

Meteorological data-based optimal control strategy for microalgae cultivation in open pond systems

Supplementary material

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S1 Model presentation

S1.1 Temperature model

The formal expression of each heat flow in Equation 8 was extracted from [1]. Assuming the water surface to be gray-diffuse, the radiation $Q_{ra,p}$ from the pond surface to the atmosphere was given by Stefan-Boltzmann's fourth power law:

$$Q_{ra,p} = -\varepsilon_w \sigma_{SB} T_p^4 S, \quad (S1-1)$$

where ε_w is the emissivity of water and σ_{SB} is the Stefan-Boltzmann constant ($\text{W m}^{-2} \text{K}^{-4}$). The heat flow associated with solar irradiance $Q_{ra,s}$ was expressed as follows:

$$Q_{ra,s} = (1 - f_a) H_s S, \quad (S1-2)$$

where f_a is the theoretical photosynthetic efficiency (the fraction of PAR that is effectively used during the photosynthetic process). The heat flow generated by air radiation was described as:

$$Q_{ra,a} = \varepsilon_a \varepsilon_w \sigma_{SB} T_a^4 S, \quad (S1-3)$$

where ε_a is the emissivity of the air and T_a is the air temperature (K). The evaporation heat flow Q_{ev} was given by the equation:

$$Q_{ev} = -m_e L_w S, \quad (S1-4)$$

where L_w is the water latent heat (J kg^{-1}), whereas m_e is the evaporation rate ($\text{kg m}^{-2} \text{s}^{-1}$). The following expression was used to calculate m_e :

$$m_e = K \left(\frac{P_w}{T_p} - \frac{RH \cdot P_a}{T_a} \right) \frac{M_w}{R}, \quad (S1-5)$$

where K is the mass transfer coefficient (m s^{-1}), P_w and P_a are, respectively, the saturated vapor pressure (Pa) at T_p and T_a , evaluated through the following empirical correlation:

$$P_i = 3385.5 \cdot e^{(-8.0929 + 0.97608(T_i + 42.607 - 273.15)^{0.5})}, \quad (S1-6)$$

where the i index represents air or water, RH is the relative air humidity above the pond surface, M_w is the molecular weight of water (kg mol^{-1}) and R is the universal ideal gas constant ($\text{Pa m}^3 \text{mol}^{-1} \text{K}^{-1}$). The mass transfer coefficient K in (S1-5) was calculated through the following two correlations:

$$Sh = 0.035 Re^{0.8} Sc^{1/3} \quad \text{for turbulent flows,} \quad (S1-7a)$$

$$Sh = 0.628 Re^{0.5} Sc^{1/3} \quad \text{for laminar flows,} \quad (S1-7b)$$

where $Sh = KL/D_{w,a}$, $Re = Lv_w/\nu_a$ and $Sc = \nu_a/D_{w,a}$. The dimensionless variables Sh , Re and Sc are, respectively, the Sherwood, Reynolds and Schmidt

numbers, L is the characteristic pond length (m), $D_{w,a}$ is the mass diffusion coefficient of water vapor in air ($\text{m}^2 \text{s}^{-1}$), v_w is the wind velocity (m s^{-1}) and ν_a is the air kinematic viscosity ($\text{m}^2 \text{s}^{-1}$). The convective flow Q_{conv} , defined as:

$$Q_{conv} = h_{conv}(T_a - T_p)S \quad (\text{S1-8})$$

was calculated by evaluating the heat transfer coefficient h_{conv} ($\text{W m}^{-2} \text{K}^{-1}$) value through the following set of correlations:

$$Nu = 0.035Re^{0.8}Pr^{1/3} \quad \text{for turbulent flows,} \quad (\text{S1-9a})$$

$$Nu = 0.628Re^{0.5}Pr^{1/3} \quad \text{for laminar flows,} \quad (\text{S1-9b})$$

