

Research Article

Preparation and Characterization of Chitosan/Bentonite Composites for Cr (VI) Removal from Aqueous Solutions

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Chitosan/bentonite composites (CSBT) prepared by physical gelation were tested for the adsorption of Cr (VI) from aqueous solutions in this work. The composites were prepared at a mass ratio from 2 : 1 to 1 : 2, and a composite of 1 : 1 was found to be most suitable for efficient Cr (VI) removal. The influencing parameters, including temperature, adsorbent dose, and pH, were statistically optimized using response surface methodology (RSM) for the removal of Cr (VI). The pH was found to be the limiting factor during the adsorption process, and under the optimal conditions, namely, adsorbent dose of 400 mg/L, pH = 3, and temperature of 298 K, 87.61% Cr (VI) would be removed expectantly. The mechanism of Cr (VI) removal by CSBT was discussed, and the protonation of amino groups on chitosan followed by the combination of $-NH_3^+$ and anionic hexavalent chromium was the primary driving force. In addition, the removal of Cr (VI) onto CSBT was monolayer adsorption with a maximum adsorption capacity of 133.85 mg/g by the Langmuir isotherm. CSBT follows a pseudosecond-order kinetic model, and within 1.5 h, adsorption was observed to reach equilibrium. The calculated thermodynamic functions clarified that the adsorption process was exothermic and spontaneous below 312.60 K. CSBT could be regenerated after desorption by 0.5 mol/L NaOH solutions and exhibited superior reusability after six cycles. This study demonstrated composites of chitosan/bentonite as eco-friendly bioadsorbents for the removal of Cr (VI) from aqueous environments.

1. Introduction

Heavy metals are critical contaminants that are harmful or carcinogenic to human health and pose a hazardous threat to the ecological environment. Chromium is a heavy metal that is widely used in industry and has two valence states, Cr (III) and Cr (VI). Trivalent chromium is less toxic and considered to be an important element for plants and animals, as it has a high value for sugar and lipid metabolism [1, 2]. Cr (VI) can cause arthritis and barrier disruption in contacts with the skin [3, 4] and nasal septum perforation in severe contact with the respiratory tract [5, 6]. Large amounts of ingestion of Cr (VI) can cause liver enlargement, circulatory failure, and even death [7]. Almost all chromium ore is processed through hexavalent chromium, which is used in anticorrosion, metal protection, paints, and dyes, so industrial wastewater has become the main source of hexavalent chromium pollution [8–10]. Due to

the high toxicity of Cr (VI), wastewater must be treated to reduce the harm of hexavalent chromium. Ion exchange, chemical precipitation, bioremediation, electrolysis, and membrane separation [11–15] are often used in heavy metal removal in aqueous environments. These treatment methods have limited applications because they are not effective for hexavalent chromium wastewater with a lower concentration of less than 100 mg/L, and the treatment cost is too high. Adsorption is easy and inexpensive to remove heavy metals in wastewater effectively; thus, it may be superior to other chromium wastewater treatment methods [16–19].

Natural polymer materials have attracted increasing attention as adsorbents due to their biodegradability and lower toxicity [20]. Chitosan (Chi) is a polysaccharide obtained from the deacetylation of chitin, which has rich functional groups and is widely used as an adsorbent to remove heavy metal ions [21, 22]. The large number of

amino groups in Chi structure can be protonated in an acid solution and then adsorb anionic compounds [23]. The amino groups and hydroxyl groups of Chi allow various chemical or physical modifications to expand its applications. By hydrogen bonding, hydrophobic interaction, or covalent bonding, chitosan molecules can relate to each other to form physical or chemical gels [24–26]. However, chitosan physical hydrogels prepared by dissolving in acid solution and then sinking into alkali solutions always cause the degradation of chitosan macromolecule chains, leading to a decrease in the mechanical strength of chitosan hydrogels. To overcome this shortcoming, several methods have been used to enhance their mechanical strength, such as nanofiller reinforcement and blending with other polymers. To overcome this shortcoming, bentonite was introduced into chitosan. Bentonites have a layered structure with exchangeable cations between the space and have a certain dispersibility, chargeability, and hydration in aqueous solution. It is helpful to prepare mechanically stable enhanced physical crosslinking hydrogels by dropping chitosan/clay suspensions into sodium hydroxide solution. Huang et al. [27] prepared a chitosan composite hydrogel, and the viscosity of the composite solution increased with clay mineral content. The mechanical properties and antideformation ability of the composite hydrogel significantly increased owing to the reinforcing effect of clay minerals. The compressive strength of pure chitosan hydrogel was 0.14 MPa, and the compressive strength was significantly increased to 0.71 MPa after adding clay minerals.

The intercalation and adsorption of chitosan on bentonite provide more adsorption sites for the composite, making the adsorption performance of the composite for heavy metals significantly better than montmorillonite [28]. These characteristics make the chitosan/bentonite composite a kind of heavy metal adsorption material with broad development prospects. Zhang et al. [29] combined chitosan and bentonite to prepare composite materials for Sc (III) removal. The results showed that the chitosan/bentonite composite had excellent adsorption performance, and the heavy metals could not only electrostatically complex with carboxyl and hydroxyl groups but also chelate with amino, azo, and pyridine groups. Cheng et al. [30] used chitosan to load iron-aluminium bimetallic particles onto bentonite and found that the iron-aluminium bimetal was surrounded by chitosan and bentonite, which can effectively solve the problem of secondary pollution of nanometal particles. Due to the excellent synergy between chitosan, bentonite, and bimetal, the removal effect of composite materials on inorganic salts is effectively improved compared with that of a single material.

The purpose of this study was to synthesize chitosan/bentonite composites to effectively remove hexavalent chromium from wastewater. The optimal preparation conditions were determined, and the conditions for removing hexavalent chromium were optimized by responsive surface methodology. To understand the removal mechanism, studies and comparisons of adsorption isotherms, adsorption thermodynamics, and kinetic models were performed. The reusability of composite materials has also been studied.

2. Materials and Methods

2.1. Preparation of Chitosan/Bentonite Composites (CSBT). Chitosan (DA \geq 95%) and bentonite (BT) were purchased from Shanghai Macklin Biochemical Co., Ltd., China. All analytical solutions were prepared by the utilization of deionized water.

A pillared process was needed to improve the interaction of bentonite with chitosan [30]. The preparation of Fe/Al pillared bentonite was carried out following the treatment of bentonite by hydroxyl-Fe and hydroxyl-Al. Hydroxyl-Fe with a final OH/Fe mole ratio of 2.0 pillared solution was prepared after 2 hours of mixing of ferric nitrate and sodium carbonate. A mixture of 0.5 mol/L aluminium chloride and 1 mol/L sodium carbonate was used to produce a hydroxyl-Al pillared solution with a final OH/Al mole ratio of 2.4. These solutions were used after 24 h ageing at 333 K. Under constant stirring, hydroxyl-Fe and hydroxyl-Al pillared solutions were added at a ratio of 0.05 to the bentonite suspension. The resulting suspension was then stirred for 2 hours at room temperature. Then, after being washed several times with distilled water, dried at 378 K and then ground, an Fe:Al:bentonite ratio of 0.5:10:1 pillared bentonite (ABT) was obtained.

Chitosan was dissolved in acetic acid (2%) with stirring overnight at room temperature (298 ± 2 K). Then, a certain amount of pillared bentonite was added. After 2 hours of stirring, the suspension was poured into 0.5 mol/L NaOH to prepare the physical gel. Sufficient agitation was needed to prevent the product from sticking. Finally, the products were washed with distilled water to neutral pH, dried at 333 K, and ground to obtain the chitosan-bentonite composite.

