

Review Article

Analysis of Necessity and Feasibility for Ground Improvement in Warm and Ice-Rich Permafrost Regions

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Characterized by low bearing capacity and high compressibility, warm and ice-rich frozen soil is a kind of problematic soil, which makes the original frozen ground formed by of that unreliable to meet the stability requirements of engineering infrastructures and foundations in permafrost regions. With the design and construction of major projects along the Qinghai-Tibet Engineering Corridor (QTEC), such as expressway and airport runway, it is a great challenge to favor the stability of overlying structures by formulating the proper engineering design principles and developing the valid engineering supporting techniques. The investigations carried out in recent years indicated that warm and ice-rich permafrost foundations were widespread, climate warming was significant, and the stability of existing engineering structures was poor, along the QTEC. When the warm and ice-rich frozen ground is used as the foundation soil, the implementation of ground improvement is an alternative measure to enhance the bearing capacity of foundation soil and eliminate the settlement of structures during operation, in order to guarantee the long-term stability of the structures. Based on the key factors determining the physicochemical properties of frozen soil, an innovative idea of stabilizing the warm and ice-rich frozen soil based on chemical stabilization is proposed in this study, and then, an in situ ground improvement technique is introduced. This study intends to explore the feasibility of ground improvement in warm and ice-rich permafrost regions along the QTEC based on in situ chemical stabilization and provide the technical support and scientific reference to prevent and mitigate the hazards in the construction of major projects in the future.

1. Introduction

The Qinghai-Tibet Engineering Corridor (QTEC) runs from Golmud to Lhasa, traversing 550 km of permafrost regions in the interior of the Qinghai-Tibet Plateau (QTP) in north-south direction [1]. Permafrost refers to soil or rock that remains at or below 0°C for at least 2 years [2–4]. Permafrost on the QTP is thin, thermally unstable, and sensitive to climate change [5–7], and the warm and ice-rich frozen soil is widely distributed [8, 9]. The physicochemical properties of the warm and ice-rich frozen soil feature high

unfrozen water content [10], low shear strength [11, 12], and high compressibility [13, 14], leading to the fact that the foundation soil with the warm and ice-rich frozen soil is low in bearing capacity and large in settlement. Now, the existing linear projects, such as the Qinghai-Tibet Highway (QTH), the Qinghai-Tibet Railway (QTR), the Golmud-Lhasa oil product pipeline, and the optical cable from Lanzhou to Lhasa, are all located in the QTEC within a width of less than 10 km [9, 15]. During the operation of the QTH and the QTR, remarkable settlement of the embankments occurred in warm and ice-rich permafrost regions [16, 17], posing an

adverse effect on the traffic safety. With the design and construction of major projects along the QTEC, it is urgent to formulate the proper engineering design principles and develop the valid engineering supporting techniques.

In civil engineering, the original foundations with the poor performance in stability, deformation, or permeability generally need to be reinforced to form the artificial foundations [18]. Based on the stabilization mechanism of ground improvement, the mitigation techniques can be divided into as follows: remove and replace, compaction or densification, drainage or consolidation, and reinforcement and modification [19, 20]. Owing to the existence of ground ice, the geotechnical properties of permafrost are affected by the variation of ground temperature when it serves as the foundation materials for construction [21]. At present, the primary technique for ground improvement in warm and ice-rich permafrost regions along the QTEC is the cast-in-place piles. With the advancement of engineering machinery, materials, and construction technology, the method of ground improvement tends to be diverse, mechanical, and intelligent [19], which creates many possibilities of technology for ground improvement in permafrost regions. For the demand of economic development and national safety, the proposed major projects, such as expressway [15] and airport runways [22], will be built along the QTEC. More importantly, the workability of foundation soil under static and dynamic loading must satisfy the strict requirements of stability and deformation for high-grade roadways. So, how to guarantee the favorable serviceability of major projects in warm and ice-rich permafrost regions along the QTEC is of vital importance. Therefore, in the context of eco-environmental protection, there is practical significance to develop a suitable technique for ground improvement to enhance the serviceability and durability of major projects in the future.

By reviewing the current situation of frozen ground conditions for engineering geology, climate changes, and existing engineering structural stability along the QTEC, this study explains the necessity of ground improvement in warm and ice-rich permafrost regions affected by climate warming and anthropogenic activities. Then, an innovative idea of stabilizing the warm and ice-rich frozen soil based on chemical stabilization is proposed, according to the excellent performance of soil stabilizer for improving the geotechnical properties of soil. Moreover, an effective soil stabilizer and an in situ technique for ground improvement are introduced. Eventually, in situ tests extending the perspective of composite foundation applied in warm and ice-rich permafrost regions for ground improvement are introduced. As a result, this study provides scientific and reasonable insight into the design and construction of major projects along the QTEC in the future.

2. Analysis of Necessity

2.1. Frozen Ground Conditions for Engineering Geology along the QTEC. A better understanding of the frozen ground conditions for engineering geology along the QTEC provides the scientific guideline for construction site selection,

engineering design principle, construction technology, operation maintenance, and freezing-thawing hazard prevention to major projects in permafrost regions [9]. When permafrost serves as a geological body supporting the overlying engineering structures, its mean annual ground temperature (MAGT) and ice content determine the bearing capacity of the foundations.

Combined with the method of fuzzy C-means algorithm and analytic hierarchy process, Chai et al. [23] evaluated the frozen ground conditions for engineering geology along the QTEC based on the visualization of geo-information system. The results indicated that the engineering geology conditions in warm and ice-rich permafrost regions were poor. Similarly, taking the distribution of permafrost, ground temperature, and ice content into consideration, Jin et al. [24] analyzed the frozen ground conditions for engineering geology along the QTH and the QTR and then described the general characteristics of engineering geology based on the three-level regionalization. Both the MAGT and the ice content are principal parameters determining the engineering geology characteristics of frozen ground [25], affecting the selection of foundations of engineering infrastructures and the design principles in permafrost regions [26]. The MAGT is an indicator of thermal regime of permafrost, and it is sensitive to climate changes and engineering activities, representing the stability of permafrost conditions [24]. Based on the MAGT, the thermal regime of permafrost along the QTEC was divided into four types: extreme unstable ($-0.5^{\circ}\text{C} < \text{MAGT} \leq 0^{\circ}\text{C}$), unstable ($-1.0^{\circ}\text{C} < \text{MAGT} \leq -0.5^{\circ}\text{C}$), basically stable ($-2.0^{\circ}\text{C} < \text{MAGT} \leq -1.0^{\circ}\text{C}$), and stable ($\text{MAGT} \leq -2.0^{\circ}\text{C}$) [8]. This study analyzes the thermal regime of the frozen ground conditions for engineering geology along the QTEC based on the MAGT simulated by GIPL 2.0 permafrost model (Figure 1) [27]. The investigations indicated that the MAGT is above -1.0°C and the thermal stability of permafrost is poor in the following regions: Qingshuihe basin, Beiluhe northern basin, Kaixinlin partial hills, Buquhe basin, Wenquan basin, etc.

Meanwhile, ice content, as a determining parameter for the evaluation of frozen ground conditions for engineering geology, controls the thawing settlement properties of frozen soil [28]. Hence, the classification of frozen ground conditions for engineering geology based on the ice content in the frozen soil layer provides the guideline for engineering design and freezing-thawing hazard prevention [24]. Based on the volumetric ice content, permafrost can be divided into five categories: ice-poor ($i_v \leq 10\%$), icy ($10\% < i_v \leq 20\%$), ice-rich ($20\% < i_v \leq 30\%$), ice-saturated ($30\% < i_v \leq 50\%$), and ice layer with soil ($i_v > 50\%$) [29]. This study illustrates the distribution of permafrost types along the QTEC (Figure 2) [30]. The data of ice content in the study are from geological investigations for the construction of ± 400 kV direct current power transmission line. From Figure 2, the distribution of ice-rich frozen soil is mainly located in the following regions: Kunlunshan mountains, Qingshuihe basin, Kekexili hills and mountains, Beiluhe basin, Fenghuoshan mountains, Kaixinlin mountains, and Tanggula mountains.