where $Nu = h_{conv}L/\lambda_a$ and $Pr = \nu_a/\alpha_a$, λ_a is the air thermal conductivity ($\text{W m}^{-1} \text{K}^{-1}$) and α_a the air thermal diffusivity ($\text{m}^2 \text{s}^{-1}$). Meteorological stations measure the wind velocity at a certain height z_0 (m), which usually differs from the height at which v_w is needed in the previous correlations (0.5 m). The conversion of the wind velocity from the height z_0 to 0.5 m was performed by using the following expression:

$$v_w = v_0 \left(\frac{z}{z_0} \right)^\alpha, \quad (\text{S1-10})$$

where v_0 is the wind velocity (m s^{-1}) measured at height z_0 and α is a power law exponent. The equation that describes the conductive heat flow between the pond and the soil was based on Fourier's law:

$$Q_{cond} = k_s S \frac{dT_s}{dz}(z = 0), \quad (\text{S1-11})$$

where k_s is the soil conductivity ($\text{W m}^{-1} \text{K}^{-1}$) and T_s the soil temperature (K). The value of T_s was obtained from the following equation and initial/boundary conditions:

$$c_{p_s} \rho_s \frac{dT_s}{dt}(z, t) = k_s \frac{d^2 T_s}{dz^2}(z, t) \quad (\text{S1-12})$$

$$\begin{cases} T_s(t, z = 0) = T_p(t) & \text{b.c.(1)} \\ T_s(t, z = l_{s_{ref}}) = T_{s_{ref}} & \text{b.c.(2)} \\ \frac{d^2 T_s}{dz^2}(t = 0) = 0 & \text{i.c.} \end{cases} \quad (\text{S1-13})$$

where c_{p_s} is the soil specific heat capacity ($\text{J kg}^{-1} \text{K}^{-1}$), ρ_s is the soil density (kg m^{-3}), and $T_{s_{ref}}$ is the soil temperature (K) at the reference depth $l_{s_{ref}}$ (m). The heat flow associated with fresh medium inflow Q_{in} was computed from the equation:

$$Q_i = \rho_w c_{p_w} q^{in}(T^{in} - T_p) \quad (\text{S1-14})$$

where T^{in} is the water inflow temperature (K). Finally, the rain heat flow Q_r was expressed as:

$$Q_r = \rho_w c_{p_w} v_r (T_a - T_p) S. \quad (\text{S1-15})$$

All the parameters values used in the energy balance are tabulated in the study of [1] and reported in table S1-1.

Table S1-1: Parameter values of the energy balance

Water Parameters		
ρ_w	water density	998 ($\text{kg}\cdot\text{m}^{-3}$)
c_{p_w}	water heat capacity	$4.18\cdot 10^3$ ($\text{J}\cdot\text{kg}^{-1}\cdot\text{K}^{-1}$)
L_w	water latent heat	$2.45\cdot 10^6$ ($\text{J}\cdot\text{kg}^{-1}$)
ε_w	water emissivity	0.97 (-)
M_w	water molecular weight	0.018 ($\text{kg}\cdot\text{mol}^{-1}$)
Soil Parameters		
k_s	soil thermal conductivity	1.7 ($\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$)
c_{p_s}	soil heat capacity	$1.25\cdot 10^3$ ($\text{J}\cdot\text{kg}^{-1}\cdot\text{K}^{-1}$)
ρ_s	soil density	$1.9\cdot 10^3$ ($\text{kg}\cdot\text{m}^{-3}$)
$T_{s_{ref}}$	soil temperature at $l_{s_{ref}} = 4.5\text{m}$	286.75 (K)
Air Parameters		
ε_a	air emissivity	0.8 (-)
ν_a	air kinematics viscosity	$1.5\cdot 10^{-5}$ ($\text{m}\cdot\text{s}^{-1}$)
λ_a	air thermal conductivity	$2.6\cdot 10^{-2}$ ($\text{W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$)
α_a	air thermal diffusivity	$2.2\cdot 10^{-5}$ ($\text{m}\cdot\text{s}^{-1}$)
$D_{w,a}$	mass diffusion coefficient of water vapor in air	$2.4\cdot 10^{-5}$ ($\text{m}\cdot\text{s}^{-2}$)
Pond parameters		
V_0	initial pond volume	30 (m^3)
S	pond surface	100 (m^2)
L	pond characteristic length	10 (m)
α	power law exponent	0.29 (-)
z	wind velocity height	0.5 (m)
z_0	wind sensor height	10 (m)
f_a	algal absorption fraction	2.5 (%)
Universal constants		
σ_{SB}	Stephan-Boltzmann constant	$5.67\cdot 10^{-8}$ ($\text{W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$)
R	ideal gas constant	8.314 ($\text{Pa}\cdot\text{m}^3\cdot\text{mol}^{-1}\cdot\text{K}^{-1}$)

