

Research Article

A Cost Effective Desalination Plant Using a Solar Chimney with Recycled Aluminum Can Collector

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The main objective of the work was to use solar energy for desalination of water. A solar chimney desalination system, which includes the solar chimney, solar collector, evaporation system, and passive condenser, was designed and built. The air enters into collector and gets heated and released at the bottom of chimney. Due to draught effect dry air goes upward. The air is humidified by spraying salt water into the hot air stream using a mistifier at the middle of chimney. Then, the partial vapours contained in the air are condensed to give desalinated water. The performance of the integrated system including power and potable water production was estimated and the results were discussed. With a 3.4 m height setup, experimental test rig was capable of evaporating 3.77 L water daily condensing 2.3 L water. It is compact in nature as it is easy to assemble and disassemble. It can be used for purifying rain water in summer under rain water harvesting. Because of using country wood, recycled Al cans, and GI sheet in fabrication, it is lower in cost.

1. Introduction

Energy is the backbone of technological and economic development. Our energy requirements have increased in the years following the industrial revolution. This rapid increase in use of energy has created an imbalance between demand and supply. If this growing world energy demand is to be met with fossil fuels, they will be no more available for producing the energy after a few years. It is the need of today's world to concentrate on renewable energy sources to satisfy the demand and conserve our finite natural resources for the generations to come.

Khan [1] explains basic concepts of alternative energy related to issue of sustainability and pollution reduction. In reality alternative energy refers to any form of energy other than that derived via fossil fuel combustion. Various forms of alternative energy sources are solar, wind, biogas/biomass, tidal energy, geothermal energy, fuel cell, hydrogen energy, small hydropower, and so forth. Solution to long-term energy problems will come only through research and development in the field of alternative energy sources. There are many benefits of alternate sources of energy such as sustainability, eco-friendly environment, human health, and enhanced income.

Human body needs three requisites for its smooth functioning—oxygen, water, and food. First requirement to live is oxygen since one cannot survive more than a few minutes without taking oxygen. Water has been ranked as second only to oxygen as essential for life. The average adult body consists of 55 to 75% water. Water available on earth is about 79%. Out of this 97% is sea water and rest is fresh water (Figure 1). Drinking water scarcity is increasing day by day (Figure 2). 3% fresh water resources are not enough for the world. Safe drinking water could be defined as water that which can be used as drinking water for humans without causing them any harm, either short term or long term Rajesh and Suresh [2]. A lot of research has gone into finding the contaminant impurities in water that are harmful to humans.

One of the best ways to get pure water is by desalinating sea water or brackish water. Desalination is a process, which is used to remove dissolved minerals in feed water sources, such as seawater or nonpotable water for getting pure water. The safest and most effective water purifier in the market today works on reverse osmosis principle. But it is high in cost. It is proposed to use a solar chimney integrated with a recycled aluminium can solar collector to produce desalinated water.

