_{S1}^{[010]} = 2.154</td>
<td>Δc_{L1}^{[010]} = -0.088</td>
<td>Δc_{Lame2} = -0.0707</td>
</tr>
<tr>
<td>Prestress</td>
<td>c_{L2}^{[010]} = 4.580</td>
<td>c_{S2}^{[010]} = 2.006</td>
<td>Δc_{L2}^{[010]} = -0.010</td>
<td>c_{Lame2} = 2.838</td>
</tr>
<tr>
<td>T_{11} = 0.04c_{44}</td>
<td>c_{L3}^{[001]} = 4.580</td>
<td>c_{S3}^{[001]} = 2.112</td>
<td>Δc_{L3}^{[001]} = -0.010</td>
<td>Δc_{Lame2} = -0.1414</td>
</tr>
</tbody>
</table>

Figure 4: Frequency spectra of (a) the phase velocity c_{ph} and (b) the semilogarithmic plot of attenuation k_{a} for the symmetric modes (red lines) and antisymmetric modes (black lines) for the thermoelastic waves propagating in an isotropic copper foil under the natural state (without any prestress).

frequency spectra of phase velocity dispersion and semilogarithmic attenuation for the symmetric modes (red lines) and antisymmetric modes (black lines) of thermoelastic waves propagating along the X_1-direction. Figures 6(a) and 6(b) show those of thermoelastic waves propagating along the X_2-direction. Comparison of Figures 5(a) and 6(a) indicates that the shift of each dispersion curve depends on the bulk wave speed differences between the natural and stressed states. According to Table 1, the changes of bulk wave speeds Δc_{L1}^{[100]} and Δc_{S1}^{[001]} in the X_1-direction due to the tensile prestress T_{11} = 0.02c_{44} are −0.044 and
0.024 mm/μs, respectively. As shown in Figure 5(a), the resulting phase velocities of plate waves increase over a broad frequency range but decrease in the vicinity of longitudinal wave speed $c_{L0} = 4.590 \text{ mm/μs}$. Similarly, the phase velocities of the plate waves along the $X_2$-direction decrease in accordance with the changes of bulk wave speeds $\Delta c_{L2}^{[10]} = -0.005$ and $\Delta c_{S2}^{[01]} = -0.050 \text{ mm/μs}$. Figure 6(a) shows that the dispersion curves of higher modes change distinguishably in the region of higher frequency and wavenumber.

On the other hand, as shown in Figures 5(b) and 6(b), the attenuation spectrum of each mode has a minimum at a specific frequency. These specific modes represent the volume resonances in the thickness direction and propagate along the plate with the least energy dissipation. Figure 5(b) shows that the minimum attenuation of each mode, except the $A_0$ mode, increases as the tensile prestress in the same direction as wave propagation increases. This phenomenon is caused by the uniaxial prestress $T_{11}$ and leads to the orthorhombic symmetry in the $X_1X_3$-plane, for example, the values $\bar{c}_{11}$, $\bar{c}_{33}$, $\bar{c}_{13}$, $\bar{c}_{55}$, $\bar{\lambda}_1$, $\bar{\lambda}_3$, $\bar{\kappa}_1$, and $\bar{\kappa}_3$ shown in Table 1. Next, Figure 6(b) shows that the specific frequencies of the Lamé modes are reduced if a tensile prestress is applied in the orientation perpendicular to the direction of wave propagation. The reductions of these specific frequencies can result from the changes of isotropic property in the $X_2X_3$-plane, that is, the specific relations $\bar{c}_{22} = \bar{c}_{33} \approx \bar{c}_{23} + 2\bar{c}_{44}$, $\bar{\lambda}_2 = \bar{\lambda}_3$, and $\bar{\kappa}_2 = \bar{\kappa}_3$ shown in Table 1. Therefore, the feature of close-to-zero attenuation of the Lamé modes is directly correlated with the isotropic material property in the sagittal plane of propagating thermoelastic guided wave.

In the previous illustrations, the horizontally polarized motion (SH wave) has been decoupled from the thermoelastic waves propagating along the $X_1$- and $X_2$-directions. Figures 7(a) and 7(b) show the frequency spectra of phase velocity dispersion and semilogarithmic attenuation of thermoelastic waves propagating along the direction inclined at $45^\circ$ to the $X_1$-axis in a copper foil which is tensilely prestressed by $0.02c_{44}$ in the

![Diagram](image-url)
Figure 6: Frequency spectra of (a) the phase velocity $c_{ph}$ and (b) the semilogarithmic plot of attenuation $k$ for the symmetric modes (red lines) and antisymmetric modes (black lines) of a thermoelastic wave propagating along the $X_3$-direction in the copper foil under the natural state (without any prestress) and two initial states with two uniaxial prestresses 0.02$c_{44}$ and 0.04$c_{44}$ applied in the $X_1$-direction.

Figure 7: Frequency spectra of (a) the phase velocity $c_{ph}$ and (b) the semilogarithmic plot of attenuation $k$ for the symmetric modes (red lines) and antisymmetric modes (black lines) for the thermoelastic waves propagating at 45° orientation to the $X_1$-axis in a copper foil under the initial state with uniaxial prestress 0.02$c_{44}$ applied in the $X_1$-direction.

$X_1$-direction. Owing to that the off-axis traveling wave motions are neither polarized in the sagittal plane nor horizontally polarized, and the P, SV, SH, and thermal waves are coupled. As shown in Figure 7(b), the “even” numbered antisymmetric modes (solid black lines), except the $A_0$ mode, and the “odd” numbered symmetric modes (solid red lines) possess the Lamé modes. These modes have the minimum attenuation at some specific
frequencies, which is similar to the feature previously mentioned. However, the Lamé mode vanishes from the “odd” numbered antisymmetric modes (dash-dotted black lines) and the “even” numbered symmetric modes (dash-dotted red lines) due to the participation of the horizontally polarized motions, that is, SH waves. This phenomenon represents that the energy of thermoelastic guided wave will dissipate into the region out of the sagittal plane during propagating along the orientation between the \( X_1 \)- and \( X_2 \)-directions. The special regions neighboring the intersecting dispersion curves represent coupling motion of different modes. Therefore, it is of difficulty to interpret the mode-converted response generated at those regions using LIU or PA technique.

4. Conclusion

In this paper, a copper foil exerted by a uniaxial tensile prestress in the \( X_1 \)-direction is considered as an example. Applying the curve-tracing method for the root finding of complex wavenumber, the numerical evidence indicates that the response of thermoelastic waves can characterize the uniaxial residual stresses in the plate-like structures through the frequency spectra of phase velocity dispersion and wavenumber attenuation, especially in the direction of wave propagation parallel or perpendicular to the loading direction. Except for the \( A_0 \) mode, the attenuation spectra of thermoelastic waves have steep descents at the specific frequencies where their unique minima occur. The attenuation increases with increasing tensile prestress in the same direction as wave propagation. If the prestress orientation is perpendicular to the direction of thermoelastic wave propagation, the reductions in these specific frequencies of Lamé modes are proportional to the magnitudes of applied stress. Along the perpendicular direction, the phase velocities apparently decrease as the prestress increases. Furthermore, the isotropic material property in the sagittal plane of propagating thermoelastic guided wave can affect the appearance of close-to-zero attenuation.

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References