S1.2 Determining the solar irradiance from cloudiness data

The solar irradiance H_s was calculated from cloudiness data CC , by using the Kasten and Czeplak correlation, recommended by [2] due to its high accuracy (the average error on solar irradiance estimates is generally within 20 W m^{-2}):

$$H_s = \begin{cases} 0 & \text{if } \omega < -\omega_s \text{ or } \omega > \omega_s \\ \frac{H_c(4-3(CC/8)^{3.4})}{4} & \text{if } -\omega_s \leq \omega \leq \omega_s, \end{cases} \quad (\text{S1-16})$$

where CC is the cloudiness expressed in OKTAS (range $0 \div 8$), H_c is the clear-sky total irradiance (W m^{-2}), ω is the hour angle which varies from $-\pi$ to π over a day, $-\omega_s$ and ω_s are, respectively, the hour angle values at sunrise and sunset. The variable ω_s is calculated from the following equation:

$$\cos \omega_s = -\tan \delta \tan \phi, \quad (\text{S1-17})$$

where ϕ is the local latitude and δ is the solar declination angle. The term δ was evaluated as follows ([3]):

$$\delta = 23.45 \frac{\pi}{180} \sin \left(2\pi \frac{284 + N}{365} \right), \quad (\text{S1-18})$$

where N is the Julian day of the year ($N = 1$ for the first day of January). The clear-sky radiation H_c was given by ([3]):

$$H_c = H_{d,c} + H_{D,c} = (\tau_{d,c} + \tau_{D,c})H_0, \quad (\text{S1-19})$$

where $\tau_{d,c} = H_{d,c}/H_0$ and $\tau_{D,c} = H_{D,c}/H_0$. $H_{d,c}$ and $H_{D,c}$ are, respectively, the diffuse and the direct components of the clear-sky total irradiance (W m^{-2}). The variable H_0 , defined as the amount of solar radiation reaching the external surface of the atmosphere, was given by ([3]):

$$H_0 = I_{sc} \left(1 + 0.033 \cos \frac{360N}{365} \right) \cos \theta_z, \quad (\text{S1-20})$$

where I_{sc} is the solar constant (1367 W m^{-2}) and θ_z is the zenith angle (the angle between the vertical axis and the sun direction), evaluated through the expression:

$$\cos \theta_z = \sin \phi \sin \delta + \cos \phi \cos \delta \cos \omega. \quad (\text{S1-21})$$

The variable $\tau_{D,c}$ was obtained through the following expression ([2]):

$$\tau_{D,c} = \exp(-\gamma T_{LK} A), \quad (\text{S1-22})$$

where T_{LK} is an empirical coefficient (set to 2.74). The term γ was given by the equation:

$$\gamma = \frac{1}{9.4 + 0.9A} \quad (\text{S1-23})$$

and A is the pressure-corrected air-mass, obtained from the following correlation ([2]):

$$A = \frac{1}{\cos \theta_z + 0.50572 \left(96.07995 - \theta_z \frac{180}{\pi} \right)^{-1.6364}}. \quad (\text{S1-24})$$

