

Research Article

Estimating Rice Panicle Temperature with Three-Layer Model

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Rice panicle temperature (T_p) is a key factor for studying high temperature impacts on spikelet sterility. Comparing with measuring T_p by hand, a T_p simulation model could obtain T_p data readily. The two-layer energy budget model which divides the soil layer and canopy layer was widely used to predict rice canopy temperature (T_c), but panicle existed mostly in the upper layer canopy, and we have proved that T_c was different from the upper layer canopy temperature (T_{c1}), and the upper layer must be separated from the whole canopy for the purpose of estimating T_p . Thus, we developed the three-layer model, contained upper canopy layer with panicle (50–100 cm), lower rice canopy layer (10–40 cm), and water surface layer (≤ 10 cm) to estimate T_p with general meteorological and vegetation growth data. There were two steps to estimate T_p . The first step was calculating T_{c1} and lower layer canopy temperature (T_{c2}) by solving heat balance equations with canopy resistances. And the second step was estimating T_p with following parameters: (a) the inclination factors of leaves and panicles (F_1 , F_2 , and F_p) which were decided by fitting the calculated transmissivity of downward solar radiation (TDSR) to the measured TDSR, (b) the aerodynamic resistance between the panicle and atmosphere (r_{ap}) denoted by wind speed, (c) the panicle resistance for transpiration (r_p) denoted by days after heading, and (d) air temperature and humidity at the panicle's height (T_{ac1} and e_{ac1}) calculated from the resistances of the pathways of sensible and latent heat fluxes in accordance with Ohm's law. The model simulated fairly well the T_{c1} , T_{c2} , and T_p with root mean square errors (RMSEs) of 0.76°C, 0.75°C, and 0.81°C, respectively, where RMSE of measured T_p and predicted T_p by integrated micrometeorology model for panicle and canopy temperature (IM²PACT) including two-layer model was 1.27°C. This model was validated well by two other rice cultivars, and thus, it demonstrated the three-layer model was a new feasible way to estimate T_p .

1. Introduction

With increasing concerns about global warming, the impacts of higher temperature on rice production have become a major focus in many rice-producing countries in tropical, subtropical, and temperate regions [1–9]. In China, extreme high temperature in 2003 caused about 5 million tonnes of rice yield loss [10], while unusual temperatures ($>40^\circ\text{C}$) in many areas of Kanto and Tokai regions of Japan resulted in 25% spikelet sterility in 2007 [11].

Rice panicle is most sensitive to high temperature during the flowering stage [12–16]. It has been proved that high temperature prevents anther dehiscence and decreases basal

pore length of the anther, resulting in low numbers of germinating pollen grains on the stigma, and thus, it causes spikelet sterility [7, 12, 15, 17–22].

Effect of high temperature on spikelet sterility has been studied under different conditions. Matsui et al. [23] reported that spikelet fertility was significantly damaged when daily maximum air temperature exceeded 35°C . Abeyisiriwardena et al. [24] revealed high temperature condition (35°C day/ 30°C night) induced complete grain sterility when relative humidity (RH) was 85–95%. Contrary to the results above, [25, 26] demonstrated spikelet sterility of rice did not occur seriously even daily maximum T_a was over 40°C in Australia during the 2004–2006 growing seasons because the

strong transpirational cooling by low relative humidity (<20%) brought panicle temperature (T_p) 6.8°C lower than T_a . But spikelet sterility occurred frequently in Jiangnan Basin, China, where T_a was not so high, since T_p was 4.0°C higher than T_a under high solar radiation with high RH (>80%) and low wind speed ($u < 1 \text{ m s}^{-1}$) conditions [27]. Therefore, T_p instead of T_a is a key factor for high temperature impact study. As measuring T_p was a time-consuming and laborious work, a T_p simulation model was needed to obtain T_p data readily.

Until now, only limited information has been reported about panicle temperature models. Sheehy et al. [28] developed a T_p model with air temperature and thermal burden. Oue et al. [29] measured T_p in every 10 cm rice canopy layer in the CO₂ ambient and CO₂ elevated plots during the daytime in Wuxi, China, and developed a heat balance model of T_p based on the measured stomatal conductance. To date, the whole canopy temperature (T_c) predicted by the two-layer model has been used to calculate the long-wave radiations to the panicle as shown in the integrated micrometeorology model for panicle and canopy temperature (IM²PACT) [30]. However, panicle exists mostly in the upper layer canopy, and we have proved that T_c is different from the upper layer canopy temperature (T_{c1}), and the upper layer must be separated from the whole canopy for the purpose of estimating T_p , whereas the multilayer model [31] required many vertical profiles of micrometeorological environments and fluxes of momentum, and heat and vapor within and above a vegetation, making it unusable to predict T_p with insufficient data.

Therefore, the objectives of this paper are (1) to develop a three-layer model to calculate panicle temperature based on general meteorological and vegetation growth data and (2) to compare the performance to estimate T_p by three-layer model and T_p by IM²PACT [30] including two-layer model.

2. Materials and Methods

2.1. Measurements in the Rice Paddy Field. The experimental paddy field was located in the Ehime University Senior High School, Matsuyama, Japan (33°50'N, 132°47'E). The Japonica type rice (cultivar Akitakomachi) was transplanted with 20 × 30 cm spacing on May 27, 2014, and then harvested on September 8, 2014.

The global solar radiation (S_t), downward long-wave radiation (L_d), and upward long-wave radiation (L_u) above the rice canopy were detected using pyranometer CNR-4 (Kipp & Zonen, the Netherlands) at 2.0 m height from the ground. To measure soil heat flux (G), a soil heat plate CHF-HDP01 (Campbell Scientific Inc., Logan, UT, USA) was buried in the soil surface. Air temperature (T_a) and relative humidity (RH) were observed using ventilated psychrometers HMP-45A (Vaisala Inc., Helsinki, Finland), first mounted at 0.6 m and 1.0 m of a 2.5 m tower, and then lifted to 1.0 m and 1.5 m on July 28, respectively, when rice plant was 81 cm in height. Three-cup anemometers 014A (MetOne, USA) were mounted as the same heights of psychrometers to measure the wind speed (u). Downward and

upward long-wave radiations beneath the rice canopy were both measured with PRI-01 (Prede, Japan) sensors. Water surface temperature (T_w) or ground surface temperature (T_g) was measured with the thermocouple sensor. All data were sampled per 10 s; then, they were averaged and recorded per 10 min using a data logger CR23x (Campbell Scientific Inc., Logan, UT, USA).

Three stubs of rice were taken to measure the upper layer canopy temperature (T_{c1}), the lower layer canopy temperature (T_{c2}), and the panicle temperature (T_p) per 2 or 3 h in the daytime using an infrared thermometer THI-500 (Tasco, Japan). The solar radiation within rice canopy was measured with a line type pyranometer PCM200 (Prede, Japan) in the center between stubs in parallel and perpendicular directions, of which the average was calibrated from the solar radiation measured with CNR-4 (Kipp & Zonen, the Netherlands) at 2.0 m. The transmissivity of downward solar radiation (TDSR) refers to the ratio of the S_t in the rice canopy in every 10 cm to that above the rice canopy. Subsequently, the average TDSRs from 50 cm to 100 cm and from 10 cm to 40 cm were set as the upper and lower layer rice canopy TDSRs, respectively. TDSRs were measured from 10 cm to the top of the canopy per 10 cm and 1.2 m (above the rice canopy). The canopy temperature, T_p , and solar radiation within canopy data were recorded using ZRRX 20 portable multilogger (Omron, Japan). At the heading and the flowering stage, irrigation was performed in the paddy field at 5-day interval. Besides, 8 cm depth irrigation water decreased to 0 through evaporation and infiltration in one and a half days. At the ripening stage, there was almost no water.