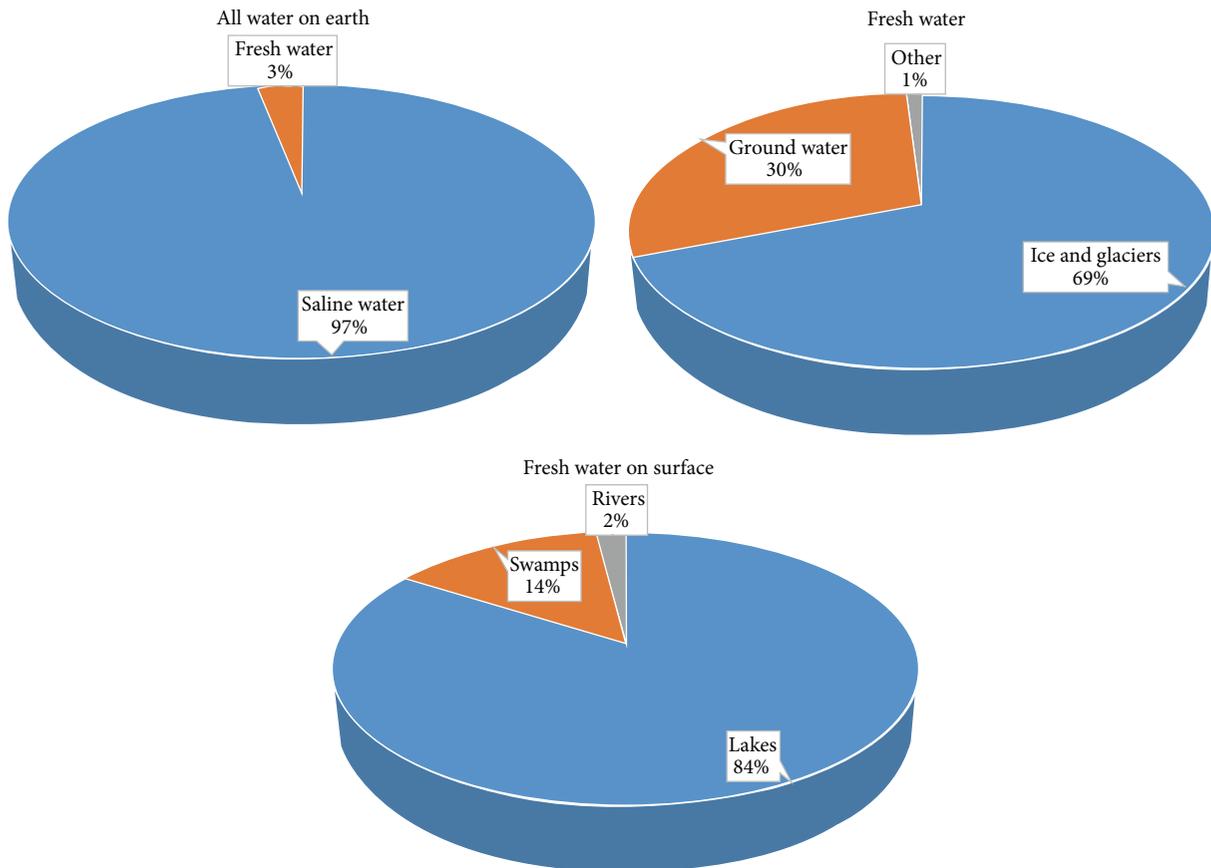


FIGURE 1: Types of water available on earth (courtesy: Pacific Islands Applied Geoscience Commission), <http://www.pacificwater.org/pages.cfm/water-services/water-demand-management/water-distribution>.



FIGURE 2: Water scarcity in villages (courtesy: Google images).

Two points considered to achieve are reduction in cost of equipment and ease of producing desalinated water.

2. Literature Review

Commercial desalination techniques have been heavily dependent on the use of electrical energy as the main source of energy. Consequently, with the high dependency on electrical energy, desalination processes also contribute to the increase in the production of greenhouse gasses emitted from the production of electrical energy.

2.1. Solar Desalination Methods. Solar desalination is a method which utilizes solar radiation to produce desalinated water. Based on this method different solar desalination plants are developed. This method is mainly classified into two types: (a) direct method and (b) indirect method.

In direct method, a solar collector is coupled with a distilling mechanism and the process is carried out in one simple cycle. Solar stills (Figure 3) of this type are employed in many small desalination and distillation plants. Water production by direct method solar distillation is proportional to the area of the solar surface and incidence angle. According to Pastohr et al. [3] solar productivity of still is low and occupies huge space. Indirect solar desalination consists of either photovoltaic or fluid based collectors. Production by indirect method is dependent on the thermal efficiency of the plant and the cost per unit produced is generally reduced by an increase in scale. Many different plant arrangements have been theoretically analysed, experimentally tested, and in some cases installed.

2.2. Solar Chimney Desalination System. According to Haaf [4], Solar Chimney Power Generation System was presented by a German Professor Schlarich in 1978. A pilot solar chimney power plant was constructed at Manzanares, Spain, in 1981. Since then, more and more researchers have

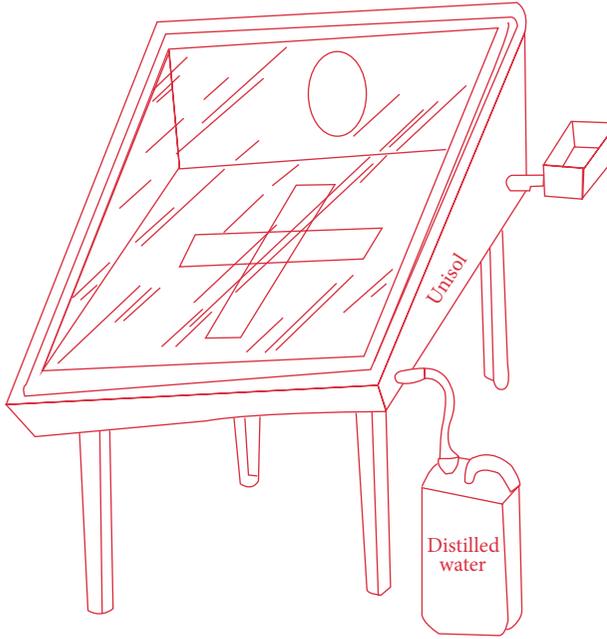


FIGURE 3: Solar still (courtesy: Unisol Company), <http://www.unisol.com/solardistillwaterplant.htm>.

shown strong interest in such solar chimney power systems. Moreover, solar chimney is a promising large-scale power technology that absorbs direct and diffused solar radiation and produces power without releasing greenhouse gasses.

The concept of combination of solar chimney and sea-water desalination was proposed by B. A. Kashiwa and C. B. Kashiwa [5] in 2008 for the first time. They introduced a theoretical basis for the feasibility of the solar cyclone, suggesting that an experimental study of the separation device would be worthwhile. Akbarzadeh et al. [6] suggested the utilization of a solar pond instead of collector in the solar chimney and built a small model of that. The thermal energy that is stored at the bottom of the solar pond is used in a heat exchanger to heat up the air. Kalogirou [7] did sea water desalination using renewable sources of energy. Nawayseh et al. [8], Alhazmy [9], and Zhou et al. [10] did their work in getting water production by humidification and dehumidification of sea water. At first Niroomand and Amidpour [11] integrated solar chimney for power generation and seawater desalination.