Finally, the variable $\tau_{d,c}$ is determined through the Erbs correlation (recommended by [3]):

$$K_d = \begin{cases} 1.0 - 0.09k_T & \text{if } k_T \leq 0.22 \\ 0.9511 - 0.1604k_T + 4.388k_T^2 + \\ \quad -16.638k_T^3 + 12.336k_T^4 & \text{if } 0.22 < k_T \leq 0.8 \\ 0.16527 & \text{if } k_T > 0.8 \end{cases} \quad (\text{S1-25})$$

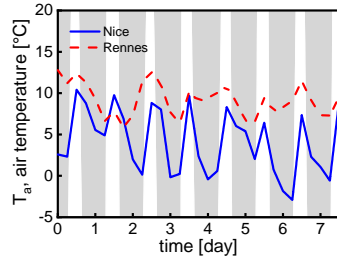
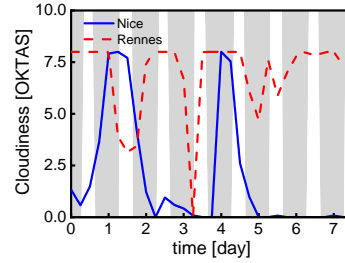
where $K_d = \tau_{d,c}/(\tau_{d,c} + \tau_{D,c})$ and $k_T = \tau_{d,c} + \tau_{D,c}$.

S2 Meteorological data

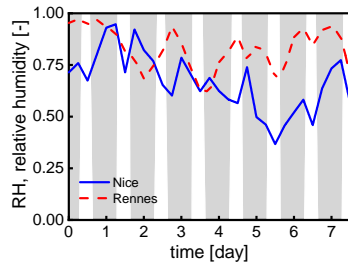
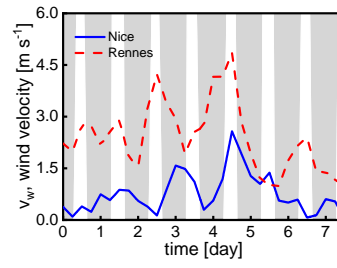
The weather data extracted from the European Centre for Medium-Range Weather Forecast (ECMWF) website were: the air temperature T_a , the sky cloudiness CC , the relative humidity RH , the wind velocity v_w and the rain volumetric flux v_r during the simulated cultivation period. Figures S2-1, S2-2 and S2-3 represent, respectively, the implemented meteorological data for the Winter, Spring and Summer case studies.

Bibliography

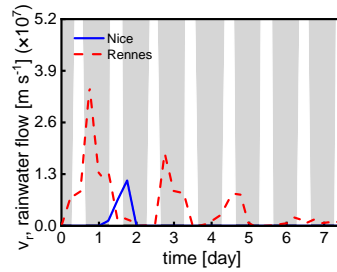
- [1] Q. Béchet, A. Shilton, J. B. K. Park, R. J. Craggs, B. Guieysse, Universal temperature model for shallow algal ponds provides improved accuracy, *Environ. Sci. Technol.* 45 (2011) 3702–3709. doi:10.1021/es1040706.
- [2] T. R. Marthews, Y. Malhi, H. Iwata, Calculating downward longwave radiation under clear and cloudy conditions over a tropical lowland forest site: an evaluation of model schemes for hourly data, *Theor. Appl. Climatol.* 107(3-4) (2012) 461–477. doi:10.1007/s00704-011-0486-9.
- [3] J. A. Duffie, W. A. Beckman, *Solar Engineering of Thermal Processes*, Little, Brown & Co., Boston, 1958.