Plant area density (PAD) was sampled three rice plants at the interval of one week. The taken three rice plants were cut at intervals of 10 cm, split into components of leaves, stems, and panicles, respectively, and then scanned. Lastly, the area of each part (projected area for panicle) was calculated using ImageJ software. Water depth (d_w) was measured per two or three hours in the daytime. Water surface evaporation (E_g) beneath the rice canopy was measured with the lysimeter (length × width × depth: 60 × 20 × 30 cm) and recorded twice (8:30 and 18:30) per day.

2.2. Estimating Panicle Temperature (T_p) with Three-Layer Model. The input data of the three-layer model to estimate T_p include (a) hourly radiations, (b) temperature, humidity, and wind speed, (c) water surface data, and (d) vegetation growth data. T_p was estimated in two steps. The first step was calculating T_{c1} and T_{c2} by solving heat balance equations with canopy resistances and the second step was estimating T_p with calculated T_{c1} and T_{c2} .

The schematic of the aerodynamic resistance and upper and lower layer canopy resistances of one-layer and three-layer models is illustrated in Figure 1. The schematic diagram illustrating the method for estimation T_{c1} , T_{c2} , and T_p by the three-layer model is shown in Figure 2. And the input parameters required for the calculation in the model are shown in Table 1.

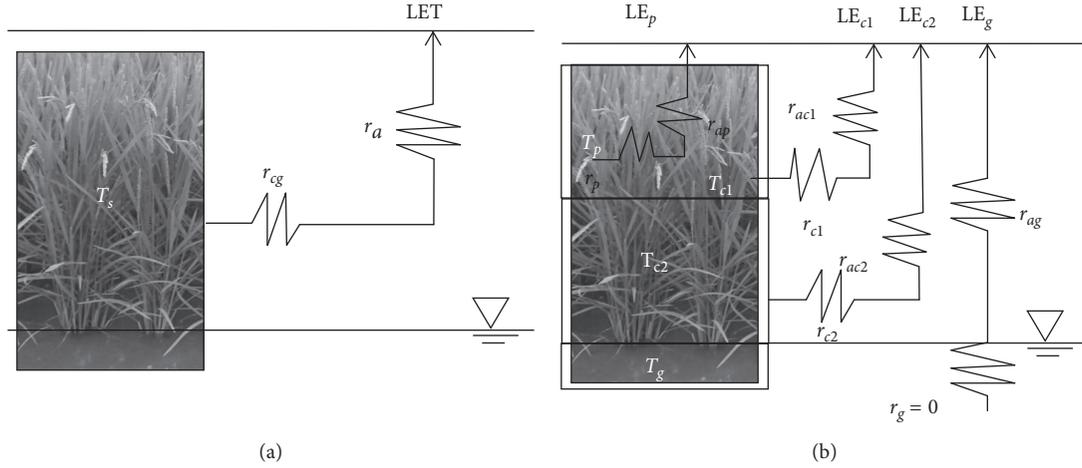


FIGURE 1: A schematic representation of the aerodynamic resistance and upper and lower canopy resistances of (a) one-layer and (b) three-layer models. LET was the latent heat flux for the whole canopy (W m^{-2}), T_s was the surface temperature of the paddy field ($^{\circ}\text{C}$), r_a was the aerodynamic resistance to the transfer of sensible heat between the whole rice canopy and water surface (s m^{-1}), r_{cg} was the total canopy resistance consists of rice canopy resistance and water surface resistance (s m^{-1}), LE_p was the latent heat flux on a panicle (W m^{-2}), LE_{c1} was the latent heat flux between upper layer rice canopy and atmosphere (W m^{-2}), LE_{c2} was the latent heat flux between lower layer rice canopy and atmosphere (W m^{-2}), LE_g was the latent heat flux between water surface beneath the rice canopy and atmosphere (W m^{-2}), T_p was the panicle temperature ($^{\circ}\text{C}$), T_{c1} was the upper layer canopy temperature ($^{\circ}\text{C}$), T_{c2} was the lower layer canopy temperature ($^{\circ}\text{C}$), T_g was the water temperature ($^{\circ}\text{C}$), r_{ap} was the aerodynamic resistance to the transfer of sensible heat between panicle and atmosphere (s m^{-1}), r_{ac1} was the aerodynamic resistance to the transfer of sensible heat between upper layer rice canopy and atmosphere (s m^{-1}), r_{ac2} was the aerodynamic resistance to the transfer of sensible heat between lower layer rice canopy and atmosphere (s m^{-1}), r_{ag} was the aerodynamic resistance to the transfer of sensible heat between water surface and atmosphere (s m^{-1}), r_p was the panicle transpiration resistance (s m^{-1}), r_{c1} was the upper layer canopy resistance (s m^{-1}), r_{c2} was the lower layer canopy resistance (s m^{-1}), and r_g was albedo of water surface (s m^{-1}).

In the one-layer model, the rice canopy and water surface were set as a whole, and energy budget in a paddy field was expressed as follows:

$$R_n = \text{LET} + H + G + \delta W, \quad (1)$$

$$\delta W = \frac{C_w d_w [T_{w(t+1)} - T_{w(t)}]}{\delta t}, \quad (2)$$

where R_n was the net radiation (W m^{-2}), LET was the latent heat flux (W m^{-2}), H was the sensible heat flux (W m^{-2}) for the whole canopy, and δW was the change of storage energy in the water surface (W m^{-2}) calculated by equation (2) based on the measured water temperatures and water depth. LET was calculated by the Bowen ratio method (equation 3(a)) with air temperatures and water vapor pressure of air at two different heights, and H was calculated by equation (1). Aerodynamic resistance between the whole rice canopy and water surface (r_a) and the total canopy resistance that consists of rice canopy resistance and water surface resistance (r_{cg}) was calculated by equations (3b) and (3c):

$$\text{LET} = \frac{(R_n - G)}{(1 + Bo)}, \quad (3a)$$

$$H = \frac{c_p \rho (T_s - T_a)}{r_a}, \quad (3b)$$

$$\text{LET} = \frac{c_p \rho [e_{\text{sat}}(T_s) - e_a]}{[\gamma(r_a + r_{cg})]}, \quad (3c)$$

where c_p was the specific heat capacity of the air at constant pressure ($\text{J g}^{-1} \text{ } ^{\circ}\text{C}^{-1}$), ρ was the air density (kg m^{-3}), T_s was the surface temperature of the paddy field ($^{\circ}\text{C}$), $e_{\text{sat}}(T_s)$ was the saturation-specific humidity at T_s (hPa), and e_a was the specific humidity of the air (kg kg^{-1}).

T_s was the surface temperature of the paddy field ($^{\circ}\text{C}$) calculated based on the upward long-wave radiation (L_u) and downward long-wave radiation (L_d), as expressed in the following equation:

$$L_u = \varepsilon_s \sigma T_s^4 + (1 - \varepsilon_s) L_d, \quad (4)$$

where ε_s was the surface emissivity set as 0.97 in this study.