2.2. Characterization of CSBT. Different analyses were conducted to characterize CSBT, such as Fourier transform infrared (FT-IR) spectroscopy, X-ray power diffraction (XRD), and scanning electron microscopy (SEM). Specifically, a D8 ADVANCE (Bruker, Germany) X-ray diffractometer was used to obtain XRD patterns with Cu/K α radiation wavelengths of 1.54056 nm and angles of 5°–40° at room temperature. A Fourier transform infrared spectrophotometer (Nicolet IS10) Thermo Nicolet, USA, was used to analyse functional groups with 400–4000 cm⁻¹ wavelength ranges of single beam optics. A HITACHI scanning electron microscope (SU8020), Japan, was used to analyse the surface morphology.

2.3. Selection of CSBT Based on Cr (VI) Removal. Various concentrations of K₂Cr₂O₇ solutions were obtained by diluting the chromium standard solution (1000 mg/L, TMRM China).

CSBT synthesized at different chitosan/bentonite ratios was tested to select the best adsorbents with the maximum removal percentage. CSBT (20 mg) was added to 50 mL of potassium dichromate, in which the Cr (VI) concentration was 10 mg/L, in a 100 mL conical flask and agitated in a magnetic stirrer at 180 rpm for 1.5 h at room temperature (298 ± 2 K). Thereafter, the solutions were filtered, and the

filtrates were analysed by a UV-vis spectrophotometer (Beijing Purkinje, China) to determine the concentration of Cr (VI) ions with the 1, 5-diphenyl carbazide method at 540 nm. The sorption capacity and removal percentage were calculated with Equations (1) and (2), respectively. All experiments were performed in triplicate, and average values are reported.

$$q_e = \frac{(C_0 - C_e) \cdot V}{m}, \quad (1)$$

$$R(\%) = \frac{C_0 - C_e}{C_0}, \quad (2)$$

where C_0 is the initial Cr (VI) concentration (mg/L), C_e is the Cr (VI) equilibrium concentration (mg/L), V is the volume (L) of Cr (VI) solutions, and m is the mass of CSBT.

2.4. Optimization of Cr (VI) Removal Process. Temperature, initial pH, and adsorbent dose were the main factors affecting the removal efficiency of Cr (VI). Adsorption experiments were performed at different temperatures (288-318 K), different initial pH values (ranging from 2.5 to 9), and different doses of adsorbent (100-1000 mg/L) to analyse the independent effect of these factors on Cr (VI) removal. HCl (0.1 mol/L) and NaOH (0.1 mol/L) were used to adjust the pH of the chromium solution.

A response surface methodology- (RSM-) based Box-Behnken design was used for further optimization of the Cr (VI) removal process. The variable input parameters used were as follows: temperature, 288-308 K; dose of CSBT, 200-600 mg/L; pH, 2.3-5.5; and factor level codes, -1 (low), 0 (medium), and 1 (high). The three independent variables used for statistical calculations were designed as X_1 (temperature), X_2 (dose of CSBT), and X_3 (pH). The selected ranges and levels of the three variables are listed in Table 1. The results were analysed using a coefficient of determination (R^2) to investigate the model fitness, and the significance of each independent variable was determined using Fisher's test for analysis of variance (ANOVA) at $P < 0.05$. A three-dimensional response surface map was drawn to identify interactions or multifactor effects between response factors.

2.5. Adsorption Isotherm. Adsorption isotherm experiments were carried out at 288, 298, and 308 K, a pH of 3, and 20 mg of adsorbent, and the initial concentrations of Cr (VI) ranged from 5-500 mg/L. The experimental data were analysed with Langmuir, Freundlich, Temkin, and Dubinin-Radushkevich (D-R) isotherm models (Equations (3) and (4)).

$$\frac{C_e}{Q_e} = \frac{1}{Q_m \cdot K_L} + \frac{C_e}{Q_m}, \quad (3)$$

$$\ln Q_e = \ln K_F + \frac{1}{n} \ln C_e, \quad (4)$$

$$Q_e = B \ln A + B \ln A, \quad (5)$$

$$\ln Q_e = \ln Q_e - b \cdot \Sigma^2, \quad (6)$$

TABLE 1: Factors and values of Box-Behnken design.

		Temperature (K)	Adsorbent dose (mg/L)	pH
X_1	-1	288	200	2.5
X_2	0	298	400	3
X_3	1	308	600	3.5

TABLE 2: Removal percentages of different CS/BT ratios.

#	Ratio of chi mass	Ratio of BT mass	Removal percentage (%)
1	2%	1%	80.07%
2	1%	1%	88.84%
3	0.5%	1%	86.68%
4	1%	2%	81.74%
5	1%	0.5%	72.71%

where C_e is the equilibrium Cr (VI) concentration (mg/L), Q_e is the equilibrium adsorption capacity (mg/g), Q_m is the maximum adsorption capacity of CSBT, K_L is the Langmuir affinity constant (L/mg), K_F is the Freundlich constant (mg/g) relating to the adsorption affinity, n is the Freundlich equation exponent relating to the heterogeneity of the adsorbent surface, A and B are Temkin constants, b is the adsorption energy, and Σ is the Polanyi potential energy.

2.6. Adsorption Kinetics. After different agitation times, the removal percentage of Cr (VI) by CSBT was measured, and pseudofirst-order and pseudosecond-order kinetic models (Equations (5) and (6)) were fitted to investigate the adsorption mechanism.

$$\ln(Q_e - Q_t) = \ln Q_e - K_1 \cdot t, \quad (7)$$

$$\frac{t}{Q_t} = \frac{1}{K_2 \cdot Q_e^2} + \frac{t}{Q_e}, \quad (8)$$

where Q_t is the adsorption capacity at time t (mg/g), and k_1 (min^{-1}) and k_2 ($\text{mg}^{-1} \cdot \text{min}^{-1}$) are the rate constants of first- and second-order kinetics, respectively.

2.7. Reusability of CSBT. NaOH (0.1 mol/L) was used to desorb the Cr (VI) adsorbed. NaOH (50 mL) was added to the adsorbents in a 100 mL conical flask and agitated in a magnetic stirrer at 180 rpm for 1.5 h at room temperature (298 ± 2 K) to desorb the adsorbed Cr (VI). After desorption, the CSBT was reused to adsorb Cr (VI) again. The desorption Cr (VI) concentration and readsorbed Cr (VI) concentration were analysed to investigate the reusability of CSBT.

3. Results and Discussions

3.1. Effect of Different Chitosan/Bentonite Ratios on Cr (VI) Removal. By fixing the mass of chitosan or AlBT and changing the mass of the other, the effect of different mass ratios on Cr (VI) removal was studied, and the results are shown in Table 2. When the mass ratio of both chitosan and AlBT

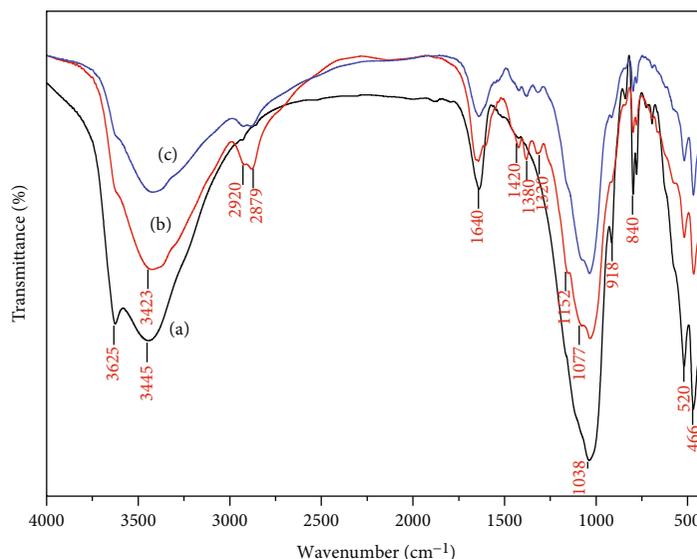


FIGURE 1: FTIR spectra of AIBT (a), CSBT (b), and CSBT after Cr (VI) removal (c).