Khoo and Lee [12] developed the complete solar desalination system (Figure 4) consisting of solar collector, chimney, desalination system, and passive condenser system. The air inside the solar collector is heated up as the solar radiation strikes the solar collector. Hence, the hot air moves from the solar collector to the chimney and rises to the top due to stack effect. Inside the chimney, a sprinkler (mistifier) sprays a fine mist of saline water downwards. The hot air rising up the chimney would then transfer heat by convection into fine water droplets, causing evaporation of the saline water. The water vapour produced will then be carried up and out of the chimney by the air flow from where it will come into contact with a passive condenser and condenses to form fresh liquid

TABLE 1: Dimensions and specifications of RAC solar collector.

| S. number | Assumption(s) | Specification(s) |
|-----------|---------------------------------------|--------------------------|
| 1 | Solar irradiation | 1000 W/m ² |
| 2 | Collector area | 1.5 × 0.6 m ² |
| 3 | Base plate temperature | Constant |
| 4 | Absorber plate material | Black painted aluminium |
| 5 | Ambient temperature | 28°C |
| 6 | Inlet air temperature | 32°C |
| 7 | Double glazing | Applied |
| 8 | Wind velocity | 2 m/s |
| 9 | Tempered glass emissivity | 0.88 |
| 10 | Tempered glass transmissivity | 0.85 |
| 11 | Tilt angle of collector | 80° |
| 12 | Testing Time | 8 hours per day |
| 13 | Black paint absorber plate emissivity | 0.09 |

water droplets which are collected in an external reservoir. Alvarez et al. [13] designed solar collectors using recycled aluminium cans at an affordable cost.

3. Proposed Desalination Plant

In the present work a recycled aluminium can collector was integrated with a solar chimney. The experimental setup mainly comprises solar collector, chimney, condenser, sprinkler system, submersible water pump, exhaust fan, solar panel for power supply, and stand. A mathematical model was developed, sensitivity analyses were conducted to optimize the system, and the design parameters obtained were then used in the dimensioning and sizing of the components for fabrication. With the understanding of complete system every subsystem operation was developed and a simplified version was described with the flowchart shown in Figure 4.

3.1. Recycled Al Can (RAC) Solar Air Collector. The collector was made up of recycled aluminium soft drink cans to be built at a low cost. The baffle plate of the collector consists of 9 circular section air flow channels each made by joining 8 recycled Al cans (Figures 5 and 6). Table 1 shows the specifications of the solar collector. For ensuring forced convection, an exhaust fan, which runs with solar energy, was used. Tempered glass and Al sheet were used at the bottom of collector to ensure more heat absorption and reflection. Optimum tilt angle of collector is obtained from Ulgen [14].

3.2. Chimney with a Bend. Chimney was circular in cross section and made with galvanized sheet (Figure 7) in order to prevent rust formation. Height of chimney (without stand) was 1.5 m and diameter of chimney was 0.16 m. The bottom of the chimney was left open to ensure ease of access into the chimney during experiments. It was light in weight. A bend

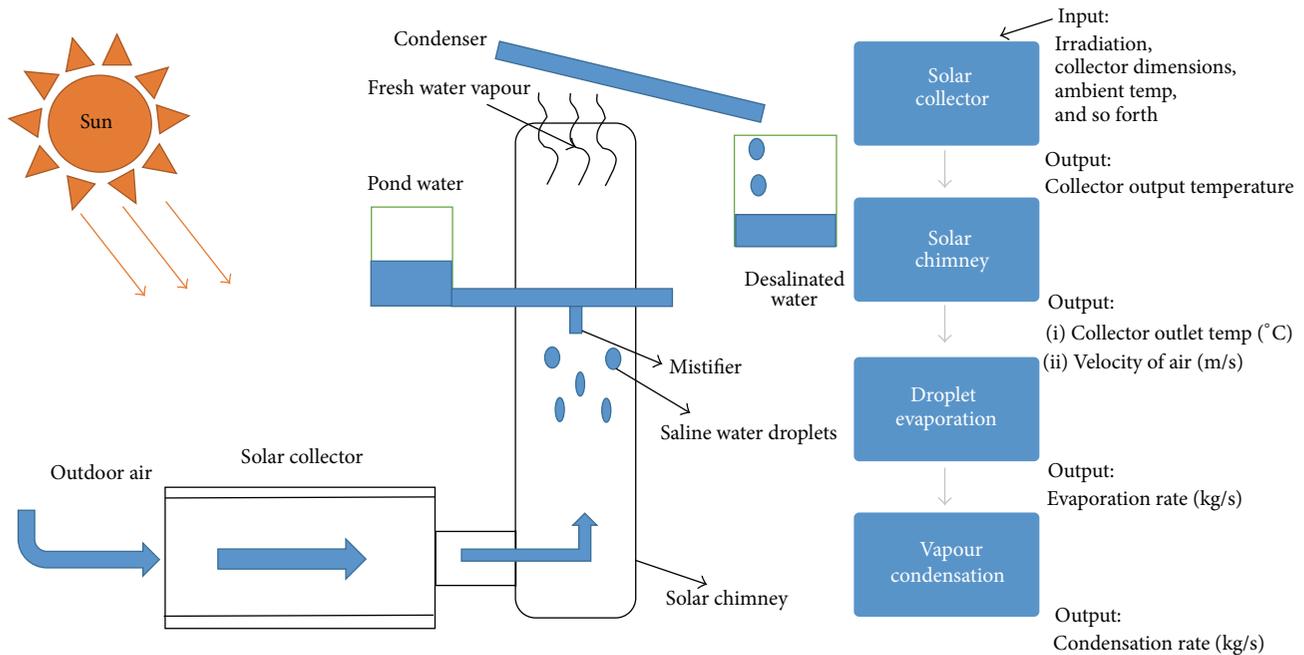


FIGURE 4: Schematic diagram and flow chart of solar desalination system.