Based on the data of measured G , δW , LE, and H were calculated by equation (1), and T_s was obtained by equation (4). Subsequently, r_a was obtained by equation (3b), and lastly r_{cg} was calculated by equation (3c) based on the data of measured T_a , e_a , and LET.

In the three-layer model, net radiation (R_n) sums the net radiation absorbed by upper canopy layer (R_{nc1}), the net radiation absorbed by lower canopy layer (R_{nc2}), and the net radiation absorbed by water surface layer (R_{ng}):

$$R_n = R_{nc1} + R_{nc2} + R_{ng}. \quad (5)$$

The energy budget equations for water surface were written from the following equations:

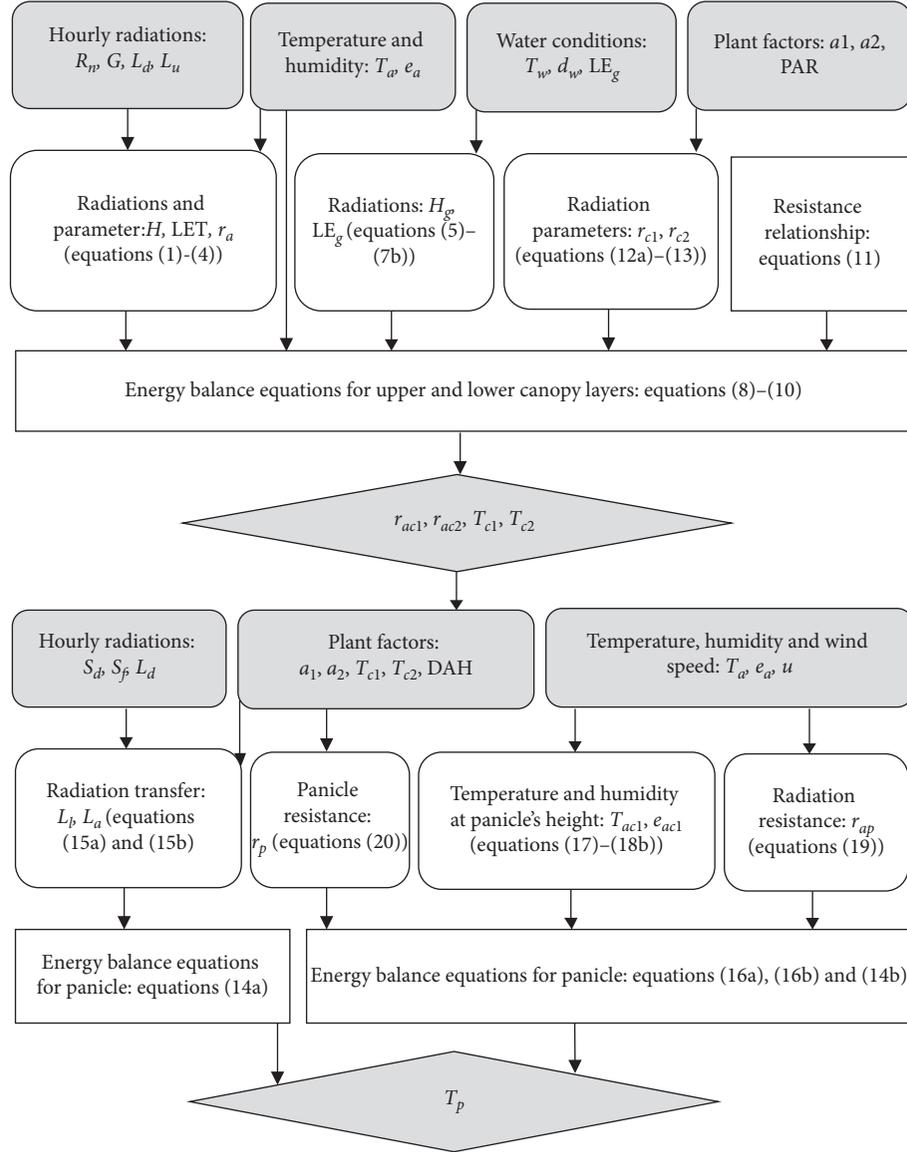


FIGURE 2: A schematic diagram illustrating the method for estimating upper and lower layer canopy temperatures (T_{c1} and T_{c2}) and panicle temperature (T_p). The grey rounded rectangles denote input data, and the grey diamonds denote output data.

$$R_{ng} = H_g + LE_g + G + \delta W, \quad (6)$$

$$LE_g = \frac{c_p \rho [e_{sat}(T_g) - e_a]}{[\gamma(r_{ag} + r_g)]}, \quad (7a)$$

$$H_g = \frac{c_p \rho (T_g - T_a)}{r_{ag}}, \quad (7b)$$

where H_g was the sensible heat flux between water surface beneath canopy and atmosphere (W m^{-2}) LE_g was the latent heat flux between water surface beneath canopy and atmosphere (W m^{-2}) obtained from the water surface evaporation by the lysimeter, T_g was the ground surface temperature ($^{\circ}\text{C}$) (assumed $T_g = T_w$ in the model), $e_{sat}(T_g)$

was the saturation-specific humidity at T_g (hPa), γ was the psychrometric constant ($\text{kPa } ^{\circ}\text{C}^{-1}$), r_{ag} was calculated by equation (7a) based on the measured LE_g and T_g first, H_g was calculated by equation (7b), and then R_{ng} , $R_{nc1} + R_{nc2}$ were calculated by equations (5) and (6), respectively.

The energy budget equations for upper canopy layer (50–100 cm) and lower canopy layer (10–40 cm) were written from equations (8) to (10c):

$$R_{nc1} + R_{nc2} = H_{c1} + LE_{c1} + H_{c2} + LE_{c2}, \quad (8)$$

$$H_{c1} + H_{c2} = H - H_g, \quad (9a)$$

$$H_{c1} = \frac{c_p \rho (T_{c1} - T_a)}{r_{ac1}}, \quad (9b)$$

TABLE 1: Input parameters required for the calculation in the three-layer model.

Symbol	Name	Unit
<i>Forcing parameters</i>		
R_n	Net radiation for the whole canopy	$W m^{-2}$
G	Soil heat flux	$W m^{-2}$
L_d	Downward long-wave radiation for the whole canopy	$W m^{-2}$
L_u	Upward long-wave radiation for the whole canopy	$W m^{-2}$
T_a	Air temperature	$^{\circ}C$
e_a	Water vapor pressure of the air	hPa
u	Wind speed	$m s^{-2}$
<i>Ground characteristics</i>		
T_w	Water temperature	$^{\circ}C$
d_w	Water depth	m
LE_g	Latent heat flux between water surface beneath canopy and atmosphere	$W m^{-2}$
<i>Canopy characteristics</i>		
a_1	Green leaf and yellow leaf area index in the upper canopy layer	$m^2 m^{-3}$
a_2	Green leaf and yellow leaf area index in the lower canopy layer	$m^2 m^{-3}$
PAR	Photosynthetically active radiation	$\mu mol m^{-2} s^{-1}$
g_s	Stomatal resistance	$cm s^{-1}$

Note: g_s was referred to Oue's literature [32]; other data were observed.