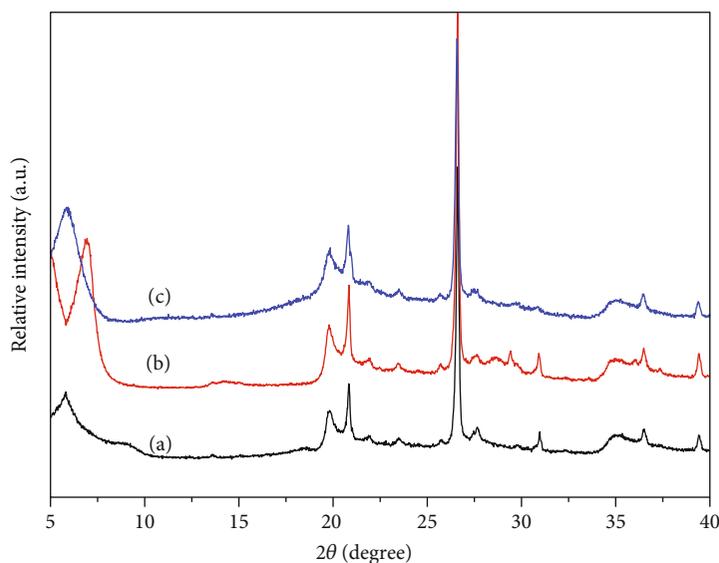


FIGURE 2: X-ray diffraction spectra of bentonite (a), AIBT (b), and CSBT (c).

was 1%, the adsorption removal of Cr (VI) was the most effective. The higher the proportion of chitosan was, the larger and harder the beads formed in the sodium hydroxide solution, and the volume shrank and led to the collapse of the structure after drying due to surface tension [31]. If the proportion was lower than 1%, the NaOH solution hindered the gelation process by diluting the chitosan solution and led to the formation of a precipitate [32]. The number of amino and hydroxyl groups as sorption sites would decrease, and the adsorption efficiency would decrease as well. Taking these factors into account, the adsorption efficiency was the best when both the mass ratio of chitosan and bentonite were 1%, and it was suitable as a Cr (VI) adsorbent. Next, the adsorption performance of CSBT with a mass ratio of chitosan and bentonite of 1% for Cr (VI) was systematically studied.

3.2. Characterization of CSBT

3.2.1. Fourier Transform Infrared (FTIR) Spectroscopy. The FTIR spectra of AIBT, CSBT, and ACSBT are shown in Figure 1. The characteristic absorption band of bentonite at 1038 cm^{-1} (asymmetrical bond stretching vibration of Si-O-Si) appeared in the curve of CSBT [33], indicating that the silicate layer structure of bentonite was not destroyed after the reaction of chitosan and AIBT. In CSBT, the absorption bands at 3625 cm^{-1} (hydrogen stretching vibration peak) in the curve of AIBT disappeared, the other hydroxyl-related absorption bands (3445 cm^{-1} of interlayer hydroxyl stretching vibration peak [34], 918 cm^{-1} of Al-OH bending vibration peak, and 840 cm^{-1} of Al-Mg-OH bending vibration peak) were also attenuated or shifted, and the characteristic absorption band of chitosan corresponding to NH_2

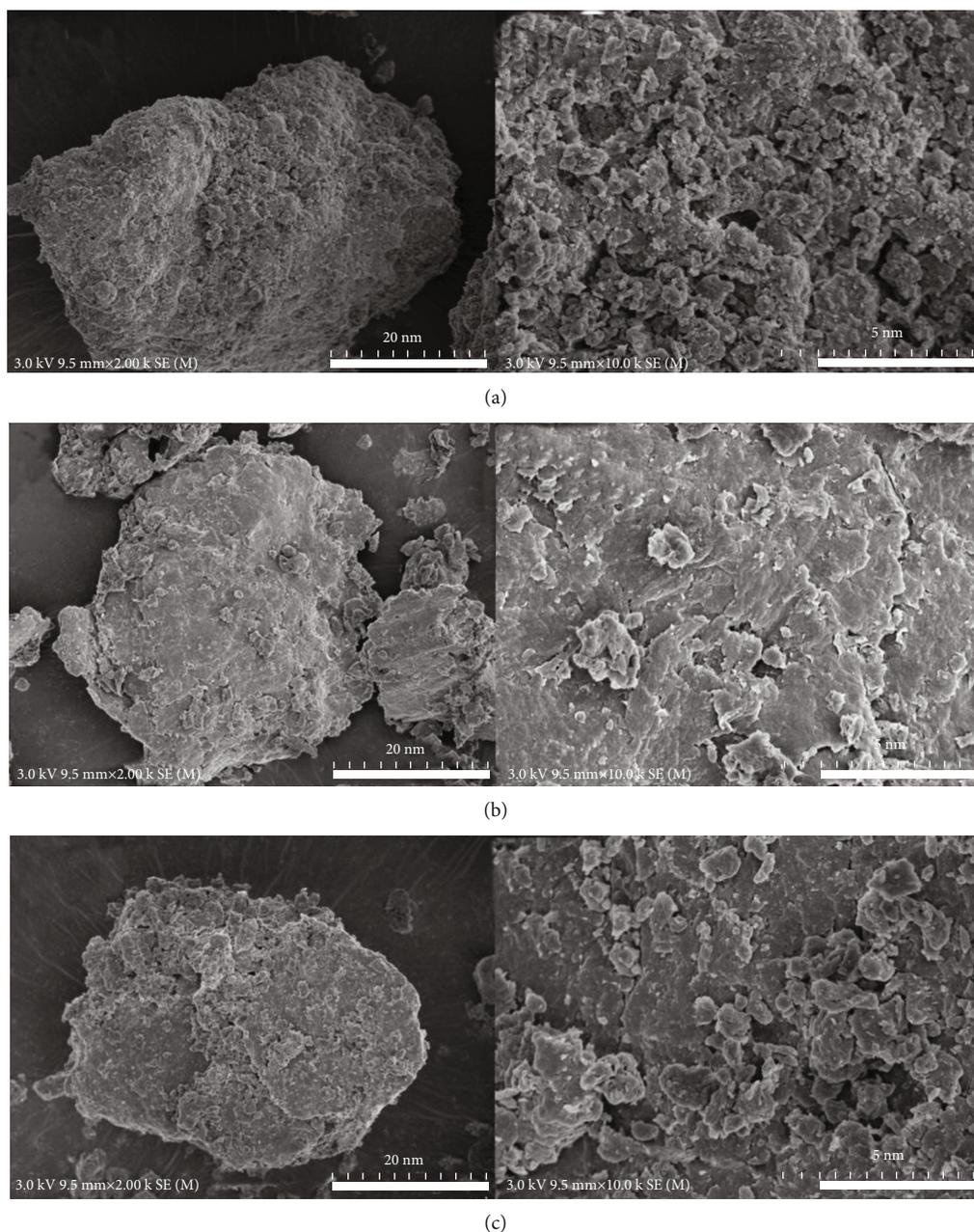


FIGURE 3: SEM images of AlBT (a), CSBT (b), and CSBT after Cr (VI) removal (c).

vibration at 1601 cm^{-1} disappeared [35], which shows that the hydroxyl groups on bentonite reacted with amino groups on chitosan.

After Cr (VI) adsorption, the characteristic bands at 3445 , 1640 , 1420 , 1152 , and 1038 cm^{-1} , which are related to NH vibrations, CN stretching, and OH vibrations, were attenuated [36]. These results agreed with former reports that -NH_2 groups are the main reaction sites adsorbing hexavalent chromium [37].