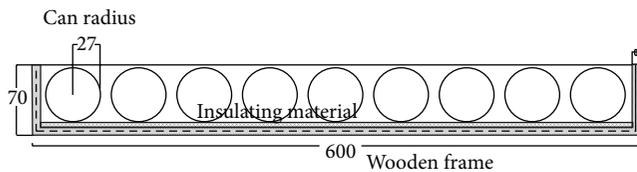


FIGURE 5: Solar collector with 9 columns of recycled aluminium cans (front view).

was provided at the end of the chimney at an angle of 45° to facilitate assembly with collector. Top end of chimney was connected to the condenser.

3.3. Condenser. The condenser (Figure 8(a)) was designed with dimensions of $400 \times 450 \times 0.5$ mm and a 30° slope. A slope was provided to condenser surface for collecting water. Condenser had the provision to store ice at top.

3.4. Sprinkler System. A sprinkler (Figure 8(b)) was used for spraying water into the chimney. However, mistifier can also be used for the operation. Sprinkler would spray water. This could be evaporated by hot air which comes from chimney. The sprinkler could be placed at 1 m from the base of the

chimney. The salt water was pumped to the sprinkler using a small submersible water pump, used in water coolers and fountains.

3.5. Construction of Desalination Plant Using Solar Chimney with RAC Collector. As seen in Figure 9, the collector and chimney were attached together using 4x M8 bolts. The condenser was attached at the top of the chimney. Finally, the entire system was mounted on a stand.

3.6. Experimental Conditions. The experiment was conducted for 8 hr. The values were taken at the following conditions.

Local time: 11:00 AM to 1:00 PM, on April 10, 2014.

Location: Tadepalligudem, Andhra Pradesh, India.

Latitude: $16^\circ 50' 10.18''$.

Longitude: $81^\circ 31' 1.81''$.

Readings for the solar panel connected are as follows: $V = 30$ volts; $i = 0.028$ amp.

The following are solar parameters prevailing in the place of work. Sukhapme and Nayak [15] have given a detailed procedure for calculating solar irradiance of a system at a location:

$$\text{Latitude } (\phi) = 16.50 \text{ deg}$$

$$\text{Day Number } (n) = 100$$

$$\text{Array Tilt (Slope) } (\beta) = 80 \text{ deg (but, optimal for that month is at 81 degrees)}$$

(1)

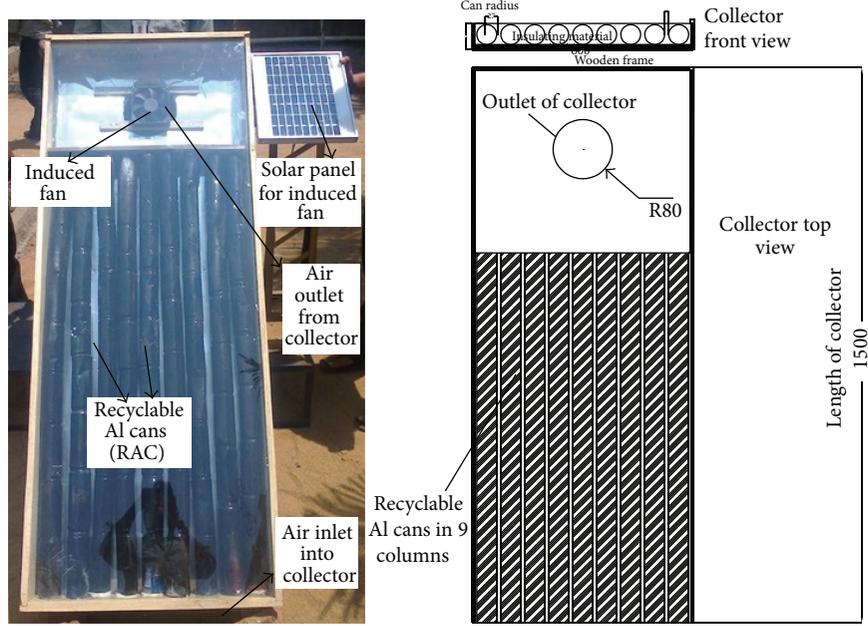


FIGURE 6: Solar collector made of recycled aluminium cans (RAC collector).

$$\text{Declination angle } (\delta \text{ (in deg)}) = 23.45 \sin \left[\frac{360}{365} (284 + n) \right] = 23.08 \text{ deg}$$

$$\text{Hour angle } (\omega) = \cos^{-1} (-\tan \phi \cdot \tan \delta)$$

$$\text{Monthly avg. radiation } (I_o) = I_{sc} \left(1 + 0.033 \cos \left(\frac{360n}{365} \right) \right) \text{ kw/m}^2$$

Solar irradiance on a tilted surface with no atmospheric effects (H_{ot})

$$= \frac{24I}{\pi} (\cos(\phi - \beta) \cos \delta \cdot \cos \omega + \omega \sin(\phi - \beta) \sin \delta) \text{ kwh/m}^2/\text{day}$$

$$\text{Solar energy with no atmosphere } (H_o) = \frac{24I}{\pi} (\cos \phi \cos \delta \cos \omega + \omega \sin \phi \sin \delta) \text{ kwh/m}^2/\text{day}.$$

(2)

The above input values were submitted in (2) and irradiance was calculated as 6.39 kWh/m². However, a minimal value of 1.0 kWh/m² was considered in the calculations.