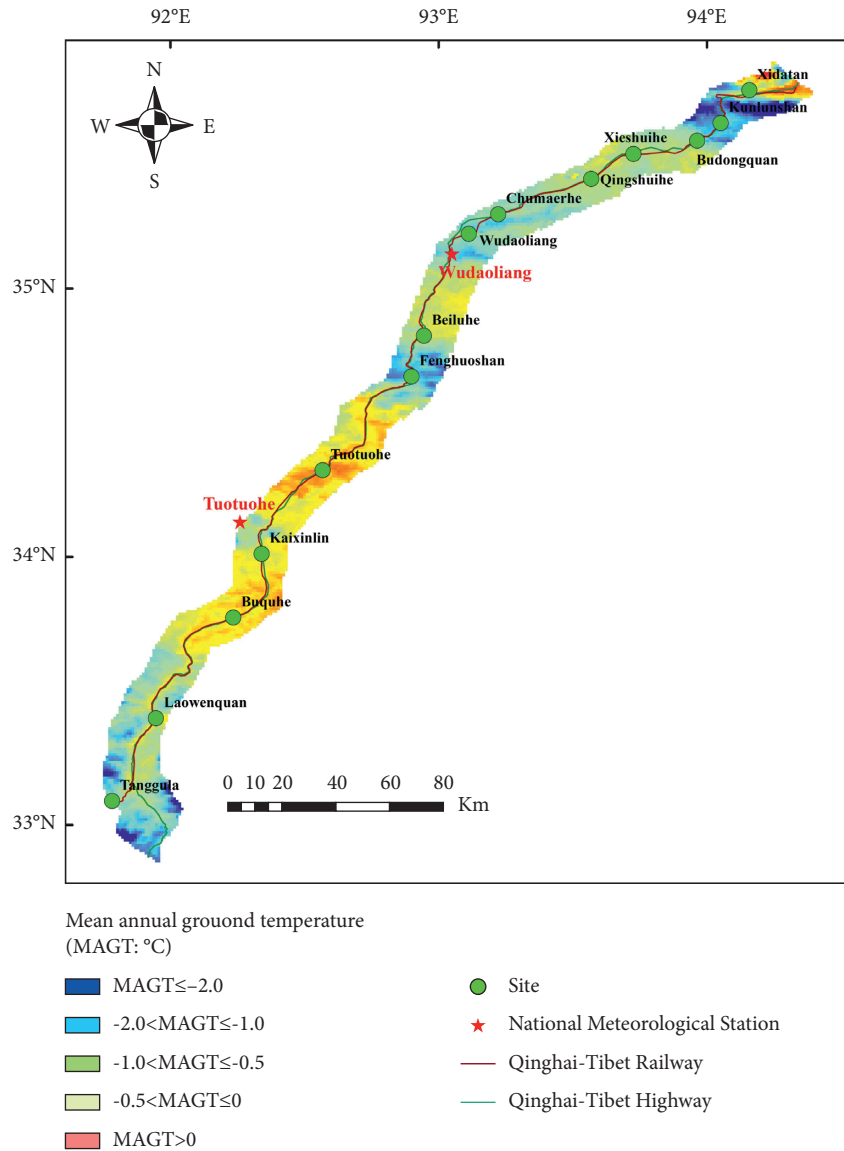


FIGURE 1: Mean annual ground temperature of permafrost along the QTEC. Note: the ground temperature distribution map was modified based on the data provided by Yin and Niu, and the original data can be used in public for scientific research and downloaded by registration (DOI: <https://doi.org/10.11888/Geocry.tpd.270044>).

The evaluation of frozen ground conditions for engineering geology shows that the higher the MAGT, the lower the thermal stability, and the higher the ice content, the higher the thawing settlement risk. Combined with Figures 1 and 2, it can be concluded that the distribution of warm and ice-rich permafrost foundations is widespread and the performance of frozen ground conditions for engineering geology is poor along the QTEC, leading to the higher requirement of countermeasures for the stability of engineering infrastructures and foundations.

2.2. Climate Changing Trends along the QTEC. Permafrost is an interactive product between the ground and the atmosphere [31, 32], and it is sensitive to climate changes [33]. The Fifth Assessment Report of the Intergovernmental Panel on Climate Change presumes that the higher

probability of global warming reaches 1.5°C between 2030 and 2052 if the current rate of warming continues [34]. Permafrost on the QTP is a sensitive indicator to global climate change, and its warming is prior to the surrounding regions; it is also a reactive amplifier of global climate change, and its temperature increases faster than the global average [35, 36]. Climate change is one of the significant parameters in permafrost engineering, and it determines the long-term performance of engineering structures. Therefore, when selecting the design principles, taking the effect of climate change on permafrost engineering into consideration is of vital importance [37]. The following contents will analyze the changing trends in climate along the QTEC based on the mean annual air temperature (MAAT) (Figure 3) and the mean annual surface temperature (MAST) (Figure 4) obtained from two national meteorological stations (Wudaoliang and Tuotuohe). From Figure 3, the

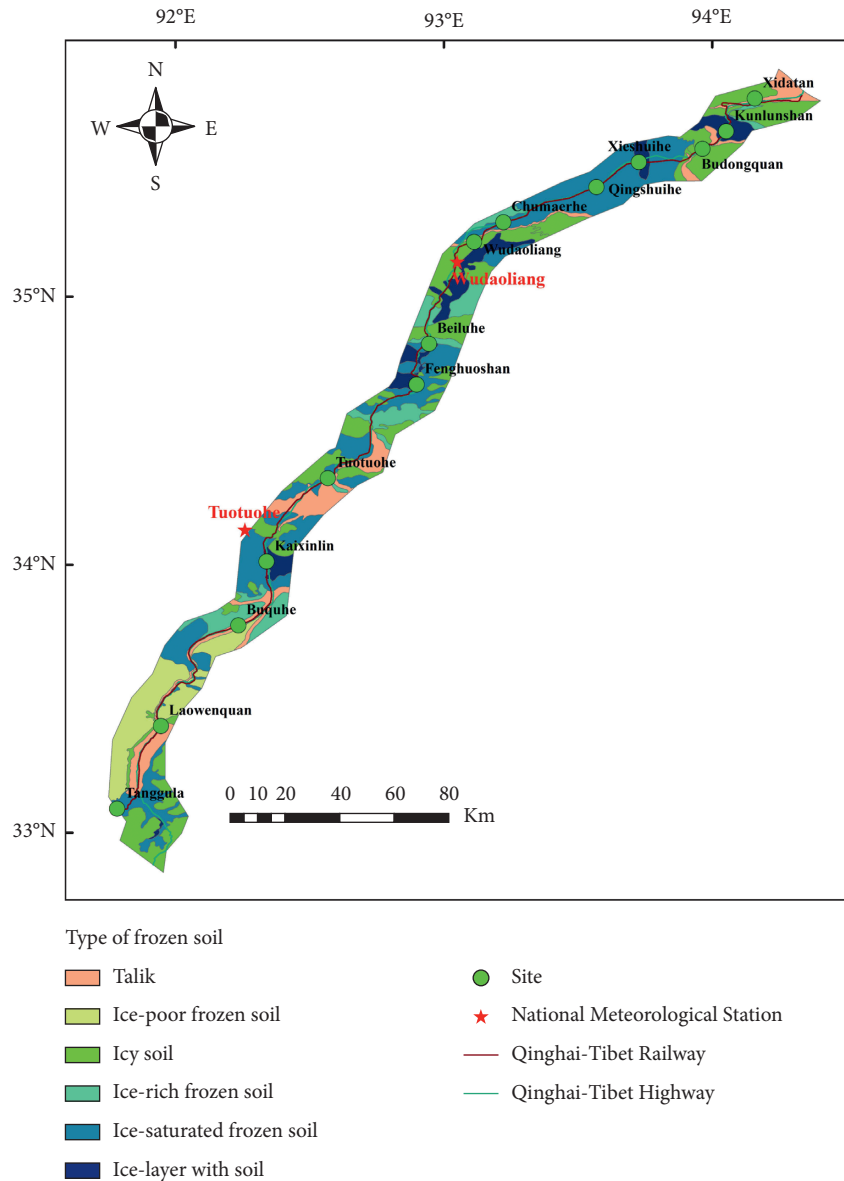


FIGURE 2: Types of frozen soil along the QTEC (source: reproduced with permission from Chai 2018, a coauthor of this study. Copyright 2018 Journal of Cold Regions Engineering).