$$H_{c2} = \frac{c_p \rho (T_{c2} - T_a)}{r_{ac2}}, \quad (9c)$$

$$LE_{c1} + LE_{c2} = LET - LE_g, \quad (10a)$$

$$LE_{c1} = \frac{c_p \rho [e_{sat}(T_{c1}) - e_a]}{[\gamma(r_{c1} + r_{ac1})]}, \quad (10b)$$

$$LE_{c2} = \frac{c_p \rho [e_{sat}(T_{c2}) - e_a]}{[\gamma(r_{c2} + r_{ac2})]}, \quad (10c)$$

where LE_{c1} and LE_{c2} were the latent heat flux between upper and lower layer canopy and atmosphere ($W m^{-2}$), respectively. H_{c1} and H_{c2} were the sensible heat flux between upper and lower layer canopy and atmosphere ($W m^{-2}$), respectively. T_{c1} was the upper layer canopy temperature ($^{\circ}C$), T_{c2} was the lower layer canopy temperature ($^{\circ}C$), $e_{sat}(T_{c1})$ and $e_{sat}(T_{c2})$ were the saturation-specific humidity at T_{c1} and T_{c2}

(hPa), r_{ac1} and r_{ac2} were aerodynamic resistances to the transfer of sensible heat between upper and lower layer canopy and atmosphere ($s m^{-1}$), respectively, r_{c1} and r_{c2} were the upper and lower layer canopy resistances ($s m^{-1}$), respectively.

For the aerodynamic resistances, the association of r_a , r_{ag} , r_{ac1} , and r_{ac2} was expressed in the following equation:

$$\frac{1}{r_a} = \frac{1}{r_{ag}} + \frac{1}{r_{ac1}} + \frac{1}{r_{ac2}}. \quad (11)$$

In this study, r_{c1} and r_{c2} were calculated by stomatal resistance (g_s), green leaf and yellow leaf area index in the upper rice canopy layer (a_1), and green leaf and yellow leaf area index in the lower rice canopy layer (a_2), as expressed in equations (12a) and (12b). Because g_s was not measured in the experimental paddy field in 2014, g_s developed by Oue [32] was adopted (values as shown in Table 2), as expressed in equation (13):

$$r_{c1} = \frac{1}{(g_s a_1)}, \quad (12a)$$

$$r_{c2} = \frac{1}{(g_s a_2)}, \quad (12b)$$

$$g_s = \frac{[m_s PAR + (g_{s \max} - g_{s \min})]}{2n_s} + g_{s \min} - \frac{1}{2n_s \times \left\{ [m_s PAR + (g_{s \max} - g_{s \min})]^2 - 4m_s PAR (g_{s \max} - g_{s \min}) n_s \right\}^{1/2}}, \quad (13)$$

where g_s was the stomatal conductance ($cm s^{-1}$), m_s and n_s were parameters, PAR was photosynthetically active radiation ($\mu mol m^{-2} s^{-1}$), $g_{s \max}$ was the maximum of stomatal conductance ($cm s^{-1}$), and $g_{s \min}$ was the minimum of stomatal conductance ($cm s^{-1}$).

With the calculated r_{c1} and r_{c2} , T_{c1} , T_{c2} , r_{ac1} , and r_{ac2} were calculated by equations (8)–(10c).

The net radiation input to a panicle (R_{in}) sums shortwave and long-wave radiation absorbed by the panicle ($W m^{-2}$), as expressed in equation (14a). L_l and L_a were long-wave

TABLE 2: m_s and $g_{s\max}$ in the g_s model.

Date	Canopy layer	VPD (hPa)	m_s (cm s ⁻¹)/(μ mol m ⁻² s ⁻¹)	$g_{s\max}$ (cm s ⁻¹)
August 6	Upper	~18	0.00247	1.500
		18~	0.00170	0.500
	Lower	~10	0.002405	1.500
		10~15	0.002095	1.200
		15~	0.001925	0.800
August 13	Upper	~8	0.00780	0.820
		8~	0.01246	0.410
	Lower	~8	0.009935	0.515
		8~	0.00833	0.470
August 27	Upper	~9	0.00282	0.500
		9~	0.00195	0.400
	Lower	~10	0.003155	0.900
		10~11	0.00261	0.750
September 4	Upper	~16	0.003475	0.550
		16~	0.000445	0.400
	Lower	~15	0.001315	0.400
		15~16	0.00123	0.400
		~16	0.00615	0.400

Note: VPD is vapor pressure deficit, g_s is the stomatal conductance (cm s⁻¹), $g_{s\max}$ is the maximum of stomatal conductance (cm s⁻¹), $g_{s\min}$ is the minimum of stomatal conductance (cm s⁻¹), and m_s and n_s are parameters.

radiations from a leaf surface adjacent to the panicle and from the atmosphere (W m⁻²), respectively. S_d and S_f were downward direct and diffused shortwave radiations (W m⁻²), respectively, and θ was the solar zenith angle (°), F_p was the inclination factor of panicle, and d_f was the diffusivity factor for radiation. Besides, the heat balance in the panicle layer was written as equation (14b).

$$R_{in} = (1 - 0.35)F_p(\sec\theta S_d + 2d_f S_f) + F_p d_f (L_l + L_a), \quad (14a)$$

$$R_{in} = 2F_p d_f \sigma T_p^4 + H_p + LE_p, \quad (14b)$$

$$L_l = \sigma T_{c1}^4 + (L_d - \sigma T_{c1}^4) \exp(-F_1 a_1 d_f), \quad (15a)$$

$$L_a = \sigma T_{c2}^4 + (\sigma T_g^4 - \sigma T_{c2}^4) \exp(-F_2 a_2 d_f) + \sigma T_{c1}^4 + (\sigma T_{c2}^4 - \sigma T_{c1}^4) \exp(-F_1 a_1 d_f), \quad (15b)$$

where F_1 and F_2 were the inclination factors of upper and lower layer rice canopy, respectively. F_1 , F_2 , and F_p were decided by fitting the calculated transmissivity of downward solar radiation (TDSR) to the measured TDSR (Figure 3).

Besides, H_p and LE_p were sensible and latent heat fluxes on a panicle (W m⁻²), which were written as follows:

$$H_p = \frac{c_p \rho (T_p - T_{ac1})}{r_{ap}}, \quad (16a)$$

$$LE_p = \frac{c_p \rho [e_{\text{sat}}(T_p) - e(T_{ac1})]}{[\gamma(r_{ap} + r_p)]}, \quad (16b)$$

$$\frac{(T_{c1} - T_{ac1})}{r_{c1}} = \frac{(T_{ac1} - T_a)}{r_{ac1}}. \quad (17)$$

Moreover, T_{ac1} was the air temperature at panicle's height (°C) which was calculated by the transposition of equation (17) as shown in equation (18a), and likewise, e_{ac1} was the absolute humidity at panicle's height (hPa) calculated as expressed in equation (18b):

$$T_{ac1} = \frac{(r_{ac1} T_{c1} + r_{c1} T_a)}{(r_{c1} + r_{ac1})}, \quad (18a)$$

$$e_{ac1} = \frac{(r_{ac1} T_{c1} + r_{c1} e_a)}{(r_{c1} + r_{ac1})}, \quad (18b)$$

where r_{ap} , the aerodynamic resistance to the transfer of sensible heat between panicle and atmosphere (s m⁻¹), denoted the parameter of wind speed (Section 3.3.2), and then r_p , panicle transpiration resistance (s m⁻¹), denoted the parameter of days after the heading stage (Section 3.3.3). Lastly, T_p was calculated by combining equations from equations (14a) to (18b).

