Brittleness is a key mechanical parameter in the evaluation of hydraulic fracturing and wellbore stability of coal and shale reservoirs [1–3]. Brittleness of coal refers to the irreversible property of coal breaking, which indirectly reflects the complexity of fractures formed after fracturing in coal and is closely related to the difficulty of fracturing in coal reservoir. Brittleness can generally be quantitatively characterized by the brittleness index. The brittleness index can measure the ability of coal to resist fragmentation under pressure, it significantly affects the cutability and coal production rate during coal mining [2, 4] and affects the drilling efficiency during the well drilling process [5]. The brittleness index is also the key index to evaluate the fracturability of coal reservoirs [1, 6].

Various researchers have devoted to the studies on the evaluation method of rock brittleness [7–14]. There were divergences between researchers on how to determine the brittleness index of rock. The evaluation of rock brittleness was put forward through uniaxial tensile and compressive experiments in 1974 by Hucka and Das [7]. The relationship between rock brittleness and hardness coefficient and fracture toughness, the functional relationship between rock brittleness and rock tensile and compressive strength, were established through mechanical property experiments and tests in succession [8, 9]. Since the beginning of this century, with the rise of the unconventional oil and gas industry, the
research of brittleness index in coal reservoirs has been widely concerned by scholars. Different researchers summed up the definition of brittleness index and put forward different quantitative calculation methods of the brittleness index. A brittleness index evaluation method based on the rock brittle mineral content was proposed based on the correlation between mineral composition and brittleness in shales [10]. Another method to quantitatively calculate the brittleness index was proposed based on Young’s modulus and Poisson’s ratio in the rock mechanics parameters [11]. Then, a new method was proposed to evaluate the brittleness of shale by using X-fluorescence element logging data [12]. Some
scholars thought that the brittleness index could be quantified from the perspective of influencing factors and coal brittleness evaluation method could be revised from that of shale [13, 14]. A review of the previous literatures makes it clear that different researchers have different definitions for the concept of rock brittleness.

So far, brittleness index studies have been widely used in shale gas and tight sandstone gas [1, 10–13]. However, limited by logging technology and the traditional low-cost exploration concept of CBM, there were few researches on the evaluation of brittleness index in coal reservoirs [15–18], especially the influence factors of coal brittleness index. Previous studies have shown that the coal brittleness was mainly affected by coal rank, composition, and coal-body structure [15–17, 19]. However, current scholars are still unclear on the quantitative relationship between coal

<table>
<thead>
<tr>
<th>Stratigraphic age</th>
<th>Stratum thickness (m)</th>
<th>Lithology section</th>
<th>Coal seam</th>
<th>Lithology description</th>
</tr>
</thead>
<tbody>
<tr>
<td>Carboniferous</td>
<td>Upper series</td>
<td>245–870</td>
<td></td>
<td>Purple-red, brick-red mudstone with yellow-green, purple-red sandstone.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>Purple-red mudstone and medium-coarse sandstone interbedded.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>Gray-green, purple-red mudstone with manganese and iron nodules.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>Gray, gray-green siltstone interbedded with fine sandstone.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>Gray sandstone and mudstone with color mudstone with slotic.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>Dark gray, gray mudstone, interbedded sandy mudstone and siltstone.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>The bottom is gray coarse, medium and fine sandstone with 1–4 layers of coal seams.</td>
</tr>
<tr>
<td></td>
<td>Upper series</td>
<td>45–71</td>
<td>No. 3 coal</td>
<td>The lithology is more complex, consisting of gray-black mudstone, sandstone, limestone and coal.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>The upper section is gray-black mudstone with gray sandstone, containing 2–3 layers of coal seams.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>The lower section is 3–4 layers of limestone with sandy mudstone, coal-bearing 2–3 layers.</td>
</tr>
<tr>
<td></td>
<td>Middle series</td>
<td>30–40</td>
<td>No 15 coal</td>
<td>The upper part is dark gray mudstone, dark gray siltstone.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>The lower part is mudstone, with breccia at the bottom, rich in iron nodules.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>The top is limestone, the upper part is gray-dark gray limestone.</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>The lower part is gray, dark gray, gray yellow marlstone, with thin gypsum layers.</td>
</tr>
</tbody>
</table>

**Figure 2:** Stratigraphic column of coal-bearing sequences in the Mabidong block.
brittleness and inherent influencing factors of coal reservoir. Therefore, the establishment of the coal brittleness index calculation method based on the coal-body structure and composition has important practical significance for brittleness evaluation of coal reservoirs in CBM exploration and development.

In this research, the brittleness index of a high-rank coal reservoir and its influencing factors were studied in Mabidong CBM block, Qinshui Basin, China. Based on the observation and description of coal cores of 15 CBM exploration wells, array sonic logging, density logging, and coal quality test data, the elastic parameter method was used to calculate

### Table 1: Coal-body structure division of a coal seam in the Mabidong block (refer to reference [21]).

<table>
<thead>
<tr>
<th>Coal-body structure</th>
<th>Coal core shape</th>
<th>Coal core photograph</th>
<th>Description of coal core characteristics</th>
</tr>
</thead>
<tbody>
<tr>
<td>Primary structure</td>
<td>Column, block</td>
<td><img src="image1.png" alt="Image" /></td>
<td>The band of coal lithotype and primary structure are clear, block structure, and hard.</td>
</tr>
<tr>
<td>Cataclastic structure</td>
<td>Column, block, coal broken</td>
<td><img src="image2.png" alt="Image" /></td>
<td>The band is visible, but the coal is intersected by exogenous fractures without clear displacement and is also block.</td>
</tr>
<tr>
<td>Granulated structure</td>
<td>Crushed, coal broken seriously</td>
<td><img src="image3.png" alt="Image" /></td>
<td>The primary band and block structure are damaged, and particle structure, small cracks in different directions developed, test by hand, it has a certain hardness and can be crushed into small fragments.</td>
</tr>
</tbody>
</table>