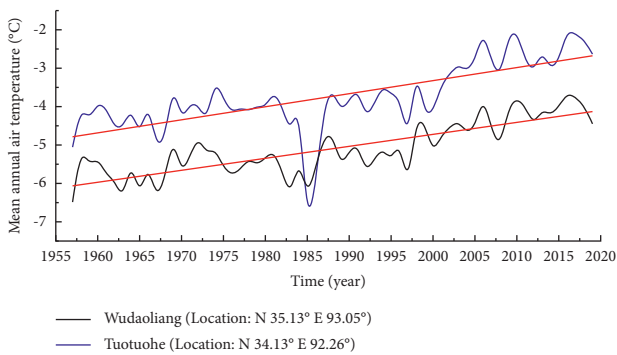


FIGURE 3: Variations of mean annual air temperature at national meteorological station within the QTEC from 1957 to 2019.

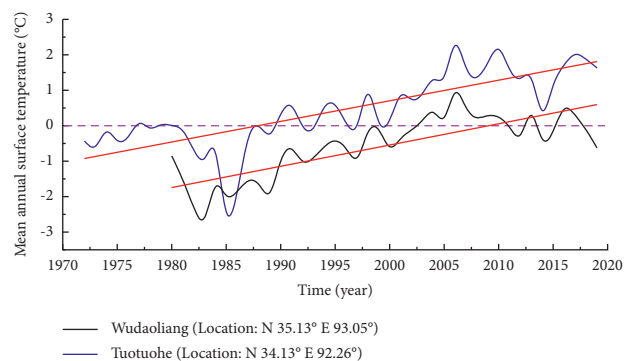


FIGURE 4: Variations of mean annual surface temperature at national meteorological station within the QTEC from 1972 to 2019.

MAAT rose by 2.04°C from -6.48°C in 1957 to -4.44°C in 2019 at Wudaoliang Station, and it rose by 2.42°C from -5.05°C in 1957 to -2.63°C in 2019 at Tuotuohe Station. Similarly, from Figure 4, the MAST rose by 0.24°C from -0.85°C in 1980 to -0.61°C in 2019 at Wudaoliang Station, and it rose by 2.07°C from -0.43°C in 1972 to 1.64°C in 2019 at Tuotuohe Station. Combined with Figures 3 and 4, it can be concluded that climate warming is obvious and the surface temperature increases significantly within the QTEC. Under climate warming scenarios, permafrost degradation along the QTEC is characterized by increasing ground temperature, thickening active layer, and melting ground ice [1, 38]. Thawing of permafrost generally results in the ground surface subsidence, which causes the failure of the overlying engineering structures and threatens their safety operations [39]. Hence, it is of great scientific significance to take the effect of climate change on permafrost engineering into consideration.

2.3. Thermomechanical Stability of Existing Linear Projects. Clarifying the interaction between permafrost and foundations of existing engineering infrastructures facilitates the adaptive analysis of countermeasures towards the application of high-grade roadways and lays a solid base for the selection of supporting techniques and for the formulation of design principles towards major projects in the future.

Engineering activities in permafrost regions inevitably disturb the energy balance on the ground surface, which affects the thermal regime of the underlying permafrost [3], leading to permafrost warming, permafrost table descending, and ground ice melting [40, 41]. In 1954, the operation of QTH was initiated with gravel pavement, and then, it was completely capped with asphalt pavement in 1985 [40]. The monitoring results indicated that permafrost degradation was significant and thawed settlement of embankments was serious along the QTH [5, 42]. Though some countermeasures, such as elevating embankment height, constructing thermal insulation berm, and placing insulation materials in the embankment, were used to reinforce the embankments based on the principle of permafrost protection or thawing rate control, some damages to the embankments occurred subsequently [43]. At present, the subgrade distress mainly results from differential settlement [16, 42], and the pavement damages are characterized by transverse cracking, potholes, and longitudinal cracking [30]. Until now, pavement damages along the QTH have not been entirely solved, and large-scale rehabilitations and remedies still need to be carried out every 2-3 years [44, 45].

The construction of the QTR adopted the advanced design idea, "cooled roadbed," and numerous cooling measures by adjusting solar radiation, and heat convection and conduction with modification of configurations were employed to cool the permafrost beneath the embankments [36]. The investigations indicated that the permafrost table beneath the crushed rock embankment in warm permafrost regions was uplifted, but the ground temperature in deep depth experienced a warming trend [46]. Meanwhile, some failures of the measures, including clogged crushed rock

layer [47] and damaged thermosyphon [48], pose a challenge to these active cooling measures. During the operation of the QTR, the embankment deformations were mainly due to thawing settlement [17], and the differential settlement was obvious in the embankment-bridge transition section [49]. For operation maintenance, the railway administrative bureau carried out supplementary ballast for track line regularity. In a word, the thermomechanical stability of the existing linear projects mentioned above along the QTEC was poor in some sections. Therefore, it can be concluded that the existing supporting techniques and the mitigation countermeasures are incapable to serve the construction of high-grade roadways because of its higher requirements for structural stabilization and its extensive disturbance to the thermal regime of the underlying permafrost [50].

Hence, faced with the poor frozen ground conditions for engineering geology and the current situation of climate warming, it is imperative to transform our insight into ground improvement as adopted in problematic soils to deal with the severe challenge in the construction of major projects in warm and ice-rich permafrost regions, and develop reliable countermeasures to guarantee the stability of foundations in permafrost engineering.

3. Analysis of Feasibility

3.1. Idea of Chemical Stabilization of Warm and Ice-Rich Frozen Soil. Soil stabilization is the collective terminology for any physical, or mechanical, or chemical, or any combination of such methods, employed to improve the geotechnical properties and performance of problematic soil to make it meet the requirements of engineering construction [51, 52]. Chemical stabilization involves the mixing of base soil with one of or a combination of soil stabilizers of powder, slurry, or liquid to improve the geotechnical properties such as permeability, shear strength, bearing capacity, and workability [52]. As a result, a series of reactions may occur in chemically stabilized soil system, including hydration, ion exchange, cementation, flocculation, and carbonation. The soil stabilizer refers to an available material that reacts physicochemically among base soil, water, and air, to improve the geotechnical properties of base soil [53]. Soil stabilizer acts on the soil to reduce the affinity of clay particles to water and thin the thickness of bound water film [54, 55], which creates a potential for reducing free water content and enhancing physicochemical properties of the warm and ice-rich frozen soil. Moreover, soil stabilizer can alter the soil microstructure to reduce the compressibility of soil skeleton [56, 57] and thus may decrease the thawing settlement of the warm and ice-rich frozen soil. The category of soil stabilizer can be divided into inorganic soil stabilizer, ionic soil stabilizer, organic soil stabilizer, and bioenzyme soil stabilizer based on their stabilizing mechanisms [58, 59]. Before commencing the warm and ice-rich frozen soil stabilization, it is beneficial to review the stabilization mechanisms of soil stabilizer and its effects on soil improvement.

Inorganic soil stabilizers are generally dry powder, mainly including cement, lime, fly ash, and industrial slag;

these soil stabilizers react with base soil to generate the cementitious products, such as calcium silicate hydrate [60, 61], calcium sulfate hydrate, and calcium aluminate hydrate [62, 63]. These cementitious products can bond soil particles to form stable soil skeleton and fill the voids in soil to enhance densification and strength [64, 65]. Chai et al. [66, 67] performed a series of laboratory tests to improve the warm and ice-rich frozen soil with Portland cement and various additives, and the results indicated that the selected optimum additives are favorable to enhance the geotechnical properties of the stabilized soil.

Ionic soil stabilizer depends on the process of ion-exchange reactions to deprive soil particles of its water affinity and thin the thickness of bound water film and thus decrease the plasticity index of soil [68, 69]. Meanwhile, subjected to ionic soil stabilizer, the volume and diameter of pore in the stabilized soil decrease, reducing the compressibility of soil [70, 71]. Zhang et al. [72, 73] adopted the Toogood and Roadbond, respectively, to stabilize the warm and ice-rich frozen soil, and the results showed that the shear strength is increased and the compressibility is decreased for the stabilized soil.