3.2.2. X-Ray Diffraction (XRD) Spectra. XRD spectra of BT, AlBT, and CSBT were given in Figure 2. The XRD results revealed that the main composites of BT, AlBT, and CSBT are montmorillonite. Compared with bentonite, no new dif-

fraction peak is added after pillaring. The only changes appeared at the $d(001)$ spacing, indicating that the pillaring process only had a significant effect on the $d(001)$ spacing. The value of the $d(001)$ spacing increased from 1.271 nm for the original bentonite to over 1.759 nm for AlBT. After combining with chitosan, the excessive interlayer distance of pillared bentonite decreased, and the value of $d001$ dropped to 1.488 nm , which may be due to the formation of hydrogen bonds between chitosan and bentonite interlayer hydroxyl groups, confirming the synthesis of chitosan/bentonite composites.

3.2.3. Scanning Electron Microscopy. As shown in Figure 3, the pillared bentonite montmorillonite particles maintained

a layered structure, but the surface split, forming many small layered particles, which were aggregated with each other forming irregular pores. After the addition of chitosan, the cluster property of the pillared bentonite was improved, the particles became larger, the surface became smooth, and the edges were more obvious, indicating that part of the chitosan was successfully inserted between the layers. After adsorbing Cr (VI), from a macroscopic perspective, the colour of CSBT was yellow–green, which is the colour of Cr (VI). After drying, the colour of CSBT was similar to that of soil, and the texture became loose. Corresponding to the SEM image, the number of surface particles increased, and the composites split again.

During the adsorption process, the amino groups were protonated by hydrogen ions in acidic solutions following the breakage of hydrogen bonds between amino and hydroxyl groups, which weakened the combination of chitosan and the bentonite silicate layer. Then, hexavalent chromium ions entered the interlayer and combined with -NH_3^+ , so the silicate layer split again, resulting in a decrease in the cluster property of CSBT after drying.

3.3. Optimization of Cr (VI) Removal Process. To investigate the optimal Cr (VI) removal conditions, 17 runs for a three-parameter Box-Behnken experimental design were performed. The experimental data are given in Table 3, and a polynomial equation was determined for the removal percentage.

$$Y = 87.61 - 4.95X_1 + 8.66X_2 + 12.46X_3 + 0.74X_1X_2 - 1.15X_1X_3 + 0.40X_2X_3 - 0.73X_1^2 - 6.77X_2^2 - 35.64X_3^2 \quad (9)$$

In Equation (8), a negative value indicates that this factor has an antagonistic effect, and a positive value indicates that there is a synergistic effect [38]. The value of adsorbent dose and pH is positive, indicating that increasing these values contributes to increasing removal percentages. The negative value of temperature indicates that the temperature increment is not conducive to the improvement of the removal percentage.

The F value and P value of ANOVA can evaluate the significance of influencing factors. The larger the F value and smaller the P value are, the more reliable the experimental data. In this experiment, the F value was 108.04, and the P value was less than 0.0001, indicating that the experimental data were reliable (Table 4). In addition, the P value of X_1 , X_2 , X_3 , X_2^2 , and X_3^2 are less than 0.05, which means that the influence of these factors cannot be ignored, and the interactive effect of any two factors is not significant on removal percentage [39]. The P value of “lack of fit” is 0.0525, and the correlation coefficient is 0.9929, revealing that the predictability of this model is reliable.

According to ANOVA, the effect of temperature and adsorbent dose on Cr (VI) removal by CSBT is significant. The corresponding three-dimensional response surface map of the removal percentage for these two factors is shown in Figure 4. In the experimental temperature range,

TABLE 3: Experimental design and its actual values.

#	Temperature X_1	Adsorbent dose X_2	pH X_3	Removal percentage (%)
1	1	0	1	57.1
2	-1	0	1	70.96
3	1	0	-1	33.83
4	0	-1	-1	27.06
5	0	1	1	64.16
6	0	-1	1	50.5
7	0	0	0	87.43
8	1	1	0	87.62
9	0	0	0	88.31
10	0	0	0	86.08
11	0	0	0	89.89
12	-1	1	0	94.39
13	0	0	0	86.36
14	-1	0	-1	43.07
15	1	-1	0	64.36
16	0	1	-1	39.11
17	-1	-1	0	74.09

(Initial concentration, 10 mg/L; contact time, 90 min; rpm, 180).

the response surface increased significantly with increasing dose, and a high removal rate was always maintained in the high dose area (400–600 mg/g), which was not affected by the temperature. Compared with the influence of the dose, the change in the response surface is not obviously affected by the temperature. If the temperature is constant, the removal percentage increases with increasing adsorbent dose, which is attributed to the increase in the number of -NH_2 , and there are more sites reacting with Cr (VI). However, when the adsorbent dose is constant, an increase in temperature will cause a decrease in the removal percentage.

According to the above data, the optimal conditions for removing Cr (VI) are pH = 3, temperature 298 K, and adsorbent dose of 400 mg/L. The predicted removal percentage is 87.61%, which is near agreement with the experimental maximum of 88.31%.

3.4. Effects of Influence Parameters on Cr (VI) Removal and Adsorption Capacity

3.4.1. pH. The pH value of potassium dichromate solution is one of the important factors affecting the adsorption process. Therefore, the influence of pH values ranging from 2.5 to 9.0 on the adsorption capacity of CSBT to Cr (VI) was studied. The adsorption capacity of AIBT was lower than that of CSBT, as shown in Figure 5. AIBT lacks the abundant functional groups in chitosan and mainly absorbs heavy metal cations in solution by cation exchange. Compared with CSBT, it has a weak ability to adsorb anionic Cr (VI). In contrast, the maximum adsorption capacity of CSBT appeared at pH = 3 (22.10 mg/g). When the pH value was greater than 3, the adsorption capacity began to decrease until it reached 0.12 mg/g at pH = 9.0. In ANOVA, pH had a significant linear and quadratic effect ($P < 0.0001$) on the

TABLE 4: ANOVA of responsive surface design.

Source	Sum of squares	df	Mean square	F value	P value Prob > F	
Model	7749.45	9	861.05	108.04	<0.0001	Significant
X_1	196.02	1	196.02	24.60	0.0016	
X_2	599.79	1	599.79	75.26	<0.0001	
X_3	1241.27	1	1241.27	155.75	<0.0001	
X_1X_2	2.19	1	2.19	0.27	0.6163	
X_1X_3	5.34	1	5.34	0.67	0.4402	
X_2X_3	0.65	1	0.65	0.081	0.7838	
X_1^2	2.26	1	2.26	0.28	0.6106	
X_2^2	192.74	1	192.74	24.18	0.0017	
X_3^2	5348.48	1	5348.48	671.10	<0.0001	
Residual	55.79	7	7.97			
Lack of fit	46.16	3	15.39	6.40	0.0525	Not significant
Pure error	9.62	4	2.41			
Cor total	7805.24	16				

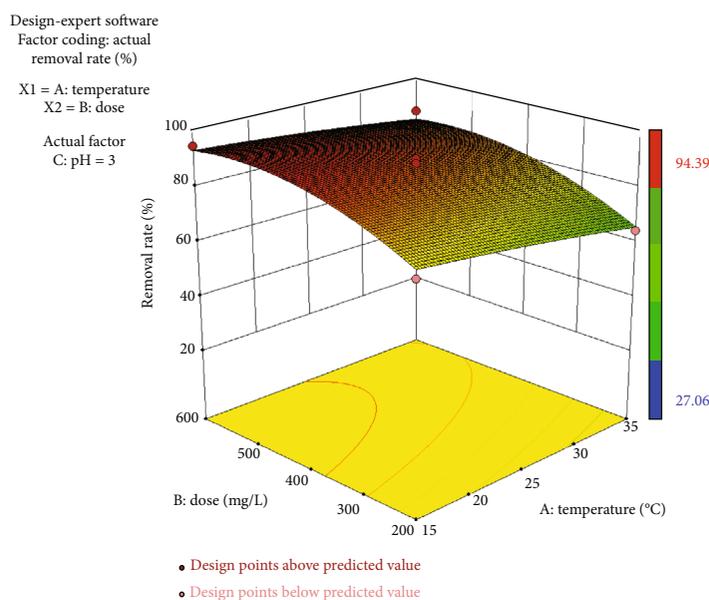


FIGURE 4: Responsive surface map of removal percentage for temperature and adsorbent dose.

removal percentage, meaning that pH was the limiting factor during Cr (VI) adsorption.