A mathematical model was developed, sensitivity analyses were conducted to optimize the system, and the design parameters obtained were then used in the dimensioning and sizing of the components for fabrication.

3.7. Draught Calculation. As per the chimney height draught calculation equations are

$$h = 353H \left[\frac{1}{T_1} - \left(\left(\frac{w+1}{w} \right) \frac{1}{T} \right) \right],$$

$$h' = H \left[\left(\frac{w}{w+1} \right) \frac{T}{T_1} - 1 \right].$$

From the input values, $H = 1.5$ m; $w = 200$ kg of air/hr; and $T = 80^\circ\text{C}$ and $T_1 = 28^\circ\text{C}$. Draught (h) and draught height (h') are 1.17×10^{-3} mm of water and 3.4 m, respectively.

3.8. Performance of RAC Solar Collector. The performance of solar air collector was calculated using the data shown in Table 2. Alvarez et al. [13] calculated RAC air solar collector thermal efficiency as the ratio of the total useful specific enthalpy flux and the total incident solar radiation flux:

$$\eta = \frac{\int_{t_1}^{t_2} \dot{m} C_p (T_o - T_i) dt}{A_c \int_{t_1}^{t_2} G \cdot dt}.$$

(4)

3.9. Performance of Chimney. As the chimney diameter was kept constant, the velocity of the heated air flow which flows through the heat collector increases and the air volume flow rate also increases in similar proportion as the chimney height increases. The pressure difference which was caused by the air density difference between inside and outside of chimney was

$$\Delta P = \rho_{ch.in} g H \frac{T_{ch.in} - T_a}{T_a}.$$

(5)

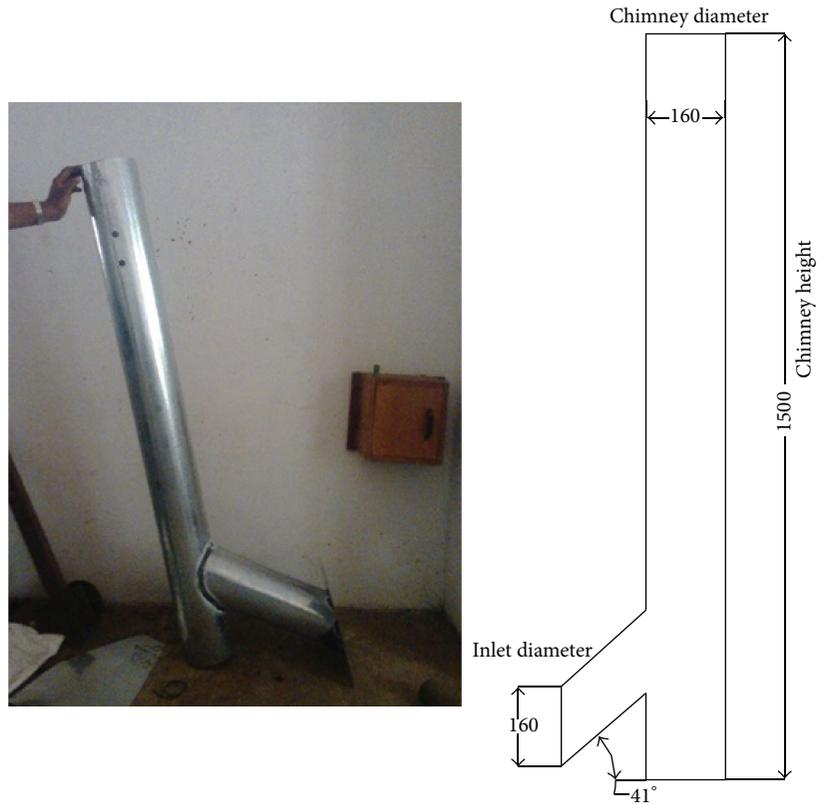


FIGURE 7: Chimney made of GI sheet and its dimensions.

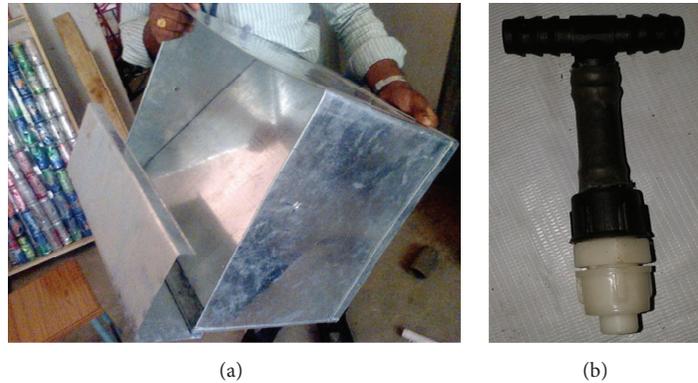


FIGURE 8: (a) Condenser. (b) Sprinkler.