Organic soil stabilizer refers to synthetic polymer solutions or emulsions, such as sulfonated oil, sodium silicate, epoxy resin, and polyacrylamide [52, 58]. Based on polymerization reactions, this kind of soil stabilizer forms organic macromolecular chains between voids to aggregate soil particles [74, 75], thus enhancing the strength and durability of the stabilized soil [76, 77]. However, there is no literature report about stabilizing frozen soil with organic soil stabilizer.

Bioenzyme soil stabilizer, as a kind of catalyst without becoming the end product, is fermented from vegetable extracts [58, 64, 78]. Bioenzymes catalyze the microorganism reactions between organic matters in soil particles and accelerate the cation-exchange process to reduce the electrical double-layer thickness [68, 79]; thus, the geotechnical properties of the stabilized soil with bioenzyme are significantly improved. However, the disadvantages of bioenzyme are characterized by biodegradation and sensitivity to the variation of temperature and pH [80]. In addition, the strength of the stabilized soil with bioenzyme is obviously decreased when the stabilized soil is soaked in water [58, 81]. Considering the successful application of various soil stabilizers in improving the geotechnical properties of problematic soil, there is theoretical and practical feasibility of the stabilization of the warm and ice-rich frozen soil. The key factors determining the physico-mechanical properties of frozen soil include soil, water, temperature, salinity, and load [3]. Therefore, the viable alternative to improve the geotechnical properties of the warm and ice-rich frozen soil based on chemical stabilization is summarized in Figure 5.

3.2. Selection of Valid Stabilizer for Stabilizing Warm and Ice-Rich Frozen Soil. After reviewing the stabilizing mechanisms mentioned above, it is concluded that soil stabilizers, other than bioenzyme, can be theoretically used to improve the warm and ice-rich frozen soil. Since the ionic and organic

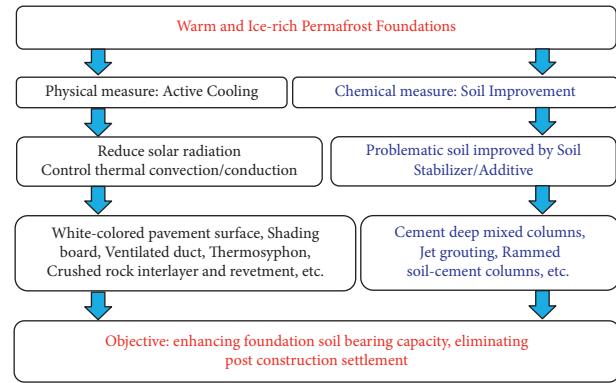


FIGURE 5: Category of frozen soil improvement.

stabilizers are liquid chemicals, they may increase the total water content in frozen soil, thus possibly causing the increase in unfrozen water and poor performance in engineering properties. Therefore, based on the unacceptable supplementary of total water content in soil stabilization, the optimum inorganic soil stabilizer of dry powder, which can react with the warm and ice-rich frozen soil at negative temperature, is emphatically selected.

According to the available materials studied, the sulphoaluminate cement, mainly composed of anhydrous calcium sulphoaluminate, dicalcium silicate, and gypsum [82], is characterized by fast hardening [83, 84] and hydration at negative temperature [85, 86]. Subsequently, our team colleagues conducted a series of laboratory tests to stabilize the warm and ice-rich frozen soil with sulphoaluminate cement. The comprehensive experimental aspects on chemical stabilization of the warm and ice-rich frozen soil are covered, and the results are as follows.

Sun et al. [87] conducted the laboratory tests, including mercury intrusion porosimetry, scanning electron microscopy, unconfined compressive strength, time-domain reflectometry, X-ray diffraction, and thawing compression tests, and found that the cementitious hydration products occur within the stabilized soil and fill the pore volume. Then, they established the correlation between microstructural characteristics and mechanical properties of the stabilized soil. One important point of the above tests mentioned is to determine the relationship between compressibility and pore orientation fractal dimension. Additionally, Yin et al. [88] performed centrifuge and freeze-dryer tests to explore the law of water transformation among free water, mineral water, and bound water during the process of soil stabilization and explained its effect on the strength of the stabilized soil. Through laboratory studies, the performance of sulphoaluminate cement-stabilized soil indicated that there is a decrease in free water, pore volume, and compressibility and an increase in unconfined compressive strength [87–90]. More importantly, it was found that the clubbed shape of ettringite occurs and establishes a skeleton structure in the pore volume of the stabilized soil, while the hydration products, such as aluminum hydroxide gel and calcium silicate hydrate gel, agglomerate and cement

the soil particles, resulting in a remarkable decrease in soil particles between 0.002 mm and 0.075 mm [90].

In conclusion, sulphoaluminate cement can be used to improve the physicochemical properties of the warm and ice-rich frozen soil and enhance its geotechnical properties; thus, it is a valid stabilizer for chemical stabilization. More importantly, compared with the currently used measure of active cooling, the physicochemical properties of the stabilized soil are no longer affected by temperature variations, so the long-term stability and durability of geotechnical properties of the stabilized soil can be guaranteed in the context of climate warming.

3.3. Technology for Ground Improvement in Warm and Ice-Rich Permafrost Regions. Similar to soft soil, the physicochemical properties of the warm and ice-rich frozen soil are characterized by high compressibility [91, 92], and its compression process is a combination of consolidation and creep [93], leading to an unreliability of foundations in frozen ground to meet the stability requirements of engineering infrastructures in permafrost regions. Based on the laboratory investigations, it is concluded that the warm and ice-rich frozen soil can be stabilized by soil stabilizers. Also, ground improvement by dry deep mixing refers to a reinforcement method mixing soil stabilizer and base soil in situ, which creates the applicability of dry jet mixing pile used in warm and ice-rich permafrost regions.

A dry jet mixing pile refers to a stabilized soil column element bearing vertical load; they can be installed with the assistance of special rotatory tool, such as a machine with several shafts equipped with mixing blades and several nozzles for pumping dry powder stabilizer using compressed air, during which a series of physicochemical reactions occur within the mixture of in situ base soil and the pumped soil stabilizer [94, 95]. Figure 6 illustrates the installation steps: positioning, drilling, elevating, and pile forming [19, 94].

The dry jet mixing pile is a kind of adhesive column with higher strength and stiffness compared with interpile soil and consists of a composite foundation with interpile soil to undertake the overlying structural load [96]. The shear strength of interpile soil is increased after installation, thus enhancing composite foundation soil bearing capacity [97, 98] and eliminating postconstruction settlement [99, 100]. More importantly, compared with currently used cast-in-place bored piles, the installation of dry jet mixing piles fully exploits the base soil properties in situ and makes no transfer of the base soil elsewhere, thus reducing the transportation cost and construction investment. Also, the advantages of dry jet mixing pile, as an environment-friendly geotechnology, are flexible installation, low noise, and small vibration [95, 97]. Through the above discussions and reviews, it is clear that the proposed ground improvement method by dry deep mixing is feasible to adjust the stress conditions of original foundation soils in warm and ice-rich permafrost regions. Therefore, adopting the composite foundation of dry jet mixing pile for supporting the stability of major projects within the QTEC is tentative and practical.

3.4. In Situ Test of Ground Improvement in Warm and Ice-Rich Permafrost Regions. To practice the idea of chemical stabilization of the warm and ice-rich frozen soil in permafrost regions, our team colleagues conducted some in situ tests at Beiluhe on the QTP, in August 2017 (Figure 7). In the experiment, the dry jet mixing pile was installed without strict accordance with the technical steps illustrated in Figure 6. The process was implemented by an excavator; the excavated frozen soil and dry stabilizer were subsequently mixed, backfilled, and compacted. The thermistors were located at different depths of the backfilled mixture to measure hydration heat during the curing period. The details of installation can be seen in the paper by Chai et al. [101]. Meanwhile, to verify the effectiveness of ground improvement, the pressuremeter test was performed after 70 days of curing. Since the dry jet mixing pile serves as a column element bearing vertical load, much attention is concentrated on pile-to-soil stress ratio and load transfer mechanism of pile under static loading in engineering application [102, 103], leading to the fact that the pressuremeter test conducted in situ has no value for reference. However, this in situ experiment is still a meaningful attempt to reinforce foundation soils by chemical stabilization in warm and ice-rich permafrost regions, and it can provide a reference for the selection and formulation of supporting technology towards major projects in the future.