In the potassium dichromate solution, the existence form of Cr (VI) and the content of each form change with the change in pH value. At pH = 2.5 – 5, the main morphology is HCrO_4^- . In an acidic solution, $-\text{NH}_2$ in CSBT is protonated, and the positive charge is expected to combine with HCrO_4^- by electrostatic attraction. In addition, the ligand-exchange mechanism chelating with Fe (III) could be another driving force in Cr (VI) adsorption because of the presence of hydroxyl-Fe [40]. When the pH value was 2.5, part of the CSBT in the solution was dissolved, affect-

ing the adsorption process. When the pH was greater than 3, the solubility was not affected. Similar results have been reported in the literature. High-acidity solutions will increase the solubility of chitosan [41]. In solutions with a high initial concentration of molybdate, the removal effect was best at pH = 3.5, and at pH 5 or 6, the removal percentage was minimal. At near-neutral pH, the electrostatic balance between anionic and cationic groups on the polymer would be expected to be less favourable for Cr (VI) binding. As the pH increases, the increased hydroxide will also compete with Cr (VI) for adsorption, reducing the adsorption capacity [42]. When the solution is alkaline or the pH

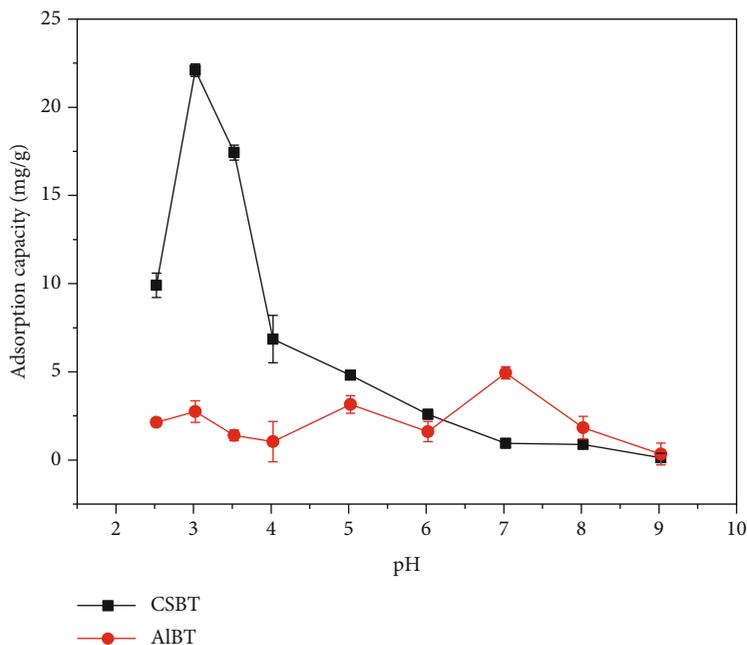


FIGURE 5: Effect of pH of Cr (VI) solutions on Cr (VI) removal by CSBT and AIBT. (absorbent dosaging, 400 mg/L; initial concentration, 10 mg/L; temperature, 298 K; contact time, 90 min; rpm, 180).

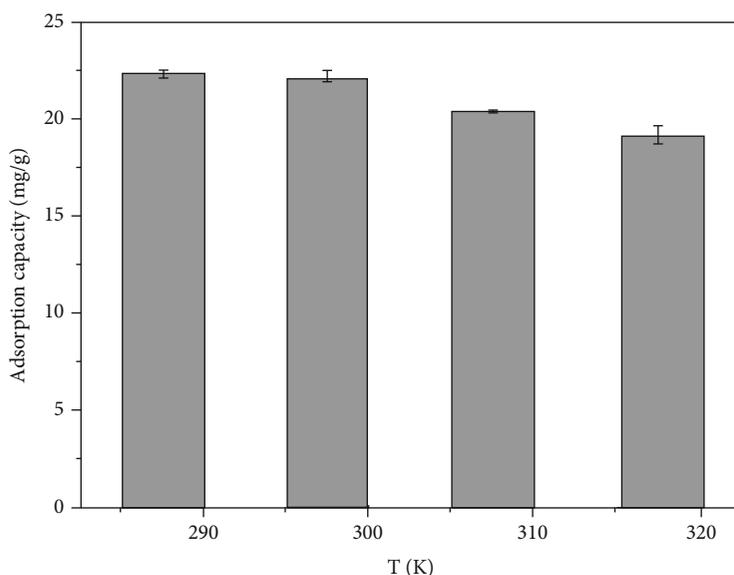


FIGURE 6: Effect of temperature on Cr (VI) removal of CSBT. (Absorbent dosaging, 400 mg/L; initial concentration, 10 mg/L; pH value, 3.0; contact time, 90 min; rpm, 180).

gradually increases, it will inhibit electrostatic adsorption, resulting in a low removal rate. Based on the above factors, to ensure the best adsorption of Cr (VI), the subsequent test pH was 3.

3.4.2. Temperature and Thermodynamics. Temperature is another important factor affecting the adsorption process. In this experiment, temperature had a significant negative effect on the Cr (VI) removal percentage ($P = 0.0016$). With increasing temperature, the removal percentage decreased (Figure 6). Adsorption can be divided into physical adsorp-

tion and chemical adsorption. Physical adsorption is fast, easily reaches equilibrium, and no activation energy is needed. Chemical adsorption is slow, has difficulty reaching equilibrium, and requires activation energy. The adsorption of Cr (VI) by CSBT was fast, and 63.51% of Cr (VI) was adsorbed within 5 minutes, indicating that at low temperature, the adsorption was physical. Since adsorption is exothermic, the adsorption capacity decreases with increasing temperature.

As most of the adsorption is performed at a lower temperature, adsorption thermodynamics were studied with

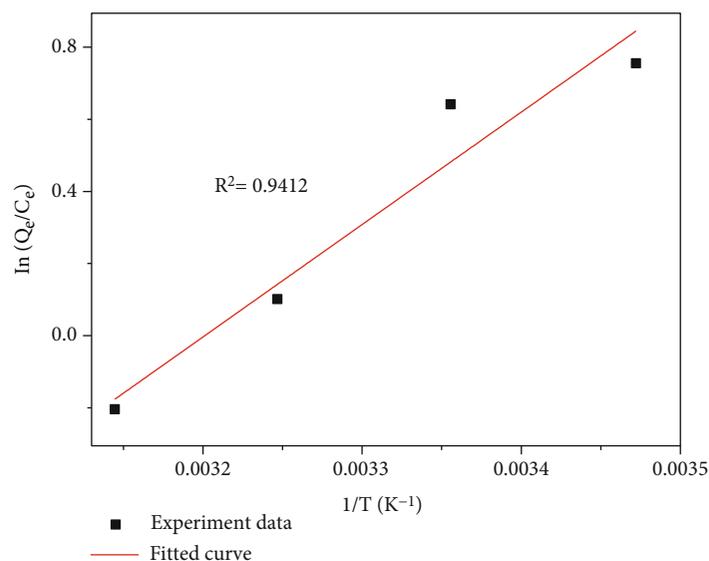


FIGURE 7: Thermodynamic adsorption for Cr (VI) removal on CSBT.