The average value of measured panicle temperature from 50 cm to 100 cm was set as the measured T_p , which was compared with the T_p using the three-layer model and by IM²PACT [30] including the two-layer model.

2.3. Statistical Analysis of Models. The measured and calculated T_{c1} , T_{c2} , and T_p were compared by using error analysis and linear regression. Root mean squared error (RMSE), mean absolute error (MAE), and the standard deviation (SD) [33–35] were adopted to evaluate measured and calculated T_{c1} , T_{c2} , T_c and T_p by the models.

2.4. Three-Layer Model Validation. We planted rice (cultivar Hinohikari) from June 21 to November 20, 2015, and rice (cultivar Nikomaru) from June 21 to November 27, 2015, in the same paddy field. PAD of two cultivars was both

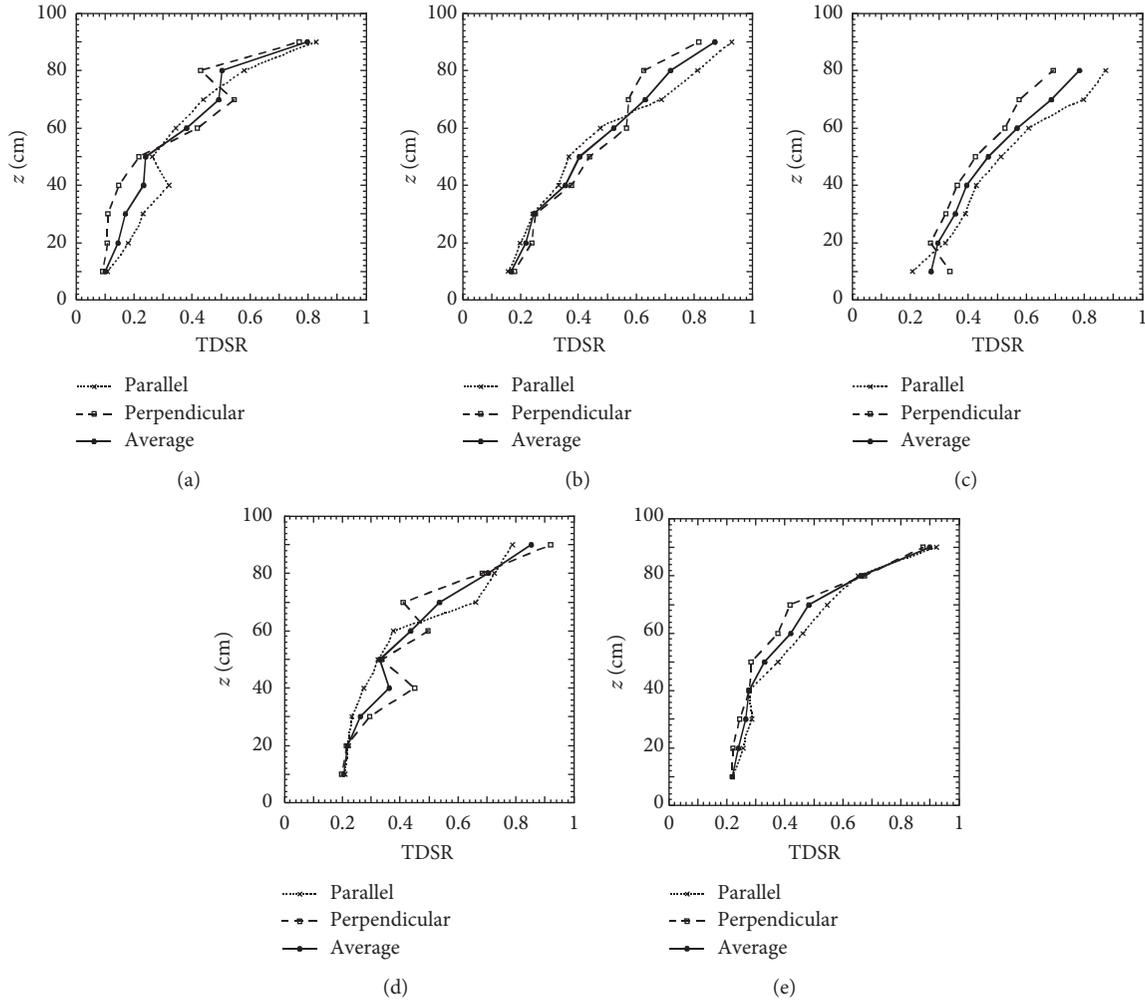


FIGURE 3: Vertical profiles of transmissivity of downward solar radiation (TDSR) within the rice canopy in every 10 cm in the paddy field on August 7, 2014 (a–e). (a) 8:50, (b) 10:50, (c) 12:40, (d) 14:50, and (e) 16:40.

measured from July 9 to October 14, 2015. Other meteorological instruments were set as same as 2014. Six images were taken to get T_c and T_p by infrared thermometer FLIR-i5 (FLIR systems, USA) at different heights every two or three hours during daytime.

3. Results and Discussion

3.1. General Meteorological Conditions. From July 18 to September 8, the daily average global solar radiation (S_t) was 262 W m^{-2} , the average air temperature (T_a) was 25°C , while the highest T_a was 35°C on July 26, 2014. The average relative humidity (RH) was 81%, and the average wind speed (u) at 1.0 m reached 0.5 m s^{-1} . The total precipitation, the total evapotranspiration, and the daily evapotranspiration were 670 mm, 567 mm, and 5 mm, respectively.

3.2. Plant Area Density (PAD). Panicles' height ranges from 50 cm to 100 cm, and this part of the rice plant was set as the upper canopy layer. There was no panicle on July 18, and the heading was observed on July 25 (Figure 4). The average of the

measured green leaf and yellow leaf area index in the upper layer rice canopy (a_1) ranged from 50 cm to 100 cm, which reached its peak on August 8 (2.5) and then decreased. However, green leaf and yellow leaf area index in the lower layer rice canopy (a_2) decreased from 3 on July 25 to 1.5 on August 8, 2014.

3.3. Modeling Parameter Results

3.3.1. Parameters F_1 , F_2 , and F_p . From August 5 to September 7 in the ripening stage, there was a little diurnal variation of rice morphology.