4. Research Work for Future

The essence of frozen soil is different from thawed soil due to the presence of ice [104, 105], leading to the fact that ice is the most important constituent controlling the strength and deformation of frozen soil [104, 106]. When engineering infrastructures and foundations are over or within frozen ground, its stability is affected by thermomechanical properties of frozen soil [107]. Currently, the dominant principle of engineering designs and remedial countermeasures mainly depends on active cooling to prevent frozen soil from thawing and warming. Nonetheless, affected by climate warming and subsequent ground temperature rising, the thermomechanical stability of existing linear projects in warm and ice-rich permafrost regions along the QTEC was poor, meaning that the countermeasures for mitigating hazard are insufficient to acquire the targeted requirements. With the design and construction of major projects along the QTEC, such as expressway and airport runway, it is imperative to reevaluate the effect of climate warming and anthropogenic activities on engineering infrastructures and foundations. Moreover, both the reliable engineering designs and the effective mitigation countermeasure need to be formulated urgently.

Soil stabilization used to improve the geotechnical properties of soil is usually applied in ground improvement. This study proposes an innovative idea of chemical stabilization of the warm and ice-rich frozen soil and introduces a method of in situ ground improvement by dry jet mixing. Although our team colleagues conducted a series of laboratory tests to stabilize the warm and ice-rich frozen soil with sulphoaluminate cement and Portland cement combined

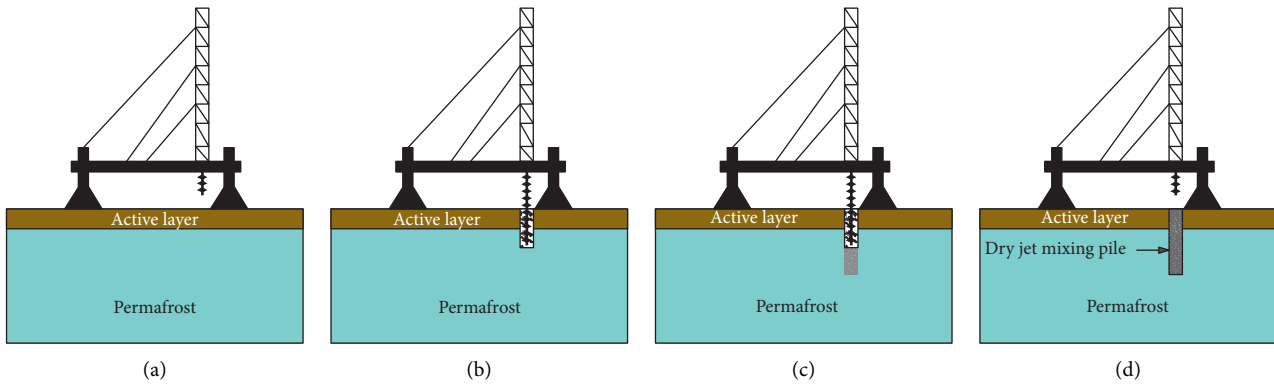


FIGURE 6: Installation of dry jet mixing pile. (a) Positioning. (b) Drilling. (c) Elevating. (d) Pile forming.



FIGURE 7: In situ test. (a) Construction site. (b) Pro-improved frozen soil. (c) Postimproved frozen soil.

with various additives, it should be noted that the degree of hydration between frozen soil and soil stabilizer is low, and the strength of the stabilized soil increased slowly at negative temperature. Hence, it is of vital significance to develop high-performance cement with high hydration degree at negative temperature and some highly effective additives used as a stimulator for improving physicochemical properties of the warm and ice-rich frozen soil. Additionally, the engineering disturbance to original foundation soils caused by the installation of dry jet mixing pile is inevitable, so how to quantify the strength variation between the decrease by installation and the increase by soil stabilization is still a key point in future research. Limited by the field conditions and cost budgets, the installation process of dry jet mixing pile is simplified, leading to producing an unsatisfactory case for the practical use towards future major projects along the QTEC. A further study is the installation of dry jet mixing pile based on practical construction similar to that applied in soft soil regions, and a series of tests, such as static loading test of pile, standard penetration, and core sample survey, should be performed in the field.

5. Summary

- (1) The distribution of warm and ice-rich permafrost foundations along the QTEC is widespread. Affected by both climate warming and anthropogenic activities, the thermal regime of permafrost distresses annually and the risk level of thawing settlement increases gradually. The thermomechanical stability of existing linear projects in warm and ice-rich permafrost regions, such as the QTR and the QTH, tends to be poor, indicating that the existing countermeasures for mitigating hazard in permafrost engineering are incapable to be applied directly to major projects in the future.
- (2) The key factors determining the physicochemical properties of frozen soil include soil, water, temperature, salinity, and load. The idea that the geo-technical properties of the warm and ice-rich frozen soil can be improved based on chemical stabilization is feasible. In addition, the method of in situ ground improvement by dry jet mixing is tentative and

practical in permafrost engineering along the QTEC. Before the application of dry jet mixing to major projects in permafrost regions, a series of in situ tests based on technical code for ground improvement still need to be performed.

- (3) With the design and construction of major projects along the QTEC, such as expressway and airport runway, principal considerations must be observed as follows: (1) focusing on implementing the zonation of frozen ground conditions for engineering geology along the QTEC; (2) emphasizing on considering the effect of climate warming on engineering infrastructures and foundations in permafrost regions; (3) paying attention to the thermal effect of engineering structures on the underlying permafrost; and (4) adopting proper engineering design principles and developing effective mitigation countermeasures.

Data Availability

The data used to support the findings of this study are available from the corresponding author upon request.

Conflicts of Interest

The authors declare that they have no conflicts of interest.