TABLE 5: Constants of adsorption thermodynamics for Cr (VI) of CSBT.

ΔH ($kJ \cdot mol^{-1}$)	ΔS ($J \cdot mol^{-1} \cdot K^{-1}$)	ΔG_{288K} ($kJ \cdot mol^{-1}$)	ΔG_{298K} ($kJ \cdot mol^{-1}$)	ΔG_{308K} ($kJ \cdot mol^{-1}$)	ΔG_{318K} ($kJ \cdot mol^{-1}$)
-25.93	-82.95	-2.04	-1.21	-0.38	0.45

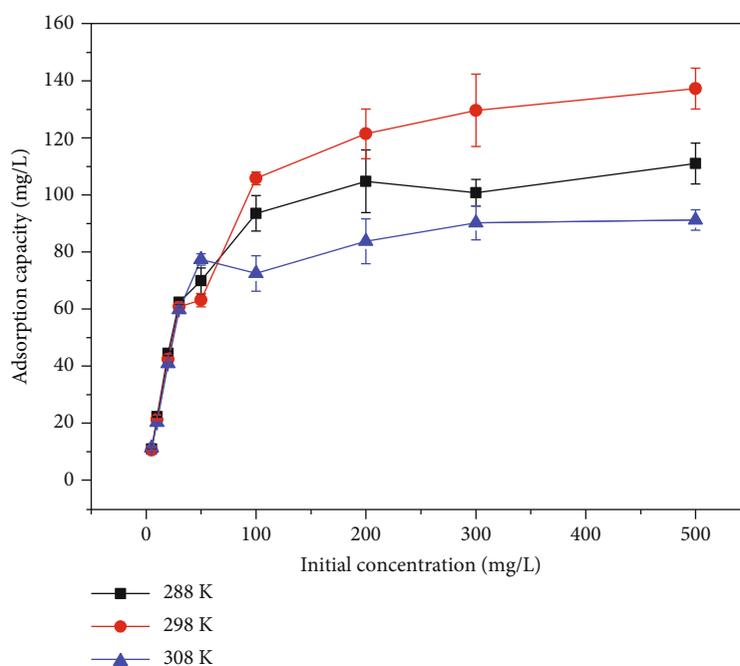


FIGURE 8: Effect of initial concentration of CSBT on Cr (VI) removal. (Absorbent dosaging, 400 mg/L; pH value, 3.0; contact time, 90 min; rpm, 180).

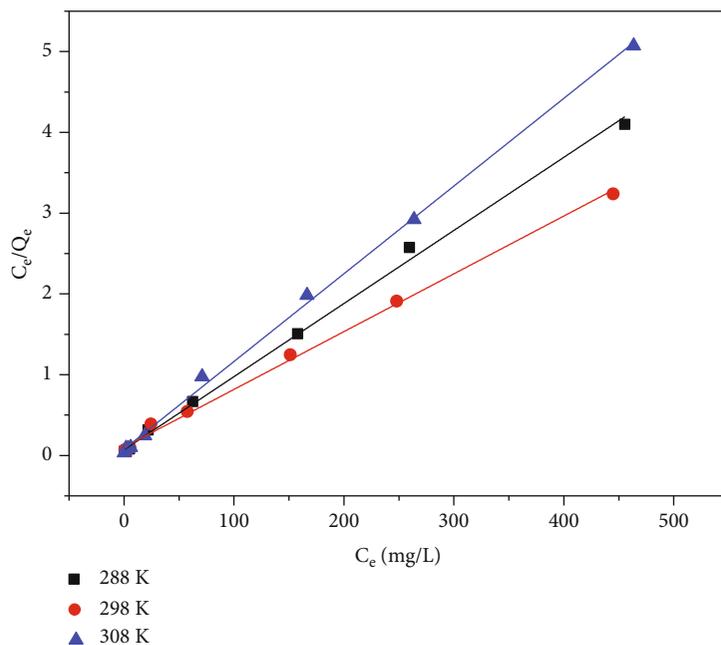


FIGURE 9: Langmuir isotherm for Cr (VI) removal on CSBT.

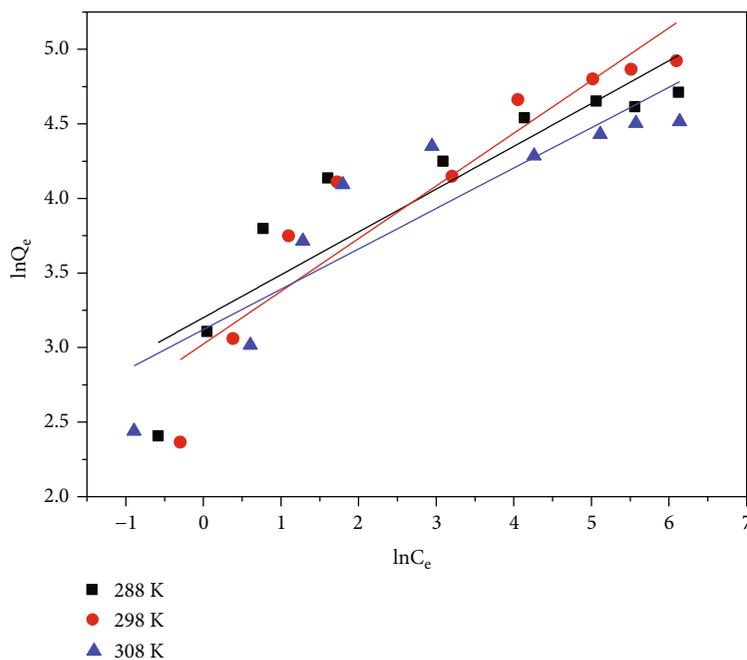


FIGURE 10: Freundlich isotherm for Cr (VI) removal on CSBT.

the data at four temperatures of 288, 298, 308, and 318 K. To obtain thermodynamic parameter information, the experimental data were analysed using the van't Hoff equation (Equation (10)).

$$\ln \left(\frac{Q_e}{C_e} \right) = \frac{\Delta S}{R} - \frac{\Delta H}{RT}, \quad (10)$$

$$\Delta G = \Delta H - T\Delta S, \quad (11)$$

where ΔS ($\text{J}\cdot\text{mol}^{-1}\cdot\text{K}^{-1}$) is the entropy change, R ($8.314\text{J}\cdot\text{mol}^{-1}\cdot\text{K}^{-1}$) is the ideal gas constant, ΔH ($\text{kJ}\cdot\text{mol}^{-1}$) is the enthalpy change, and $T(K)$ is the absolute temperature. To examine the spontaneity of the adsorption process, Equation (11) is used to calculate the Gibbs free energy.