(a) Winter: Air temperature T_a 

(b) Winter: Cloudiness

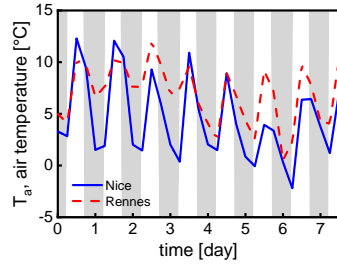
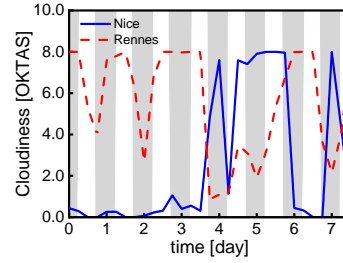
(c) Winter: Relative humidity RH 

(d) Winter: Wind velocity

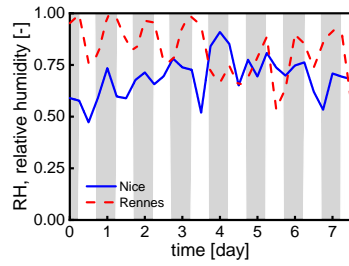
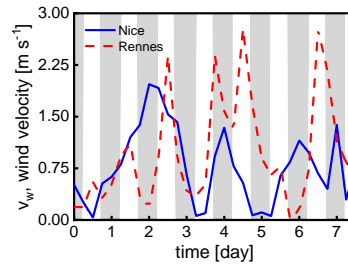


(e) Winter: Rain

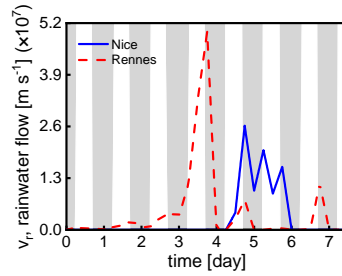
Figure S2-1: Meteorological data: Winter case (Plain line: Nice; dashed line: Rennes. The background is colored in white at daytime and in grey at night-time.)

(a) Spring: Air temperature T_a 

(b) Spring: Cloudiness

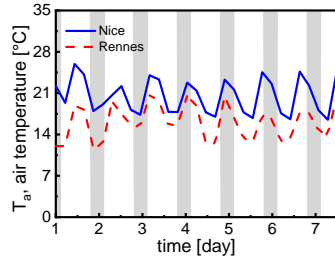
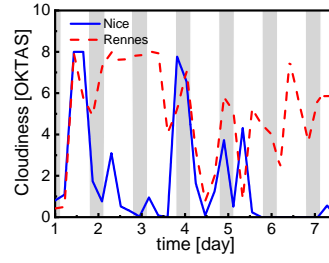
(c) Spring: Relative humidity RH 

(d) Spring: Wind velocity

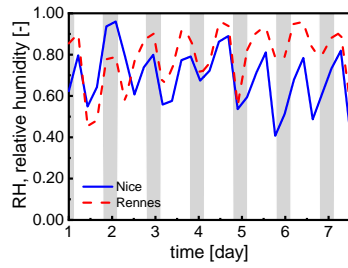
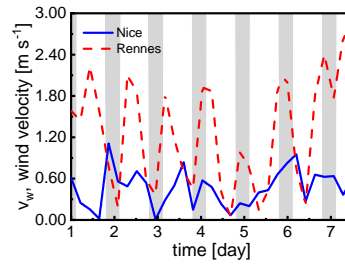


(e) Spring: Rain

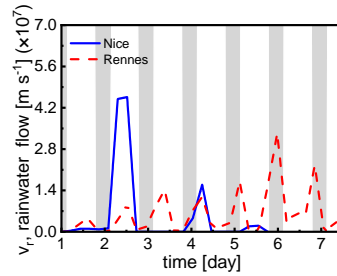
Figure S2-2: Meteorological data: Spring case (Plain line: Nice; dashed line: Rennes. The background is colored in white at daytime and in grey at night-time.)

(a) Summer: Air temperature T_a 

(b) Summer: Cloudiness

(c) Summer: Relative humidity RH 

(d) Summer: Wind velocity



(e) Summer: Rain

Figure S2-3: Meteorological data: Summer case (Plain line: Nice; dashed line: Rennes. The background is colored in white at daytime and in grey at night-time.)