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References

- [1] H. J. Jin, Q. H. Yu, S. L. Wang, and L. Z. Lü, "Changes in permafrost environments along the Qinghai-Tibet engineering corridor induced by anthropogenic activities and climate warming," *Cold Regions Science and Technology*, vol. 53, no. 3, pp. 317–333, 2008.
- [2] S. A. Harris, H. M. French, J. A. Heginbottom et al., *Glossary of Permafrost and Related Ground-Ice Terms*, National Research Council of Canada Ottawa, Ontario, Canada KIA 0R6, 1988.
- [3] O. B. Anderland and B. Ladanyi, *Frozen Ground Engineering*, John Wiley & Sons, Hoboken, New Jersey, 2004.
- [4] W. Dobinski, "Permafrost," *Earth-Science Reviews*, vol. 108, no. s3-4, pp. 158–169, 2011.
- [5] H. J. Jin, L. Zhao, S. L. Wang, and R. Jin, "Thermal regimes and degradation modes of permafrost along the Qinghai-Tibet Highway," *Science in China - Series D: Earth Sciences*, vol. 49, no. 11, pp. 1170–1183, 2006.
- [6] B. L. Wang and H. M. French, "Permafrost on the Tibet Plateau, China," *Quaternary Science Reviews*, vol. 14, no. 3, pp. 255–274, 1995.
- [7] Q. B. Wu, T. J. Zhang, and Y. Z. Liu, "Permafrost temperatures and thickness on the Qinghai-Tibet Plateau," *Global and Planetary Change*, vol. 72, no. 1-2, pp. 32–38, 2010.
- [8] Q. B. Wu, G. D. Cheng, and W. Ma, "Impact of permafrost change on the Qinghai-Tibet Railroad engineering," *Science in China - Series D: Earth Sciences*, vol. 47, no. 1, pp. 122–130, 2004.
- [9] H. J. Jin, Z. Wei, S. L. Wang et al., "Assessment of frozen-ground conditions for engineering geology along the Qinghai-Tibet highway and railway, China," *Engineering Geology*, vol. 101, no. 3-4, pp. 96–109, 2008.
- [10] K. Xue, Z. Wen, M. L. Zhang, D. S. Li, and Q. Gao, "PF meter-based study on the relationship between soil matric potential and unfrozen water content during soil freezing and thawing," *Journal of Arid Land Resources & Environment*, vol. 31, no. 12, pp. 155–160, 2017.
- [11] M. Huo, S. J. Wang, J. Z. Zhang, and L. Jin, "Experimental study on influences of water content and temperature on mechanical properties of ice-rich frozen soil," *Journal of Hydraulic Engineering*, vol. 41, no. 10, pp. 1165–1172, 2010.
- [12] X. D. Zhao, G. Q. Zhou, G. L. Lu, Y. Wu, W. Jiao, and J. Yu, "Strength of undisturbed and reconstituted frozen soil at temperatures close to 0 °C," *Sciences in Cold and Arid Regions*, vol. 9, no. 4, pp. 0404–0411, 2017.
- [13] X. J. Ma, J. M. Zhang, X. X. Chang, B. Zheng, and M. Y. Zhang, "Experimental study on creep of warm and ice-rich frozen soil," *Chinese Journal of Geotechnical Engineering*, vol. 29, no. 6, pp. 848–851, 2007.
- [14] B. Zheng, J. M. Zhang, X. J. Ma, and J. W. Zhang, "Study on compressibility deformation of warm and ice-enriched frozen soil," *Chinese Journal of Rock Mechanics and Engineering*, vol. 28, no. 1, pp. 3063–3069, 2009.
- [15] W. Ma, F. J. Niu, and Y. H. Mu, "Basic research on the major permafrost projects in the Qinghai-Tibet plateau," *Advances in Earth Science*, vol. 27, no. 11, pp. 1185–1191, 2012.
- [16] F. Yu, J. Qi, Y. Lai et al., "Typical embankment settlement/heave patterns of the Qinghai-Tibet highway in permafrost regions: formation and evolution," *Engineering Geology*, vol. 214, pp. 147–156, 2016.
- [17] Z. Z. Sun, W. Ma, S. J. Zhang, and Z. Wen, "Embankment stability of the qinghai-tibet railway in permafrost regions," *Journal of Cold Regions Engineering*, vol. 32, no. 1, pp. 118–124, 2018.
- [18] Ministry of Construction of the People's Republic of China, *Technical Code for Ground Treatment of Buildings, JGJ 79-2012*, China Architecture and Building Press, Beijing, 2012.
- [19] X. N. Gong, *Ground Improvement Handbook*, China Architecture and Building Press, Beijing, 2008.
- [20] W. Sondermann, "Ground improvement as alternative to piling - effective design solutions for heavily loaded structures," *Sustainable Civil Infrastructures*, Springer, Cham, in *Proceedings of the 2nd GeoMEast International Congress and Exhibition on Sustainable Civil Infrastructures, Egypt 2018-The Official International Congress of the Soil-Structure Interaction Group in Egypt (SSIGE)*, pp. 1–25, October 2018.
- [21] Y. W. Zhou, D. X. Guo, G. Q. Qiu, G. D. Cheng, and S. D. Li, *Geocryology in China*, Sciences Press, Beijing, 2000.
- [22] W. B. Liu, W. B. Yu, L. Chen et al., "Techniques of airport runway construction in permafrost regions: a review," *Journal of Glaciology and Geocryology*, vol. 37, no. 6, pp. 1599–1610, 2015.
- [23] M. T. Chai, J. M. Zhang, Y. H. Mu, G. Liu, and K. Mu, "Assessment on engineering geological conditions of frozen ground along the Qinghai-Tibet engineering corridor (QTEC) based on FCM and AHP," *Journal of Engineering Geology*, vol. 23, no. S8, pp. 49–56, 2015.

- [24] H. J. Jin, S. L. Wang, Q. H. Yu, Q. B. Wu, and Z. Wen, "Regionalization and assessment of environmental geological conditions of frozen soils along the Qinghai-Tibet Engineering Corridor," *Hydrogeology & Engineering Geology*, vol. 6, pp. 66–71, 2006.
- [25] S. P. Wang, "Railway route selection principles based on the classification of engineering geological condition in permafrost regions," *Journal of Railway Engineering Society*, pp. 48–52, 2009.
- [26] O. B. Anderland and D. M. Anderson, *Geotechnical Engineering for Cold Region*, McGraw-Hill, New York, NY United States, 1978.
- [27] G. A. Yin and F. J. Niu, *The Ground Temperature Distribution Map of the Tibet Engineering Corridor (2010-2015)*, National Tibetan Plateau Data Center, Beijing, China, 2018.
- [28] Y. Q. Li and L. M. Han, "Engineering geological characteristic and evaluation of permafrost ground along Qinghai-Tibet railway," *Journal of Engineering Geology*, vol. 16, no. 2, pp. 245–249, 2008.
- [29] Q. B. Wu, X. F. Dong, and Y. Z. Liu, "Spatial distribution model of high ice content frozen soil along Qinghai-Tibetan highway-a GIS-aided model," in *Proceedings of the Sixth International Symposium on Permafrost Engineering*, 2004.
- [30] M. T. Chai, Y. H. Mu, J. M. Zhang, W. Ma, G. Liu, and J. B. Chen, "Characteristics of asphalt pavement damage in degrading permafrost regions: case study of the qinghai-tibet highway, China," *Journal of Cold Regions Engineering*, vol. 32, no. 2, pp. 1–12, 2018.
- [31] R. Vaikmäe, M. Böse, F. A. Michel, and B. J. Moormann, "Changes in permafrost conditions," *Quaternary International*, vol. 28, pp. 113–118, 1995.
- [32] M. W. Smith and D. W. Riseborough, "Climate and the limits of permafrost: a zonal analysis," *Permafrost and Periglacial Processes*, vol. 13, no. 1, pp. 1–15, 2002.
- [33] Q. B. Wu and T. J. Zhang, "Recent permafrost warming on the Qinghai-Tibetan plateau," *Journal of Geophysical Research*, vol. 113, Article ID D13108, 2008.
- [34] IPCC Summary for Policymakers, "Global warming of 1.5°C, an IPCC special report on the impacts of global warming of 1.5°C above pre-industrial levels and related global greenhouse gas emission pathways," in *the context of strengthening the global response to the threat of climate change, sustainable development, and efforts to eradicate poverty*, 2018.
- [35] B. T. Pan and J. J. Li, "Qinghai-Tibetan plateau: a driver and amplifier of the global climate change-III: the effects of uplift of Qinghai-Tibetan plateau on climate changes," *Journal of Lanzhou University*, vol. 32, no. 1, pp. 108–115, 1996.
- [36] G. D. Cheng, "Construction of qinghai-tibet railway with cooled roadbed," *China Railway Science*, vol. 24, no. 3, pp. 1–4, 2003.
- [37] Q. B. Wu and F. J. Niu, "Permafrost changes and engineering stability in Qinghai-Xizang Plateau," *Chinese Science Bulletin*, vol. 58, no. 2, pp. 115–130, 2013.
- [38] G. D. Cheng and T. H. Wu, "Responses of permafrost to climate change and their environmental significance, Qinghai-Tibet Plateau," *Journal of Geophysical Research*, vol. 112, Article ID F02S03, 2007.
- [39] F. E. Nelson, O. A. Anisimov, and N. I. Shiklomanov, "Subsidence risk from thawing permafrost," *Nature*, vol. 410, no. 6831, pp. 889–890, 2001.
- [40] Y. Sheng, J. M. Zhang, Y. Z. Liu, and J. M. Wu, "Thermal regime in the embankment of Qinghai-Tibetan Highway in permafrost regions," *Cold Regions Science and Technology*, vol. 35, no. 1, pp. 35–44, 2002.
- [41] Q. B. Wu, G. D. Cheng, W. Ma, F. Niu, and Z. Z. Sun, "Technical approaches on permafrost thermal stability for Qinghai-Tibet Railway," *Geomechanics and Geoengineering*, vol. 1, no. 2, pp. 119–127, 2006.
- [42] Q. B. Wu, Z. Q. Zhang, and Y. Z. Liu, "Long-term thermal effect of asphalt pavement on permafrost under an embankment," *Cold Regions Science and Technology*, vol. 60, no. 3, pp. 221–229, 2010.
- [43] J. B. Chen, S. J. Wang, and J. Z. Zhang, "Formation and mechanism of high subgrade diseases of Qinghai-Tibet highway," *Journal of Chang'an University (Natural Science Edition)*, vol. 28, no. 6, pp. 30–35, 2008.
- [44] S. J. Wang, M. Huo, and W. J. Zou, "Subgrade failure of Qinghai-Tibet highway in permafrost Area," *Highways*, vol. 5, pp. 22–26, 2004.
- [45] M. J. Dou, C. S. Hu, Z. W. He, and Y. Q. Zhang, "Distributing regularities of subgrade diseases in permafrost section of the Qinghai-Tibetan highway," *Journal of Glaciology and Geocryology*, vol. 24, no. 6, pp. 780–784, 2002.
- [46] Q. B. Wu, S. Y. Zhao, W. Ma, Y. Liu, and L. Zhang, "Monitoring and analysis of cooling effect of block-stone embankment for Qinghai-Tibet Railway," *Chinese Journal of Geotechnical Engineering*, vol. 27, no. 12, pp. 1386–1390, 2005.
- [47] L. Chen, W. Yu, X. Yi, D. Hu, and W. Liu, "Numerical simulation of heat transfer of the crushed-rock interlayer embankment of Qinghai-Tibet Railway affected by aeolian sand clogging and climate change," *Cold Regions Science and Technology*, vol. 155, pp. 1–10, 2018.
- [48] S. Z. Zhang, F. J. Niu, J. C. Wang, and T. C. Dong, "Evaluation of damage probability of railway embankments in permafrost regions in Qinghai-Tibet Plateau," *Engineering Geology*, vol. 284, Article ID 106027, 2021.
- [49] F. J. Niu, Z. J. Lin, J. H. Lu, and H. Liu, "Study of the influencing factors of roadbed settlement in embankment-bridge transition section along Qinghai-Tibet Railway," *Rock and Soil Mechanics*, vol. 32, no. S2, pp. 372–377, 2011.
- [50] Q. H. Yu, K. Fan, J. Qian, L. Guo, and Y. H. You, "Key issues of highway construction in permafrost regions in China," *Scientia Sinica Technologica*, vol. 44, pp. 425–432, 2014.
- [51] S. M. Hejazi, M. Sheikhzadeh, S. M. Abtahi, and A. Zadhoush, "A simple review of soil reinforcement by using natural and synthetic fibers," *Construction and Building Materials*, vol. 30, pp. 100–116, 2012.
- [52] H. Y. Fang, *Foundation Engineering Handbook*, Van Nostrand Reinhold, Second Edition, Van Nostrand Reinhold, New York, NY, USA, 1991.
- [53] Ministry of Construction of the People's Republic of China, *Technical Standard for Application of Soil Stabilizer, CJJ/T 286-2018*, China Architecture and Building Press, Beijing, 2018.
- [54] X. S. Lu, W. Xiang, and L. J. Cao, "Zeta potential test of red clay reinforced by soil ionic stabilizer," *Subgrade Engineering*, vol. 147, pp. 32–33, 2009.
- [55] Q. Yang, X. H. Luo, X. Qiu, and J. H. Wu, "Analysis on mechanical behavior characteristics of stabilized clay under the coexistence condition of acidic and alkalic additives," *Journal of Highway and Transportation Research and Development*, vol. 33, no. 6, pp. 46–53, 2016.
- [56] Z. Metelková, J. Boháč, R. Příkryl, and I. Sedlářová, "Maturation of loess treated with variable lime admixture: pore