As shown in Figure 7, the correlation coefficient (R^2) is 0.9412, meaning that the experimental data fit the equation well. The negative value of ΔH indicated that the adsorption was exothermic (Table 5). The negative value of ΔS revealed the decrement of randomness at the solid-solution interface,

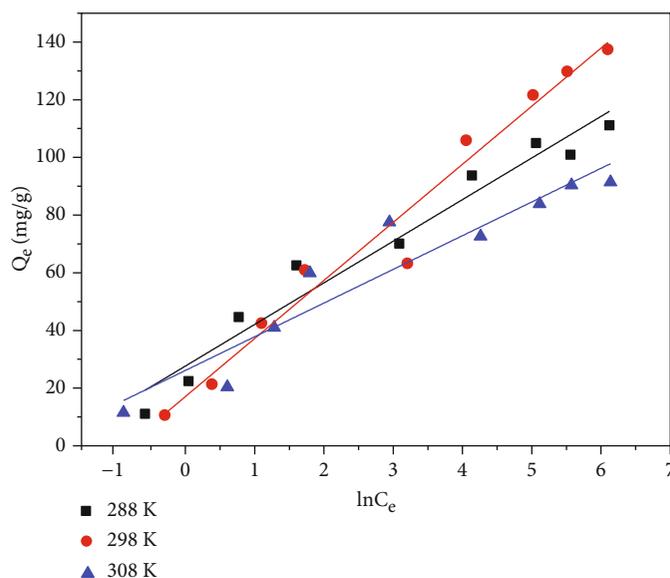


FIGURE 11: Temkin isotherm for Cr (VI) removal on CSBT.

meaning that CSBT has a better affinity towards hexavalent chromium [43]. Moreover, ΔG was negative at a lower temperature, and the adsorption process could be carried out spontaneously and was dominated by physical adsorption. However, with increasing temperature, specifically higher than 312.60 K, ΔG becomes positive, and external energy is required to force the adsorption process to carry on.

3.4.3. CSBT Dose. With increasing CSBT dose, the removal efficiency of Cr (VI) increased. The maximum removal percentage was achieved at 600 mg/L, which was 92.23%. However, at a CSBT dose of 1000 mg/L, the removal percentage decreased from 92.23% to 91.45%. This decrement could be explained by the overlap of sorption sites that negatively affect the adsorption process. Despite the maximum removal percentage at 600 mg/L, the adsorption capacity decreased with increasing CSBT dose. Therefore, the best dose of CSBT was chosen as 400 mg/L.

3.5. Adsorption Isotherm. To investigate the reaction between CSBT and Cr (VI), the effect on the removal percentage and initial Cr (VI) concentration was studied. The result (Figure 8) has shown that at a higher initial Cr (VI) concentration, the adsorption capacity of CSBT is larger for a high driving force of high Cr (VI) concentration, which can overcome the resistance of Cr (VI) ions from the solution phase to the surface of the adsorbent [44], and the adsorbent can be exposed to more Cr (VI) ions, resulting in a higher adsorption capacity. The experimental data were analysed using the Langmuir, Freundlich, Temkin, and D-R isotherm models to further understand the interactions of Cr(VI) and the adsorbent, and the results are shown in Figures 9–12.

The parameters calculated are shown in Tables 6 and 7. The theoretical Q_m at 298 K of the Langmuir isotherm is close to the experimental value of 137.43 mg/g, and it is obvious that the Langmuir isotherm model gives better fit-

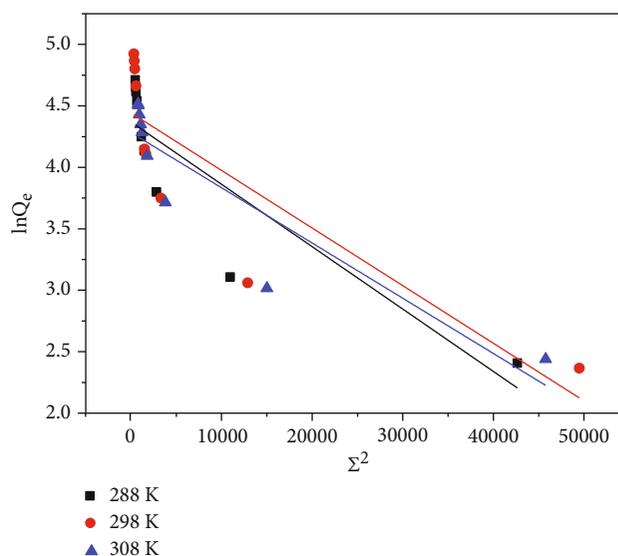


FIGURE 12: D-R isotherm for Cr (VI) removal on CSBT.

ting of the experimental data. This result described the adsorption behaviour of Cr (VI) onto the CSBT surface, and at each temperature, the R^2 value of the Langmuir isotherm was over 0.99, indicating that the adsorption was monolayer, and that the distribution of Cr (VI) ions between the solid and liquid phases was in equilibrium. Compared with other research materials, the maximum Cr (VI) adsorption capacity of CSBT is calculated to be 137.43 mg/g, which is relatively better than most related adsorbents from the use environment and adsorption capacity [18, 19, 33]. Therefore, CSBT can stand out from current materials in a theoretical environment.

3.6. Adsorption Kinetics. Adsorption efficiency is of importance for the application of an adsorbent. Therefore, the effect of different stirring times on Cr (VI) removal was

TABLE 6: Constants of Langmuir and Freundlich isotherm models for Cr (VI) removal of CSBT.

Temperature (K)	Q_m (mg/g)	K_L (L/mg)	R^2	K_F (mg/g)	$1/n$	R^2
288	110.49	0.1275	0.9976	24.55	0.2871	0.8760
298	133.85	0.0840	0.9937	19.80	0.3804	0.8192
308	90.14	0.1653	0.9965	21.90	0.2969	0.8142

TABLE 7: Constants of Temkin and D-R isotherm models for Cr (VI) removal of CSBT.

Temperature (K)	A	B	R^2	Q_m (mg/g)	b	R^2
288	27.66	14.4294	0.9570	4.37	5.0763	0.7510
298	17.08	20.1375	0.9679	4.44	4.6889	0.6886
308	26.14	11.6819	0.8906	4.28	4.4953	0.8012

TABLE 8: Pseudofirst-order and pseudosecond-order kinetic model parameters for Cr (VI) adsorption of CSBT.

k_1 (min^{-1})	Pseudofirst-order model		k^2 ($\text{mg}^{-1}\cdot\text{min}^{-1}$)	Pseudosecond-order model	
	Q_e (mg/g)	R^2		Q_e (mg/g)	R^2
13.14587	21.4472	0.97052	1.10671	22.62311	0.9978

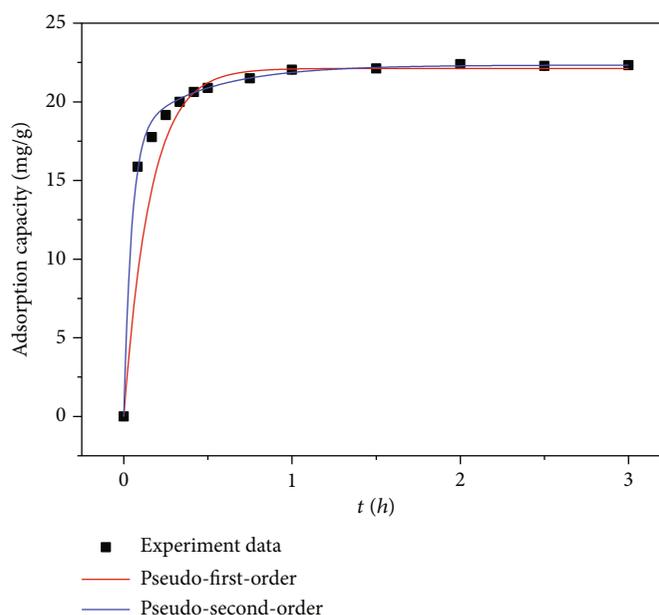


FIGURE 13: Adsorption kinetics for Cr (VI) removal on CSBT.

studied. During the initial 30 minutes, Cr (VI) was adsorbed quickly, and then the adsorption reached equilibrium at 1.5 h. Such a fast adsorption process can be attributed to the fact that at the initial stage, adsorption mainly occurred on the adsorbent surface due to the strong electrostatic interaction between amino groups on CSBT and Cr (VI) in solutions, resulting in a fast initial adsorption rate [45]. After that, the adsorption process occurred internally because of the saturation of the sorption sites on the surface, and the adsorption slowed down until equilibrium.

