

APPENDIX

The resistance, capacitances and inductances of circuit model are evaluated by the formulas available in the literature. They are given here for reference:

The capacitor C_i is equal to the average of C_{ia} and C_{ib} for a better approximation

$$C_i = \frac{1}{2}(C_{ia} + C_{ib}) \quad (1)$$

Where [8-10]:

$$C_{ia} = (\epsilon_r + 1)l_f[(N - 3)A_1 + A_2] \quad (2)$$

$$A_1 = 4.409 \tanh \left\{ \left(0.55 \left(\frac{h}{w_c} \right)^{0.45} \right) \right\} (F/\mu m), A_2 = 9.92 \tanh \left\{ \left(0.52 \left(\frac{h}{w_c} \right)^{0.5} \right) \right\} (F/\mu m) \quad (3)$$

$$C_{ib} = \frac{\epsilon_{eff}(f)10^{-3}}{18\pi} \frac{K(k)}{K(k')} (N-1)l_f (pF), \frac{K(k)}{K(k')} = \begin{cases} \frac{1}{\pi} \ln \left(2 \frac{1+\sqrt{k}}{1-\sqrt{k}} \right) & 0.707 \leq k \leq 1 \\ \frac{\pi}{\ln \left(2 \frac{1+\sqrt{k'}}{1-\sqrt{k'}} \right)} & 0 \leq k \leq 0.707 \end{cases} \quad (4)$$

$$k = \tan^2 \left(\frac{\pi a}{4b} \right), a = \frac{w_f}{2}, b = \frac{w_f + gap}{2}, k' = \sqrt{1-k^2} \quad (5)$$

The interdigital capacitor is considered as a transmission line with width w_c and characteristic impedance Z_{oc} in order to determine its capacitance and inductance. Its magnetic behaviour is neglected [11]. The interdigital capacitor and its circuit modal is shown in Fig. 1.

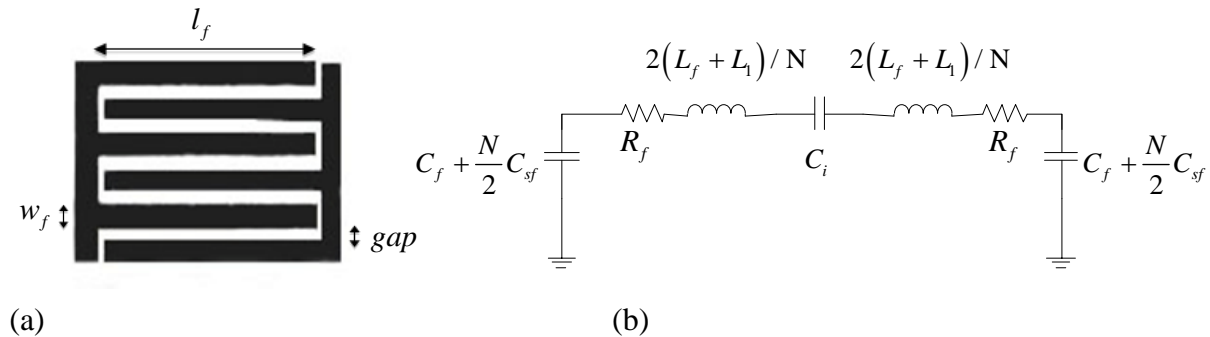


Fig. 1. Interdigital Capacitor. (a) Layout; (b) Circuit Model

$$L_f = \frac{1}{2} \frac{Z_{0c}(f) \sqrt{\epsilon_{effc}(f)}}{c_0} l_f(H), C_f = \frac{1}{2} \frac{\sqrt{\epsilon_{effc}(f)}}{Z_{0c}(f) C_0} (F) \quad (6)$$

The capacitance and inductance of step junctions are [8]:

$$C_{sf} = 1370 \times h^{(m)} \times \frac{\sqrt{\epsilon_{effc}(f)}}{Z_{oc}} \left(1 - \frac{w_f}{w_c}\right) \left(\frac{\epsilon_{effc}(f) + 0.3}{\epsilon_{effc}(f) - 0.258}\right) \times \left(\frac{\frac{w_c}{h} + 0.264}{\frac{w_c}{h} + 0.8}\right) (pF) \quad (7)$$

$$L_{sf} = h^{(m)} \left[1 - \frac{Z_{oc}}{Z_{of}} \sqrt{\frac{\epsilon_{effc}(f)}{\epsilon_{efff}(f)}}\right]^2 (\mu H) \quad (8)$$