- space textural evolution and related phase changes,” *Applied Clay Science*, vol. 61, pp. 37–43, 2012.
- [57] N. Latifi, A. S. A. Rashid, S. Siddiqua, and S. Horpibulsuk, “Micro-structural analysis of strength development in low- and high swelling clays stabilized with magnesium chloride solution - a green soil stabilizer,” *Applied Clay Science*, vol. 118, pp. 195–206, 2015.
- [58] H. H. Fan, J. E. Gao, and P. T. Wu, “Prospect of researches on soil stabilizer,” *Journal of Northwest A&F University (Natural Science Edition)*, vol. 34, no. 2, pp. 141–146, 2006.
- [59] J. F. Mi, H. Wang, J. B. Liu, and H. Yan, “Research and application progress of soil stabilizer,” *Materials Reports*, vol. 31, pp. 388–391, 2017.
- [60] M. Y. Hu, C. Fu, L. L. W, and J. Zheng, “Effect of inorganic soil stabilizer on properties of raw soil material,” *Chinese Journal of Materials Research*, vol. 31, no. 6, pp. 445–450, 2017.
- [61] S. Inazumia, S. Intuib, A. Jotisanakasac, S. Chaiprakaikeow, and T. Shinsaka, “Applicability of mixed solidification material based on inorganic waste as soil stabilizer,” *Case Studies in Construction Materials*, vol. 12, Article ID e00305, 2020.
- [62] H. H. Fan, P. T. Wu, J. E. Gao, and Z. K. Lou, “Micro-structure characteristics of soil stabilized with cement-based soil stabilizer,” *Journal of Building Materials*, vol. 13, no. 5, pp. 669–674, 2010.
- [63] N. Hassan, W. H. W. Hassan, A. S. A. Rashid et al., “Microstructural characteristics of organic soils treated with biomass silica stabilizer,” *Environmental Earth Sciences*, vol. 78, no. 12, 2019.
- [64] Q. Li, K. W. Sun, B. Xu, and S. P. Li, “Progress and application on curing mechanism of soil stabilizer,” *Materials Reports*, vol. 25, no. 5, pp. 64–67, 2011.
- [65] H. Afrin, “A review on different types soil stabilization techniques,” *International Journal of Transportation Engineering and Technology*, vol. 3, no. 2, pp. 19–24, 2017.
- [66] M. T. Chai, H. Zhang, J. M. Zhang, and Z. L. Zhang, “Effect of cement additives on unconfined compressive strength of warm and ice-rich frozen soil,” *Construction and Building Materials*, vol. 149, pp. 861–868, 2017.
- [67] M. T. Chai and J. M. Zhang, “Improvement of compressibility and thaw-settlement properties of warm and ice-rich frozen soil with cement and additives,” *Materials*, vol. 12, no. 7, 2019.
- [68] D. E. Scholen, *Nonstandard Stabilizers, Report FHWA-FLP-92-011*, Federal Highway Administration, Washington DC, 1992.
- [69] Q. B. Liu, W. Xiang, W. F. Zhang, and D. S. Cui, “Experimental study of ionic soil stabilizer-improves expansive soil,” *Rock and Soil Mechanics*, vol. 30, no. 8, pp. 2286–2290, 2009.
- [70] D. S. Cui and W. Xiang, “Pore diameter distribution test of red clay treated with ISS,” *Rock and Soil Mechanics*, vol. 31, no. 10, pp. 3096–3100, 2010.
- [71] Q. Yang, X. H. Luo, X. Qiu, and J. H. Wu, “Analysis of microstructure characteristics and stabilization mechanism of ionic soil stabilizer treated clay,” *Journal of Highway and Transportation Research and Development*, vol. 32, no. 11, pp. 33–40, 2015.
- [72] Z. L. Zhang, J. M. Zhang, H. Zhang, and M. T. Chai, “Experimental study of the engineering properties of warm frozen soil treated with ionic soil stabilizer (ISS),” *Journal of Glaciology and Geocryology*, vol. 41, no. 1, pp. 140–146, 2019.
- [73] Z. L. Zhang, J. M. Zhang, and H. Zhang, “Effects and mechanisms of ionic soil stabilizers on warm frozen soil,” *Arabian Journal for Science and Engineering*, vol. 43, no. 10, pp. 5657–5666, 2018.
- [74] W. P. Miller, R. L. Willis, and G. J. Levy, “Aggregate stabilization in kaolinitic soils by low rates of anionic polyacrylamide,” *Soil Use & Management*, vol. 14, pp. 101–105, 1998.
- [75] Y. Li, M. Shao, and R. Horton, “Effect of polyacrylamide applications on Soil hydraulic characteristics and sediment yield of sloping land,” *Procedia Environmental Sciences*, vol. 11, pp. 763–773, 2011.
- [76] R. N. Georgees, R. A. Hassan, and R. P. Evans, “A potential use of a hydrophilic polymeric material to enhance durability properties of pavement materials,” *Construction and Building Materials*, vol. 148, pp. 686–695, 2017.
- [77] H. Soltani-Jigheh, M. Bagheri, and A. R. Amani-Ghadim, “Use of hydrophilic polymeric stabilizer to improve strength and durability of fine-grained soils,” *Cold Regions Science and Technology*, vol. 157, pp. 187–195, 2019.
- [78] A. S. A. Rashid, S. Tabatabaei, S. Horpibulsuk, N. Z. Mohd Yunus, and W. H. W. Hassan, “Shear strength improvement of lateritic soil stabilized by biopolymer based stabilizer,” *Geotechnical & Geological Engineering*, vol. 37, no. 6, pp. 5533–5541, 2019.
- [79] M. Shukla, S. Bose, P. Sikdar, and IRC Seminar, *Integrated Development of Rural and Arterial Road Networks*, National Rural Roads Development Agency, New Delhi, Delhi, 2003.
- [80] M. R. Taha, T. A. Khan, I. T. Jawad, and A. Firoozi, “Recent experimental studies in soil stabilization with bio-enzymes-A review,” *Electronic Journal of Geotechnical Engineering*, vol. 18, pp. 3881–3894, 2013.
- [81] H. L. Zhou and X. D. Shen, “Application research situation and prospect of soil stabilizer,” *Materials Reports*, vol. 28, no. 5, pp. 134–138, 2014.
- [82] Y. M. Wang, M. Z. Su, and L. Zhang, *Sulphoaluminate Cement*, Beijing University of Technology Press, Beijing, China, 1990.
- [83] P. M. Wang, N. Li, and L. L. Xu, “Hydration evolution and compressive strength of calcium sulphoaluminate cement constantly cured over the temperature range of 0 to 80 °C,” *Cement and Concrete Research*, vol. 100, pp. 203–213, 2017.
- [84] C. L. Hu, D. S. Hou, and Z. J. Li, “Micro-mechanical properties of calcium sulfoaluminate cement and the correlation with microstructures,” *Cement and Concrete Composites*, vol. 80, pp. 10–16, 2017.
- [85] J. A. Deng, D. D. Li, Q. D. Li, and S. H. Wu, “The hydration and hardening of high early strength sulfoaluminate cement under subzero performance,” *Journal of the Chinese Ceramic Society*, vol. 11, no. 1, pp. 85–94, 1983.
- [86] H. X. Yang and R. J. Tian, “Effect of sodium nitrite on the hydration process of sulfoaluminate cement at negative temperature,” *China Concrete and Cement Products*, pp. 9–13, 1986.
- [87] G. C. Sun, J. M. Zhang, Y. S. Dang, and C. Ding, “Micro-structure and strength features of warm and ice-rich frozen soil treated with high-performance cements,” *Journal of Mountain Science*, vol. 16, no. 6, pp. 1470–1482, 2019.
- [88] Z. H. Yin, J. M. Zhang, H. Zhang, and H. L. Wang, “Water transfer law of cement improved frozen soil and the effect on the strength,” *Journal of Harbin Institute of Technology*, vol. 53, no. 11, pp. 136–144, 2020.
- [89] G. C. Sun, J. M. Zhang, Y. S. Dang, H. Zhang, C. Ding, and X. Chen, “Structural properties changes before and after solidification and their effects on melting and compression