The pressure difference was proportional to some of the factors, such as the density of the air flow at the inlet of the chimney, the temperature difference ($T_{\text{ch.in}} - T_a$), and chimney height. This pressure drop would help condensation.

4. Results and Discussion

Before any water was sprayed into the system, the air in the system was heated through the solar collector with minimum solar irradiation of 1000 W/m^2 applied. The temperature distributions along the collector and chimney were recorded

in Tables 3 and 4 by using laboratory thermometer and represented graphically in Figure 10.

From Figures 10(a) and 10(b), it can be seen that, with an increase in the solar radiation, the collector outlet temperature was increasing. The outlet temperature of air in the chimney is increasing continuously and this temperature could make the mist evaporate and move up. In order to determine the amount of water evaporated, the initial and final weight of the water tank were measured with the difference in weight being the amount of water evaporated by the system. The condenser walls were kept at a constant temperature of 10°C by using crushed ice. Initial tests were

TABLE 2: Dimensions and specifications of RAC solar collector.

| Data assumed | Value(s) |
|--|--------------------------|
| Length of collector | 1.5 m |
| Width of collector | 0.6 m |
| Length of absorber plate (L_1) | 1.5 m |
| Width of absorber plate (L_2) | 0.6 m |
| Spacing between absorber plate and bottom plate (L) | 1.5 cm |
| Air flow rate (\dot{m}) | 200 kg/hr |
| Air inlet temperature (T_{in}) | 30°C |
| Ambient temperature (T_a) | 28°C |
| Solar flux incident on the collector face (I_T) | 950 W/m ² -°C |
| Transmissivity ($\tau_{\alpha,avg}$) | 0.85 |
| Top loss coefficient (U_t) | 6.2 W/m ² -°C |
| Bottom loss coefficient (U_b) | 0.8 W/m ² -°C |
| Emissivity top plate and bottom plate surfaces $\epsilon_p = \epsilon_b$ | 0.95 |

TABLE 3: RAC collector temperature distribution.

| Time | Inlet temperature of collector (°C) | Outlet temperature of collector (°C) |
|----------|-------------------------------------|--------------------------------------|
| 11:30 AM | 30 | 43 |
| 11:45 AM | 31 | 49 |
| 12:00 PM | 32 | 53 |
| 12:15 PM | 32 | 59 |
| 12:30 PM | 34 | 64 |
| 1:00 PM | 35 | 74 |

TABLE 4: Chimney temperature distribution.

| Time | Inlet temperature of chimney (°C) | Outlet temperature of chimney (°C) |
|----------|-----------------------------------|------------------------------------|
| 11:30 AM | 42 | 41 |
| 11:45 AM | 47 | 45 |
| 12:00 PM | 52 | 51 |
| 12:15 PM | 59 | 58 |
| 12:30 PM | 63 | 61 |
| 1:00 PM | 73 | 72 |

TABLE 5: Temperature distribution of air in chimney at different heights (before water is sprinkled in chimney).

| Height (m) | Initial temperature when no mist is sprayed (°C) | | |
|------------|--|---------------------|---------|
| | Trial 1 at 11:00 AM | Trial 2 at 01:00 PM | Average |
| 2.2 | 60 | 68 | 64 |
| 2.5 | 59 | 66 | 62.5 |
| 2.8 | 54 | 63 | 58.5 |
| 3.1 | 52 | 57 | 54.5 |
| 3.4 | 49 | 56 | 52.5 |

TABLE 6: Temperature distribution of air in chimney at different heights (after water is sprinkled in chimney).

| Height (m) | Final temperature when water is sprayed (°C) | | |
|------------|--|---------------------|---------|
| | Trial 1 at 11:00 AM | Trial 2 at 01:00 PM | Average |
| 2.2 | 33 | 33 | 33 |
| 2.5 | 32 | 33 | 32.5 |
| 2.8 | 31 | 32 | 31.5 |
| 3.1 | 29 | 32 | 30.5 |
| 3.4 | 29 | 31 | 30 |

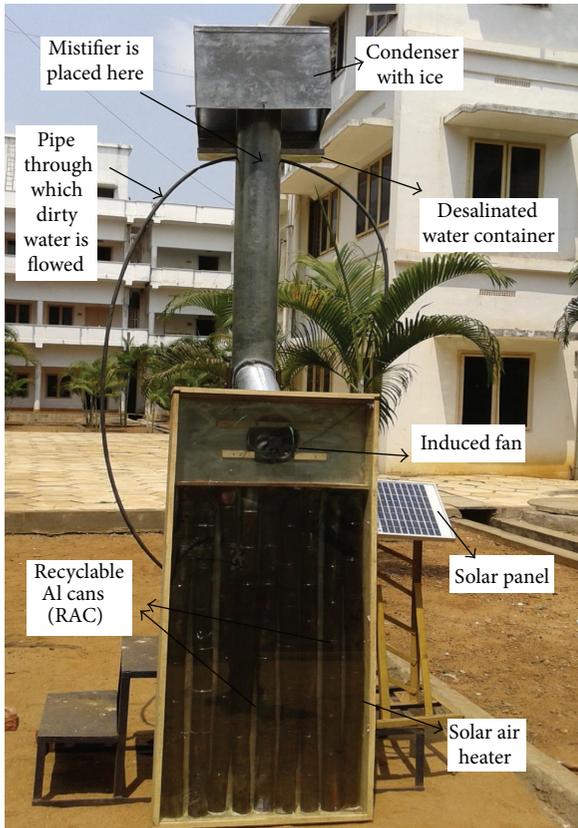


FIGURE 9: Desalination plant using a solar chimney with RAC collector.

conducted for the sprinkler system installed near the chimney outlet (0.5 m height from base of chimney) and each test ran for 1 hr. Later tests are done at second position 1 m from the base of chimney.