F_1 was smaller than F_2 because the transmissivity of solar radiation was larger in the upper layer, and the leaf area index of the upper layer canopy (a_1) was also bigger than that in the lower layer (a_2). For example, a_1 was 2.5 and a_2 was 1.5 on August 8. F_1 and F_2 were larger in the morning and afternoon than those at noon, respectively. This was because of the different solar radiation altitudes: in the morning and afternoon, the solar altitude was low, and the solar radiation in the upper layer was large after cutting off, and at noon, the solar radiation was the highest, and the

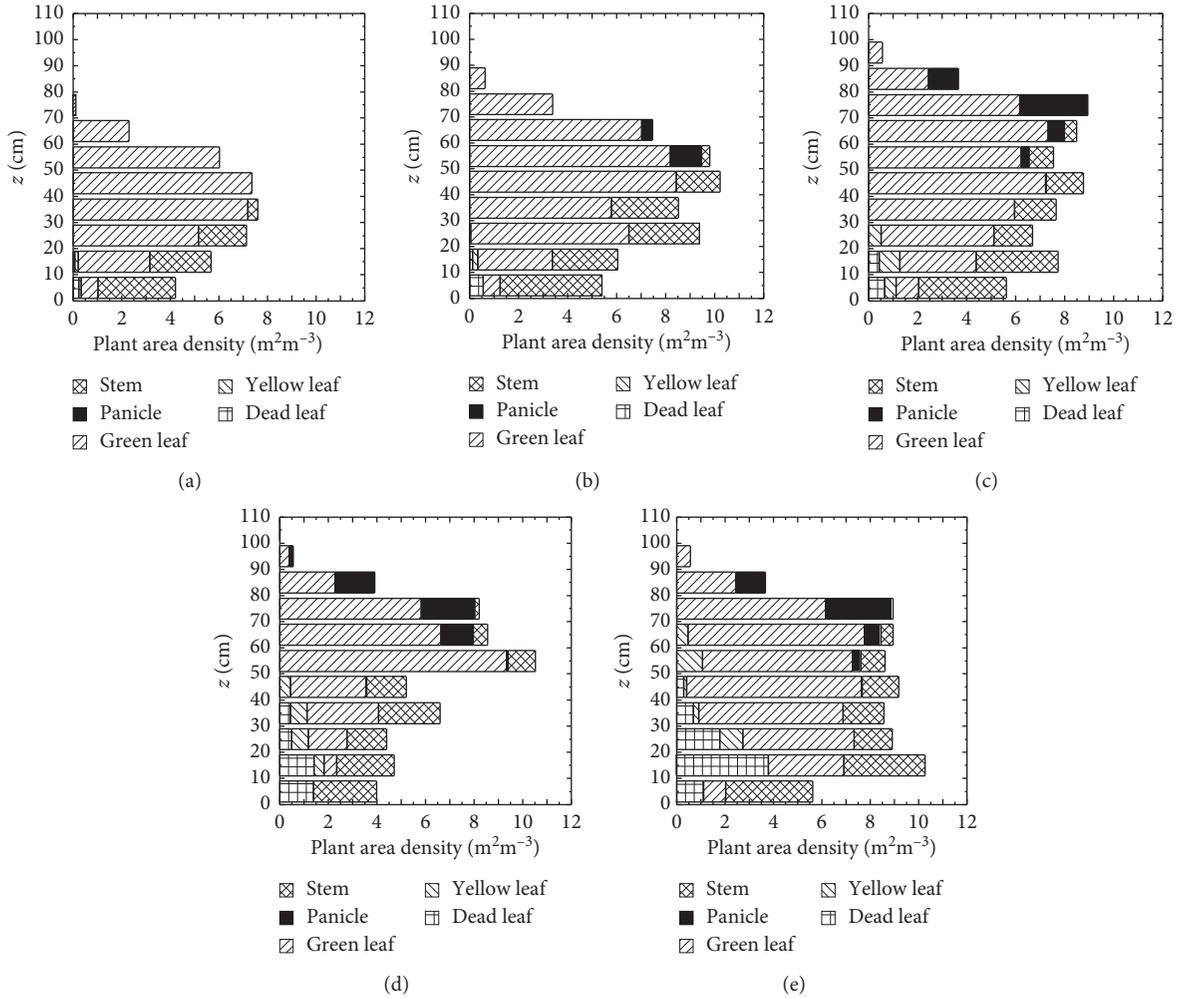


FIGURE 4: Observed vertical profiles of plant area density (PAD) in the rice paddy field from July 18 to August 15, 2014. (a) July 18, (b) July 25, (c) August 1, (d) August 8, and (e) August 15.

solar radiation in the upper layer was smaller after cutting off. This was dependent on the morphology of canopy: leaves stood upright from 60 cm to 100 cm in the upper layer. In the lower layer, in the morning and afternoon, the solar radiation coming diagonally would be cut off by leaves, while at noon, the solar radiation coming from overhead would not be largely cut off, thereby leading to the smaller F_1 and F_2 during this period.

F_p was important after the ripening stage, when the panicles hung their heads and cover the top of the canopy [36]. F_p variation was similar to that of F_1 from morning to afternoon because of the similar form of panicles and leaves.

F_1 and F_2 were smaller than the leaf inclination factor (F) in the ripening stage published by Maruyama et al. [37]. To estimate the radiation exchange processes in the rice canopy, the hourly variation of F_1 , F_2 , and F_p should be considered for accuracy.

3.3.2. Aerodynamic Resistance between the Panicle and Atmosphere (r_{ap}). Table 3 lists the aerodynamic resistance between the panicle and atmosphere (r_{ap}) and

meteorological data when r_p was set as 0: there was rain before, or dew was found in the morning (August 5, 7, 18, 26, and 28).

As a result of correlation analysis between the meteorological conditions (S_b , T_a , RH, and u) and r_{ap} , it was found that r_{ap} was primarily affected by u with the correlation coefficient of -0.93 . This is consistent with the results reported by Yan and Oue [38], which suggested that u at 2.0 m from the ground was the major factor affecting r_a , r_{ag} , and r_{ac} (aerodynamic resistance between the rice canopy and atmosphere). The association between u ($0.35 \text{ m s}^{-1} < u < 1.75 \text{ m s}^{-1}$) and r_{ap} on the same days is shown in Figure 5(a), as expressed below:

$$r_{ap} = \frac{6.7551}{u}. \quad (19)$$

The friction of the panicle-atmosphere surface could be weakened by the wind speed, and the transport of heat and water vapor between panicle and atmosphere was primarily attributed to molecular diffusion.

Since from August 5 to September 7, the plant height and PAD only had little difference, and the effect of the canopy structure was not considered for r_{ap} in this study.

TABLE 3: r_{ap} in the rice paddy field.

Date	Time	T_p (°C)	T_{ac1} (°C)	u (m s ⁻¹)	r_{ap} (s m ⁻¹)
August 5	8:30	26.8	27.8	0.4	18.1
August 7	8:30	26.8	28.4	0.6	10.9
August 18	8:30	26.3	26.9	0.6	10.9
August 26	9:30	26.1	27.6	1.7	6.2
August 28	8:30	24.7	25.1	0.6	12.4

Note: r_{ap} is the aerodynamic resistance to the transfer of sensible heat between panicle and atmosphere, T_p is the panicle temperature, T_{ac1} is the air temperature at the panicle's height, and u is the wind speed.