To further understand the adsorption mechanism, experimental data were analysed using pseudofirst-order and pseudosecond-order kinetic models. As shown in Table 8 and Figure 13, the pseudosecond-order kinetic model has a higher correlation coefficient ($R^2 = 0.9978$), and Q_e (22.62 mg/g) is closer to the experimental value (22.39 mg/g). In other words, the pseudosecond-order kinetic model is more suitable for describing the adsorption process of CSBT, and it demonstrated that the adsorption process is dependent on the reacting sites with Cr (VI).

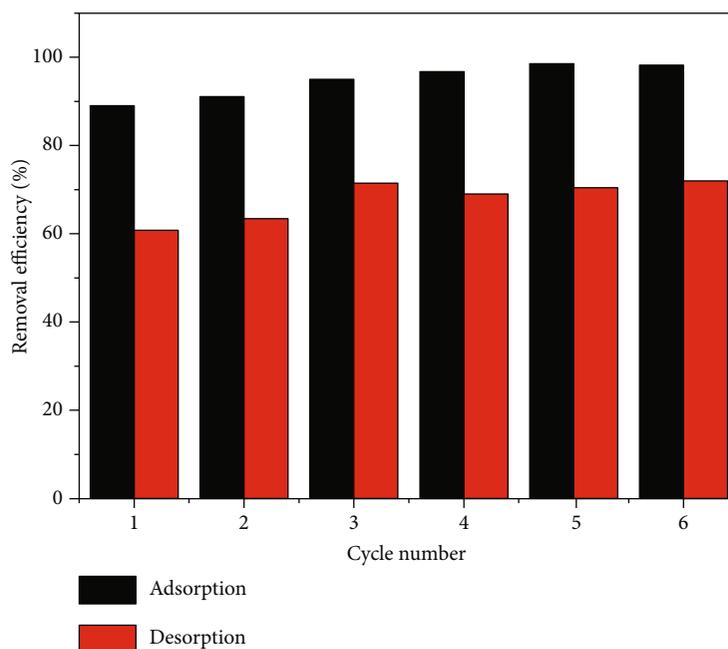


FIGURE 14: Desorption-regeneration cycles. (Adsorbent dosaging, 400 mg/L; pH value, 3.0; initial concentration, 10 mg/L; temperature, 298.15 K; contact time, 90 min; rpm, 180).

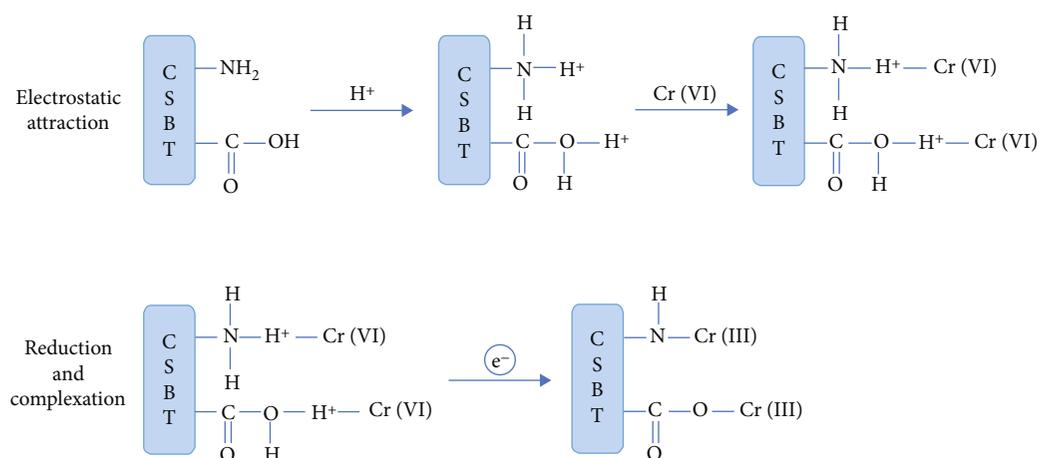


FIGURE 15: The adsorption mechanism of CSBT on Cr (VI).

3.7. Regeneration of CSBT. In practical applications, it can reduce the cost and recycle Cr (VI) resources if an adsorbent has better reusability. As discussed above, in alkaline solutions, the combination of hydroxyl groups and CSBT is more primary than Cr (VI); thus, alkaline solution can cause Cr (VI) ions to desorb. After-adsorption equilibrium, the adsorbent was transferred into 0.1 mol/L sodium hydroxyl solution to desorb the Cr (VI) ions. Then, the adsorbent will be reused. After 5 cycles, the adsorption ability of CSBT to absorb Cr (VI) was not weakened but was stronger than last time (Figure 14). For the first time, 89% of Cr (VI) was adsorbed, and for the fifth time, 98% of Cr (VI) was adsorbed, and the removal percentage was increased by 9%. The sixth adsorption rate decreased slightly, from 98.54% to 98.22%. The desorption rate increases with increasing adsorption rate, and more than 60% of Cr (VI)

can be recovered by elution with NaOH. In summary, as a Cr (VI) adsorbent, CSBT can adsorb most Cr (VI) and has good reproducibility.

3.8. Adsorption Mechanism. According to FTIR and XRD, there are a large number of active functional groups (such as hydroxyl and amino groups) on the surface of CSBT, which can interact with Cr (VI) in ion exchange and precipitation. Due to the addition of iron-modified bentonite, a porous structure is formed on the surface of the chitosan hydrogel, and the adsorption performance is enhanced [27]. There are a large number of hydrogen ions in acidic solutions. The functional groups of CSBT can be combined with hydrogen ions, effectively reducing Cr (VI) in solution to Cr (III), which is less toxic and can be complexed on the surface of CSBT by precipitation and chelation

[24–26]. The adsorption of Cr (VI) by CSBT is mainly completed by the following process: first, in an acidic environment, the amino groups ($-\text{NH}_2$) and carboxyl groups ($-\text{COOH}$) on the surface of CSBT are easily protonated into $-\text{NH}_3^+$ and $-\text{COOH}^+$ and electrostatically interact with the negatively charged Cr (VI) in the solution; then, combined with H^+ in the solution, Cr (VI) will be transformed into negatively charged Cr (III) acid radical ions, and part of the Cr (III) will interact with the CSBT surface. The functional groups undergo chelation and precipitation (Figure 15). In summary, the adsorption of Cr (VI) by CSBT is a complex and changeable process that mainly involves electrostatic interactions, reduction, and coprecipitation.

4. Conclusions

The composite material CSBT was successfully prepared by the reaction of chitosan and pillared bentonite. The layered structure of bentonite was not destroyed after composition; instead, amino groups on chitosan were connected to the pillared bentonite by hydrogen bonds. During the adsorption process, the amino groups were protonated and combined with anionic hexavalent chromium for the purpose of Cr (VI) removal. The composites have an efficient effect on Cr (VI) removal at a wide range of temperatures and adsorbent doses. However, Cr (VI) removal has been limited by the pH value of the solutions. The optimal factors for Cr (VI) removal by response surface methodology were estimated to be 298 K of temperature, $\text{pH} = 3$, and 400 mg/L of adsorbent dose, which can remove 87.61% of Cr (VI) in potassium dichromate solution. The Langmuir isotherm model and the pseudosecond-order kinetic model fit the experimental data best. The maximum adsorption capacity predicted for CSBT at 298 K is 133.85 mg/g, which is close to the experimental value of 137.43 mg/g. CSBT can be reused and maintained a high removal efficiency after six cycles.

Data Availability

The data produced or investigated during this work are involved in this submitted article.

Conflicts of Interest

The authors declare that there is no conflict of interest regarding the publication of this article.

Acknowledgments

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