In addition, temperature measurements along the chimney were also taken to determine the temperature drop in

the system as water was injected into the system. Tables 5 and 6 show the air temperature distributions in chimney (before and after water was sprayed in chimney) and were represented graphically in Figure 11. Because of heat and mass transfer in the mist of water and air, the change of phase from liquid to vapour takes place. The drop in temperature with height of the chimney is due to heat losses across the chimney wall. It clearly demonstrates the need for a good insulation to be done to the chimney to minimize convection and radiation.

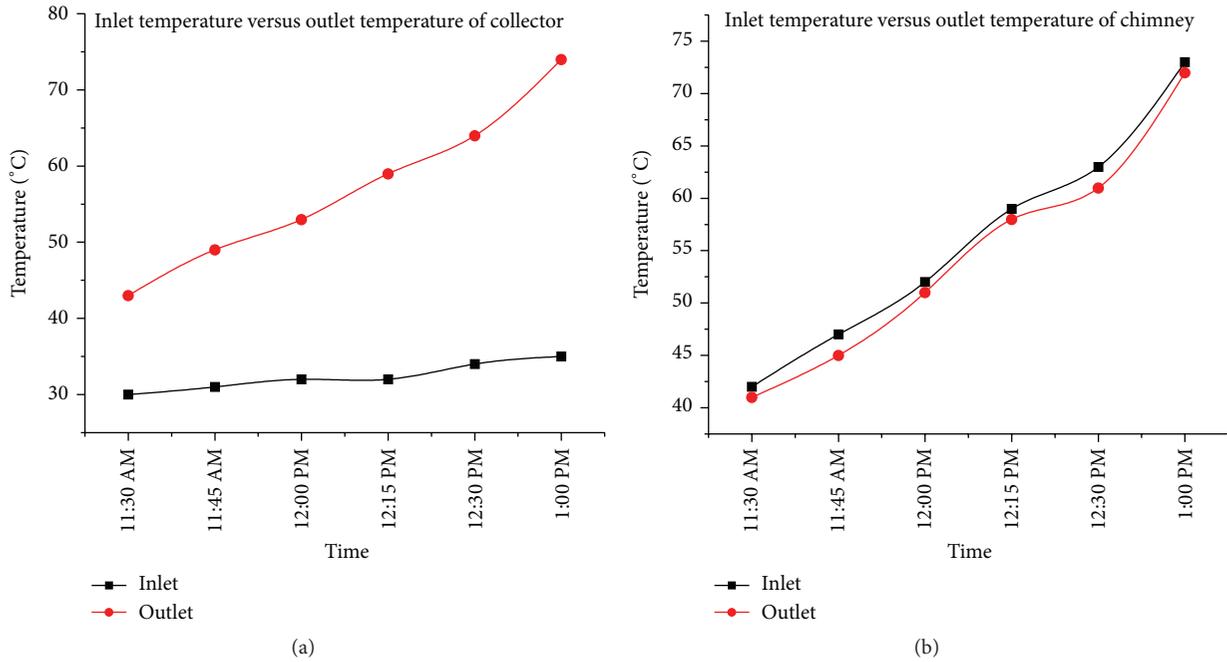


FIGURE 10: (a) Inlet and outlet temperature of collector. (b) Inlet and outlet temperatures of chimney.

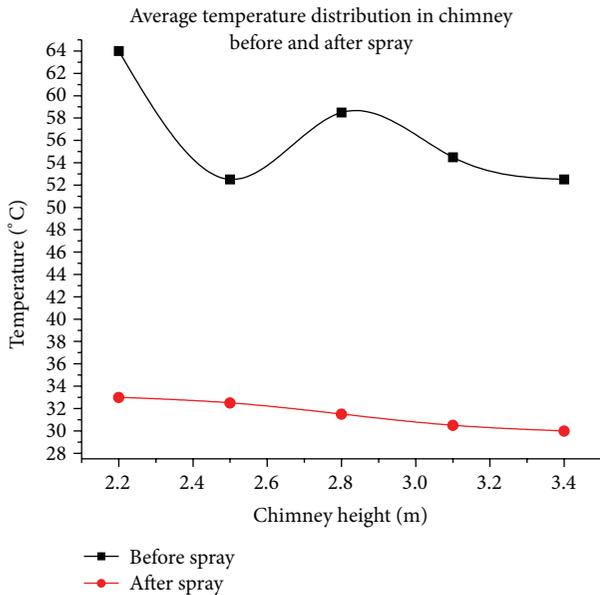


FIGURE 11: Average temperature distribution in chimney before and after spray at different height.