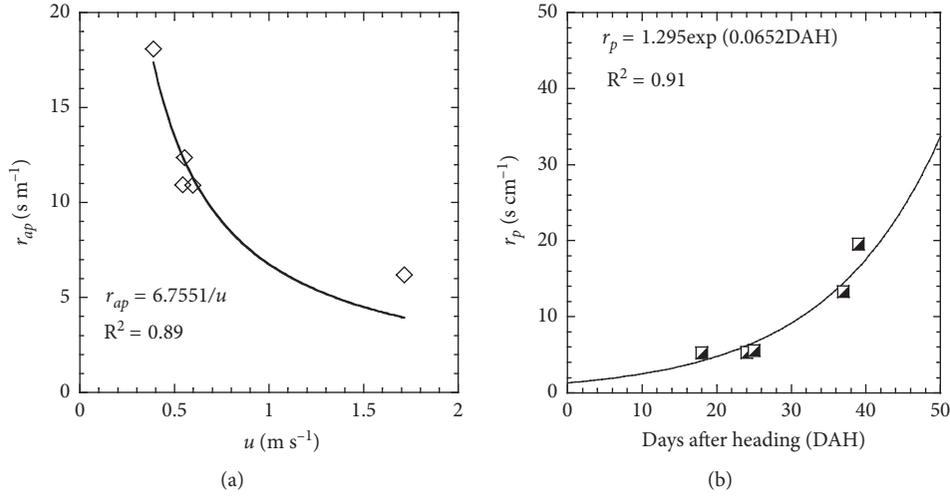


FIGURE 5: Relationship between wind speed (u) and aerodynamic resistance to the transfer of sensible heat between panicle and atmosphere (r_{ap}) in the rice paddy field on August 5, 7, 18, 26, and 28, 2014 (a). Change of panicle transpiration resistance (r_p) against the days after heading (DAH) in the rice paddy field on August 12, 18, 19, and 31 and September 2, 2014 (b).

3.3.3. Panicle Resistance for Transpiration (r_p). Based on the measured average T_p from 50 cm to 100 cm and r_{ap} calculated by Eq. (19), r_p can be calculated by equations (16a) and (16b). Five days under large S_v , high T_a and low RH conditions meaning strong transpiration (August 12, 18, 19, and 31 and September 2) were selected to analyze the influence of r_p (Table 4).

Correlations between days after heading (DAH), meteorological conditions (S_v , T_a , u , and RH), and r_p suggest that DAH was the major influencing factor, with the correlation coefficient of 0.92. Besides, the changes of r_p against the DAH in the rice paddy field are shown in Figure 5(b). r_p increased asymptotically with the rise in DAH, and their relationship was expressed as follows:

$$r_p = 1.295 \exp(0.0652 \text{ DAH}). \quad (20)$$

Thus far, though there was rare information about r_p , few researchers have measured the transpirational conductance g_p ($=1/r_p$) in rice paddy fields. Our results showed a similar variation but smaller values compared with those of cultivar ‘‘Wuxiangjing 9’’ reported by Oue et al. [29], in which g_p decreased with the increase in DAH from 0 to 9 under both ambient CO₂ and free air CO₂ enrichment condition.

This new useful method was presented in this study to denote r_p as a parameter by DAH, while some other methods

were reported. In the integrated micrometeorology model for panicle and canopy temperature (IM²PACT) developed by Yoshimoto et al. [30], g_p denotes the parameter of the relative humidity in the vicinity of panicle (RH_{ac}), which was not easily and accurately measured with the ordinary ventilated psychrometers. Based on the measurements of rice varieties at the time of flowering, Fukuoka et al. [39] presented three regression equations of g_p as a function of vapor pressure deficit (VPD).

3.4. Modeling T_p . The differences between T_{c1} and T_{c2} were presented by Wang et al. [40]. The average values of measured canopy temperature from 50 cm to 100 cm and from 10 cm to 40 cm were set as the measured T_{c1} and T_{c2} , which were then compared with the modelled ones, as shown in Figures 6(a) and 6(b). The root mean square errors (RMSE) of modelled T_{c1} and T_{c2} were 0.76°C and 0.75°C. Besides, the difference between modelled and measured T_{c1} and T_{c2} ranged from -1.69°C to 1.35°C and from -1.50°C to 1.61°C, respectively. According to results of the 2-tailed t -test statistical analysis, the modelled T_{c1} and T_{c2} values were not significantly different from the measured values at the 0.05 probability level.

In this study, we set $T_c = (T_{c1} \times a_1 + T_{c2} \times a_2) / (a_1 + a_2)$, and measured T_c was compared with that estimated by the two-layer model developed by Yan and Oue [38], as

TABLE 4: r_p in the rice paddy field.

Date	Time	DAH	S_t (W m^{-2})	T_a ($^{\circ}\text{C}$)	u (m s^{-1})	RH (%)	r_p (s m^{-1})
August 12	14:30	18	773	29	1.4	70	5.3
August 18	11:10	24	662	31	1.2	68	5.4
August 19	10:30	25	748	33	1.6	60	5.6
August 31	13:00	37	711	29	1.4	65	13.3
September 2	11:30	39	761	29	1.1	67	19.6

Note: DAH is days after heading, S_t is solar radiation, T_a is the air temperature, RH is the relative humidity, u is the wind speed, and r_p is the panicle transpiration resistance.

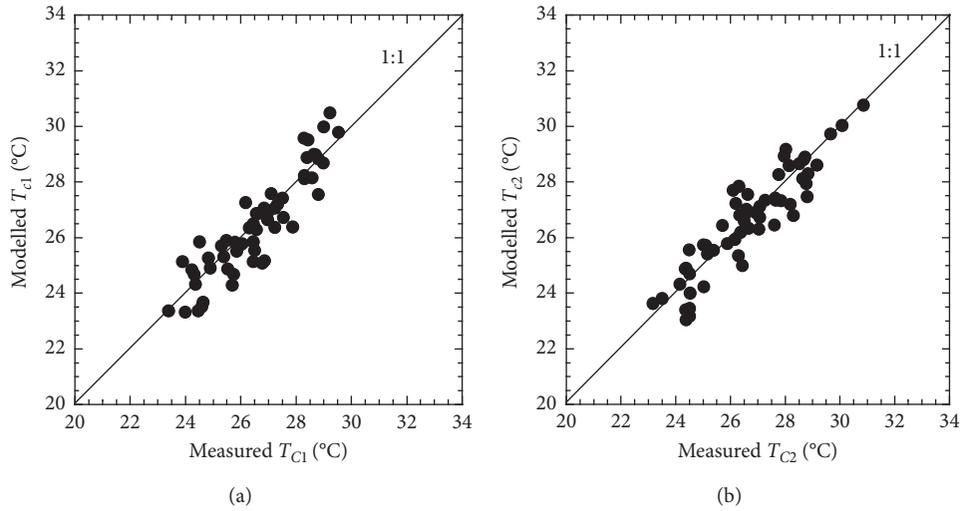


FIGURE 6: Comparisons between the measured and modelled upper layer canopy temperature (T_{c1}) (a) and lower layer canopy temperature (T_{c2}) (b) in the rice paddy field from August 5 to September 7, 2014.