- characteristics of high warm and frozen soil,” *Journal of Harbin Institute of Technology*, vol. 52, no. 2, pp. 17–25, 2020.
- [90] Z. H. Yin, H. Zhang, J. M. Zhang, and M. T. Chai, “Mechanical behavior of frozen soil improved with sulphoaluminate cement and its microscopic mechanism,” *Scientific Reports*, vol. 10, Article ID 16297, 2020.
- [91] Y. H. Qin, J. M. Zhang, B. Zheng, and X. J. Ma, “Experimental study for the compressible behavior of warm and ice-rich frozen soil under the embankment of Qinghai-Tibet Railroad,” *Cold Regions Science and Technology*, vol. 57, no. 2-3, pp. 148–153, 2009.
- [92] H. Zhang, J. M. Zhang, Z. L. Zhang, and M. T. Chai, “Measuring the long-term deformation of in-situ ice-rich permafrost using a plate loading test,” *Measurement*, vol. 149, Article ID 107030, 2020.
- [93] H. Zhang, J. Zhang, Z. Zhang, J. Chen, and Y. You, “A consolidation model for estimating the settlement of warm permafrost,” *Computers and Geotechnics*, vol. 76, pp. 43–50, 2016.
- [94] S. Y. Liu, G. C. Qian, and D. W. Zhang, *The Principle and Application of Dry Jet Mixing Composite Foundation*, China Architecture and Building Press, Beijing, 2006.
- [95] A. Porbaha, “State of the art in deep mixing technology: part I. Basic concepts and overview,” *Proceedings of the Institution of Civil Engineers - Ground Improvement*, vol. 2, no. 2, pp. 81–92, 1998.
- [96] X. N. Gong, *The Principle and Application of Composite Foundation*, China Architecture and Building Press, Beijing, 2007.
- [97] G. Holm, “State of practice in dry deep mixing methods,” in *Proceedings of the Third International Conference on Grouting and Ground Treatment*, pp. 581–593, ASCE, New Orleans, Louisiana, United States, February 2003.
- [98] S. L. Shen, N. Miura, and H. Koga, “Interaction mechanism between deep mixing column and surrounding clay during installation,” *Canadian Geotechnical Journal*, vol. 40, no. 2, pp. 293–307, 2003.
- [99] S. Y. Liu, Y. J. Du, Y. L. Yi, and A. J. Puppala, “Field investigations on performance of T-shaped deep mixed soil cement column-supported embankments over soft ground,” *Journal of Geotechnical and Geoenvironmental Engineering*, vol. 138, no. 6, pp. 718–727, 2012.
- [100] Y. L. Yi, S. Y. Liu, and A. J. Puppala, “Laboratory modelling of T-shaped soil-cement column for soft ground treatment under embankment,” *Géotechnique*, vol. 66, no. 1, pp. 85–89, 2016.
- [101] M. T. Chai, J. M. Zhang, W. Ma, Z. H. Yin, Y. H. Mu, and H. Zhang, “Thermal influences of stabilization on warm and ice-rich permafrost with cement: field observation and numerical simulation,” *Applied Thermal Engineering*, vol. 148, pp. 536–543, 2019.
- [102] W. Xiang, S. Y. Liu, F. Jing, and Z. B. Liu, “Bearing capacity of composite foundation of soil cement deep mixing columns with different cross section parts,” *Journal of Southeast University (Natural Science Edition)*, vol. 39, no. 2, pp. 328–333, 2009.
- [103] X. G. Song, S. G. Wang, Y. S. Yang, and Y. H. Zhang, “Field study of load transfer behavior of DJMP,” *Rock and Soil Mechanics*, vol. 20, no. 4, pp. 81–85, 1999.
- [104] H. Tsyrovich, “The mechanics of frozen ground,” in *Translation*, C. Q. Zhang, and Y. L. Zhu, Eds., Science Press, Beijing, 1988.
- [105] J. L. Qi and W. Ma, “State-of-art of research on mechanical properties of frozen soils,” *Rock and Soil Mechanics*, vol. 31, no. 1, pp. 133–143, 2010.
- [106] Z. W. Wu and W. Ma, *Strength and Creep of Frozen Soil*, Lanzhou University Press, Chengguan, China, 1994.
- [107] Q. B. Wu, Z. J. Li, and Y. P. Shen, “Cryosphere engineering science supporting interactivity infrastructures construction,” *Bulletin of Chinese Academy of Sciences*, vol. 35, no. 4, pp. 443–449, 2020.