The air flow rate values, in chimney, measured using anemometer were tabulated in Table 7 and were represented explicitly in Figure 12. It can be seen that air flow rate without mist reaches peak at 12.00 noon, which corresponds to highest irradiance time. Accordingly the air flow rate with mist falls to minimum at around the same time as humidification increases the density of air. Air flow rate with mist curve slightly trails behind one without mist.

TABLE 7: Airflow rates in chimney.

| Trial | Time | Air flow rate in chimney (velocity (m/s)) | |
|---------|----------|---|---------------------|
| | | Flow rate without mist | Flow rate with mist |
| Trial 1 | 11:00 AM | 0.12 | 0.08 |
| Trial 2 | 12:00 PM | 0.15 | 0.06 |
| Trial 3 | 01:00 PM | 0.10 | 0.07 |
| Average | | 0.12 | 0.07 |

The chimney flow rate with and without mist gives the pressure drop in the chimney. The influence of chimney diameter, height, and solar radiation on the inlet water temperature and the glass cover temperature was different, respectively. Therefore, the temperature difference between water vapour and glass inner cover ΔT increased and hourly freshwater production increased in the daytime, while, at night time, the temperature difference ΔT decreased by which the freshwater production decreased.

5. Conclusions

The daily utilization efficiency of solar energy of the integrated system depends on the heat energy which was gained from solar energy to prepare freshwater. The primary goal of the project was achieved through the feasible solar chimney for water desalination. With the specified design parameters at a minimum solar irradiation of 1000 W/m^2 , experimental testing was done on the prototype system, the middle of the chimney being the optimum sprinkler height capable of condensing and collecting 2.3 L of water by evaporating 3.77 L with the 3.4 m height of entire setup. The success of the system

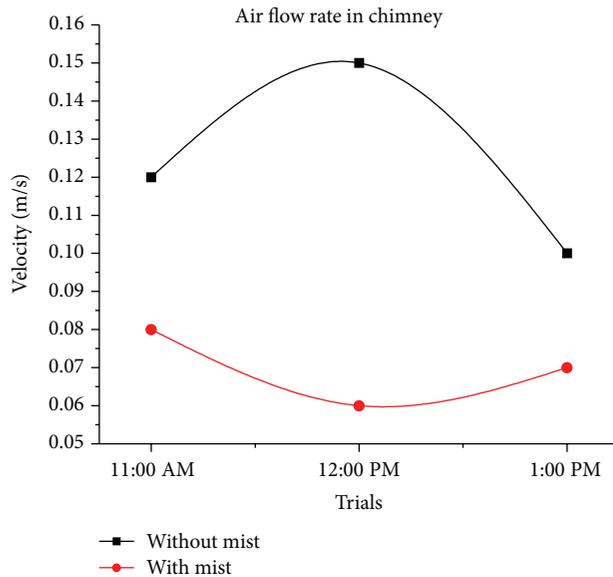


FIGURE 12: Air flow rate in chimney with and without mist.

is attributed to the unique design of RAC collector integrated with solar chimney.

Nomenclature

| | |
|-------------------------|---|
| h : | Draught (mm of water) |
| w : | Weight of air (kg/kg of fuel) |
| T : | Average absolute temperatures of chimney gasses ($^{\circ}\text{C}$) |
| T_1 : | Absolute temperature of air outside the chimney ($^{\circ}\text{C}$) |
| H : | Height of chimney above the grate level (m) |
| h' : | Draught height of hot gasses (m) |
| A_c : | Collector area (m^2) |
| G : | Incident solar radiation (W/m^2) |
| η : | Thermal efficiency of the collector (dimensionless) |
| C_p : | Specific heat ($\text{J}/\text{kg K}$) |
| t : | Time (s) |
| T_o : | Mean outlet temperature of the collector ($^{\circ}\text{C}$) |
| T_i : | Mean inlet temperature of the collector ($^{\circ}\text{C}$) |
| \dot{m} : | Mass flow rate (kg/s) |
| ΔP : | Pressure difference in chimney |
| $\rho_{\text{ch.in}}$: | Specific density of gasses in chimney |
| g : | Gravity of earth |
| $T_{\text{ch.in}}$: | Inlet temperature of chimney ($^{\circ}\text{C}$) |
| T_a : | Ambient temperature around chimney ($^{\circ}\text{C}$) |
| ΔT : | Temperature difference between pond water and glass inner cover ($^{\circ}\text{C}$). |

Disclosure

The authors further certify that proper citations to the previously reported work have been given and no data/tables/figures have been quoted verbatim from other publications without

giving due acknowledgment and without the permission of the authors.

Competing Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

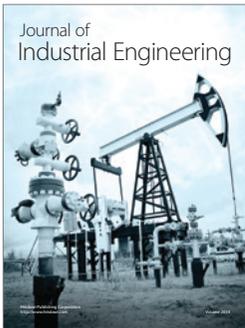
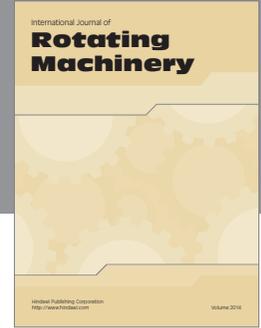
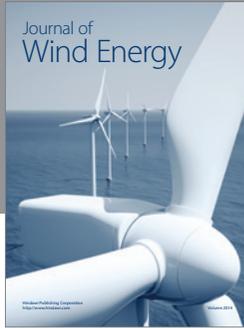
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