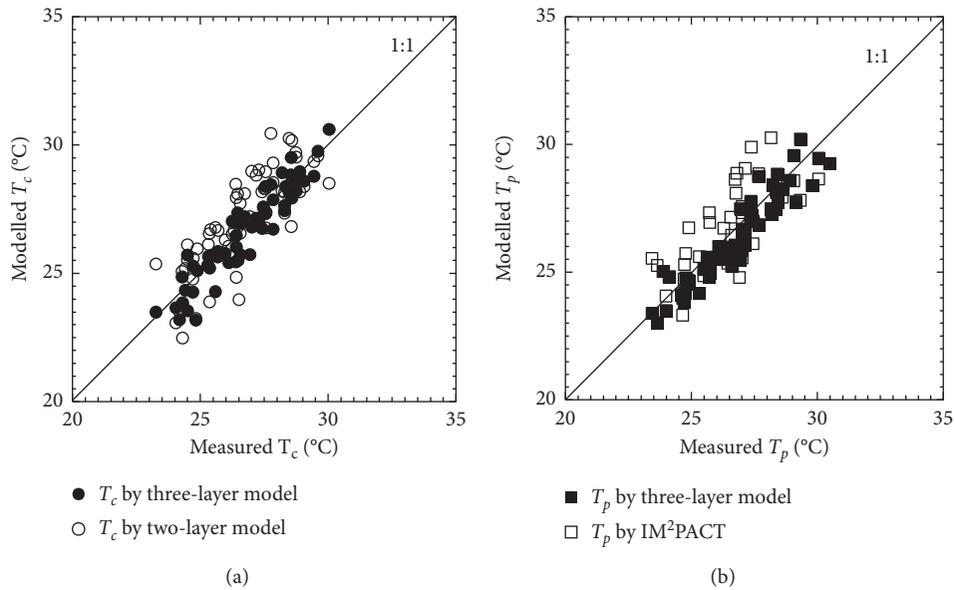


FIGURE 7: Comparison of T_c by the three-layer model and the two-layer model (a) and T_p by the three-layer model and IM²PACT (b) in the rice paddy field from August 5 to September 7, 2014.

shown in Figure 7(a). RMSE of T_c by our three-layer model was 0.63°C , smaller than that by the two-layer model (1.21°C).

As shown in Figure 7(b), RMSE of T_p estimated by the three-layer model was 0.81°C , smaller than that estimated by IM²PACT (1.27°C) including the two-layer model. Better

TABLE 5: T_p estimated by three-layer model and by IM²PACT [30].

Date	Time	S_t ($W\ m^{-2}$)	T_a ($^{\circ}C$)	RH (%)	T_c ($^{\circ}C$)	T_{c1} ($^{\circ}C$)	T_p by IM ² PACT ($^{\circ}C$)	T_p by three-layer model ($^{\circ}C$)	Mea T_p ($^{\circ}C$)
August 5	9:00	212	28	80	26.7	26.2	28.9	26.6	26.8
August 5	14:00	201	30	71	28.1	26.9	27.6	26.9	27.0
August 11	11:00	671	27	73	28.9	25.5	27.0	25.2	25.7
August 18	9:00	235	27	84	26.3	25.8	26.7	26.2	26.3
August 18	12:00	599	31	68	26.8	29.5	27.4	28.4	28.4
August 18	15:00	485	32	68	28.5	26.7	29.7	28.8	28.7
August 19	9:00	477	32	66	28.2	26.1	29.8	28.5	28.9
August 19	14:00	745	32	66	28.5	30.5	28.6	29.6	30.1
August 19	16:00	541	33	59	28.5	28.9	28.5	29.3	29.1
August 20	17:00	188	29	77	28.3	26.4	28.9	27.8	27.7
August 20	18:00	80	29	78	27.7	25.1	27.2	26.5	26.6
August 26	12:00	474	29	67	27.6	26.5	25.7	27.4	27.0
August 26	15:00	442	30	69	28.2	26.4	30.3	27.5	28.1
September 3	15:00	86	29	70	27.2	25.2	29.1	26.5	27.1
September 6	10:00	474	29	71	26.7	24.9	28.1	25.7	26.7
September 6	16:00	93	28	76	29.3	28.8	27.8	30.1	29.3

Note: Mea means measured.

TABLE 6: Error analysis statistics of the comparison between measured and calculated canopy and panicle temperatures by models.

Temperature	RMSE ($^{\circ}C$)	MAE ($^{\circ}C$)	SD ($^{\circ}C$)
T_c estimated by three-layer model	0.73	0.81	0.64
T_c estimated by two-layer model	1.21	1.56	1.25
T_{c1} estimated by three-layer model	0.76	0.75	0.74
T_{c2} estimated by three-layer model	0.75	0.63	0.98
T_p estimated by three-layer model	0.81	0.7	0.67
T_p estimated by IM ² PACT	1.27	0.95	0.76

Note: T_c is the canopy temperature ($^{\circ}C$); two-layer model is developed by Yan and Oue [38]; T_{c1} and T_{c2} are the upper and lower layer canopy temperatures, respectively; T_p is the panicle temperature ($^{\circ}C$); IM²PACT is integrated micrometeorology model for panicle and canopy temperature developed by Yoshimoto et al. [30]; RMSE is the root mean square error, MAE is the mean absolute error, and SD is the standard deviation.

agreements between the measured and modelled T_p by the three-layer model than that by IM²PACT were obtained, particularly under high T_a conditions as shown in Table 5. This was because (1) T_{c1} instead of T_c was used to predict T_p , since modelled T_{c1} could be $3^{\circ}C$ different with modelled T_c ; (2) F_1 , F_2 , and F_p were determined by fitting the calculated TDSR to the measured TDSR, F_1 , F_2 , and F_p varied with time because of the different solar radiation altitudes: rather than set to be constant; and (3) r_p denotes the parameter of measured T_p by DAH which considering transpiration cooling instead of the RH_{ac} .

RMSE of T_p estimated by the three-layer model for rice (cultivar Hinohikari) was $0.93^{\circ}C$, and RMSE of T_p estimated by the three-layer model for rice (cultivar Hinohikari) was $0.89^{\circ}C$. Error analysis statistics of the comparison between measured and calculated canopy and panicle temperatures by models is shown in Table 6.

4. Conclusions

Rice panicle temperature (T_p) is a key factor for studying high temperature impacts on spikelet sterility. Comparing with measuring T_p by hand, a T_p simulation model could obtain T_p data readily. We developed the three-layer model to estimate T_p and compared the performance to estimate T_c by three-layer model and T_c by two-layer model developed

by Yan and Oue [38]; and to compare the performance to estimate T_p by three-layer model and T_p by IM²PACT [30]. RMSE of T_c by our three-layer model was $0.63^{\circ}C$, smaller than that by the two-layer model ($1.21^{\circ}C$). RMSE of T_p estimated by the three-layer model was $0.81^{\circ}C$, smaller than that estimated by IM²PACT ($1.27^{\circ}C$).

However, from July 9 to September 8, 2014, there was 29 rainy days, on which T_{c1} , T_{c2} , and T_p measurement could not be performed, thereby leading to the reduction of measured data. The highest T_a was $34.64^{\circ}C$ on July 26, 2014, and T_{c1} and T_p higher than $35.0^{\circ}C$ could not be observed, so our model was not used for extreme temperature. Furthermore, the three-layer model simulated fairly well the T_{c1} , T_{c2} , and T_p with root mean square errors of $0.76^{\circ}C$, $0.75^{\circ}C$, and $0.81^{\circ}C$, and it was validated well by two other rice cultivars, and thus, it demonstrated that the three-layer model was a new feasible way to estimate T_p . In the future, we will measure stomatal resistance (g_s) in the rice paddy field and analyze the microclimate observational results in the elevated carbon dioxide concentration experiments [41] with different land use [42] to predict T_p .

Data Availability

The data used to support the findings of this study are available from the corresponding author upon request.

Disclosure

Hiroki Oue and Zhijun Luo are the co-first authors.

Conflicts of Interest

The authors declare that they have no conflicts of interest.

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