The shunt stub is modeled by a capacitor C_{st} parallel to a series combination of L_{st} and R_{st} . The via is modeled by L_{via} connected in series with R_{via} and the formulas are given in [8]. The circuit model is shown in Fig. 2(a). The T-junction controls the right-handed part of the CRLH and its model is given by [16] which is shown in Fig. 2(b).

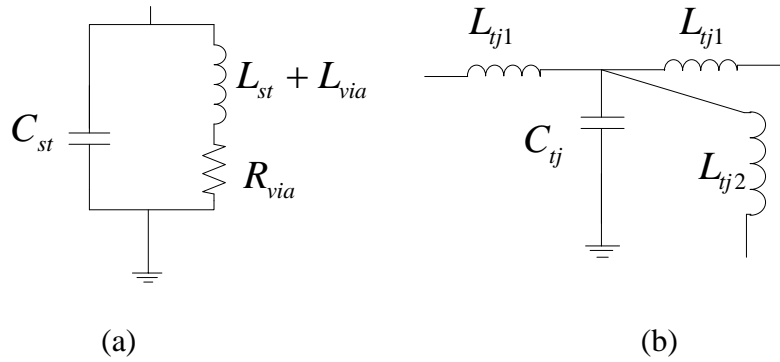


Fig. 2.(a)Shorted Stub Model (b)T-Junction Model.

$$C_{st} = \epsilon_0 \epsilon_r \frac{l_{st} w_{st}}{h} (F), L_{st} = \frac{Z_{0st}(f) \sqrt{\epsilon_{effst}(f)}}{c_0} l_{st} (H), R_{st} = \frac{l_{st}}{\sigma_c w_{st} t} (\Omega) \quad (9)$$

$$L_{via} = \frac{\mu_0}{2\pi} \left[h \times \ln\left(\frac{h - \sqrt{r_{via}^2 + h^2}}{r_{via}}\right) + \frac{3}{2} (r_{via} - \sqrt{r_{via}^2 + h^2}) \right] (pH) \quad (10)$$

Where h is in μm and r_{via} is the radius of via.

$$R_{via} = R(f=0) \sqrt{1 + \frac{f}{f_\delta}(\Omega)}, f_\delta = \frac{1}{\pi \mu_0 \sigma_c t^2} \quad (11)$$

The parameters of T-junction are [8]:

$$\frac{C_{ij}}{w_{ij1}} = \frac{100}{\tanh(0.0072Z_{02})} + 0.64Z_{02} - 261(pF / m) \quad (12)$$

$$L_{ij1} = -w_{ij2} \left(\frac{w_{ij2}}{h} (-0.016 \frac{w_{ij1}}{h} - 0.064) + \frac{0.016}{w_{ij1}/h} \right) L_{w_1} (nH) \quad (13)$$

$$L_{ij2} = \left\{ \left(0.12 \frac{w_{ij1}}{h} - 0.47 \right) \frac{w_{ij2}}{h} + 0.195 \frac{w_{ij1}}{h} - 0.357 + 0.0283 \sin(\pi \frac{w_{ij1}}{h} - 0.75\pi) \right\} L_{w_2} (nH) \quad (14)$$

The microstrip line connecting the interdigital capacitor and meander inductor is [8,11]:

$$L_l = 2 \times 10^{-4} d_1 \left(\ln \left(\frac{d_1}{w_m + t} \right) + 1.193 + 0.2235 \frac{w_m + t}{d_1} \right) \times K_g (nH) \quad (15)$$

Where,

$$K_g = 0.57 - 0.145 \ln \left(\frac{w_m}{h} \right) \quad (16)$$

And meander inductance is

$$L_m = 0.004 l_m \left[\ln \left(\frac{d_2}{w_m + t} \right) + 1.5 + \ln k - \ln e \right] \quad (17)$$