### Table 2: Coal brittleness index seams with different coal-body structures in the Mabidong block.

<table>
<thead>
<tr>
<th>Well number/coal seam</th>
<th>Primary structure</th>
<th>Well number/coal seam</th>
<th>Cataclastic structure</th>
<th>Well number/coal seam</th>
<th>Granulated structure</th>
</tr>
</thead>
<tbody>
<tr>
<td>Ma 1/No. 3</td>
<td>58.18-68.06</td>
<td>Ma 69/No. 3</td>
<td>71-75.1</td>
<td>Ma 11/No. 3</td>
<td>79.7-83.4</td>
</tr>
<tr>
<td>Ma 17/No. 3</td>
<td>56.6-73.2</td>
<td>Ma 1/No. 15</td>
<td>76.24-77.13</td>
<td>Ma 27/No. 3</td>
<td>75.4-84.2</td>
</tr>
<tr>
<td>Ma 58/No. 3</td>
<td>61.4-70.9</td>
<td>Ma 59/No. 15</td>
<td>71.8-72.33</td>
<td>Ma 66/No. 3</td>
<td>76.5-89</td>
</tr>
<tr>
<td>Ma 67/No. 3</td>
<td>62.9-67.9</td>
<td>Ma 68/No. 3</td>
<td>77.09-77.44</td>
<td>Ma 58/No. 15</td>
<td>75.92-82.4</td>
</tr>
<tr>
<td>Ma 6/No. 15</td>
<td>68.25-75.02</td>
<td>Ma 58/No. 15</td>
<td>79.87-80.15</td>
<td>Ma 66/No. 15</td>
<td>79.87-80.15</td>
</tr>
<tr>
<td>Ma 25/No. 15</td>
<td>72.58-73.77</td>
<td>Average</td>
<td>73.01-74.85</td>
<td>Average</td>
<td>77.41-82.77</td>
</tr>
<tr>
<td>Average</td>
<td>63.3-71.48</td>
<td>Average</td>
<td>73.01-74.85</td>
<td>Average</td>
<td>77.41-82.77</td>
</tr>
</tbody>
</table>
the coal brittleness index reservoirs in this block, and the geological factors on coal brittleness index were analyzed and discussed.

2. Research Method, Process and Data Source

2.1. Evaluation Method of Coal Brittleness Index Reservoirs. Coal reservoirs are typical organic reservoirs, so the mineral component method commonly used in shale brittleness index evaluation is unable to be used in evaluation of the coal brittleness index. Therefore, the elastic parameter method was adopted in this study to calculate the brittleness index of high-rank coal reservoir. The calculation of rock brittleness by the elastic parameter method can provide a convenient and practical means for evaluating rock reservoir brittleness by using logging and seismic data [17, 18]. Rickman et al. first used normalized Young’s modulus and Poisson’s ratio to characterize rock brittleness [11]. The calculation formula and definitions of brittleness used in this study are formulated as follows:

\[
E = \frac{\rho (3\Delta t_s^2 - 4\Delta t_c^2)}{\Delta t_s^2 (\Delta t_s^2 - \Delta t_c^2)},
\]

(1)

\[
\mu = \frac{0.5\Delta t_s^2 - \Delta t_c^2}{\Delta t_s^2 - \Delta t_c^2},
\]

(2)

\[
BI = \left( 0.5 \times \frac{E - E \min}{E \max - E \min} + 0.5 \times \frac{\mu - \mu \max}{\mu \min - \mu \max} \right) \times 100,
\]

(3)

where \(E\) is Young’s modulus, GPa; \(\mu\) is Poisson’s ratio, dimensionless; \(\rho\) is the density, g/cm\(^3\); \(\Delta t_s\) is the transverse wave time difference, \(\mu\)m/s; \(\Delta t_c\) is the longitudinal wave time difference, \(\mu\)m/s; BI is the coal brittleness index, dimensionless; \(E\max\) and \(E\min\) are the maximum and minimum values of Young’s modulus in a certain coal seam section in a certain block, GPa; and \(\mu\max\) and \(\mu\min\) are the maximum and minimum values of Poisson’s ratio in a certain coal seam section in a certain block, dimensionless.

According to the statistics of elastic parameters of coal reservoirs in Mabidong block, the \(\mu\max\) and \(\mu\min\) of coal used in the normalization of brittleness index calculation are 0.3 GPa and 0.2 GPa, and the \(E\max\) and \(E\min\) are 0.9 GPa and 0.3 GPa in this study.

2.2. Research Processes and Data Source. The overall research approach of this study is to use the elastic parameter method to calculate the coal brittleness index and combine the coal core analysis data to find out the influencing factors of the coal brittleness index reservoirs. The specific research process is detailed as follows: (1) Based on the core test data of CBM exploration wells in the Mabidong block, the vitrinite reflectance, macerals, and industrial analysis data of the tested coal samples were obtained. (2) Based on core photograph features corresponding to the depth of coal samples, the coal-body structure types of the corresponding coal seam were qualitatively determined. (3) Through the process of core true depth determination, the density logging parameters (density logging value) and array acoustic logging parameters (transverse wave time difference and longitudinal wave time difference) corresponding to the sampling depth of core were obtained, and then, the coal brittleness index was obtained by elastic parameter method. (4) The influence of the coal-body structure and mechanical parameters on the coal brittleness index was analyzed. (5) The influence of coal quality parameters on the brittleness index is analyzed.

In this study, all the data of array acoustic logging, density logging, coal maceral composition, and coal quality parameters were approved and obtained from the field and laboratory test report of Huabei oilfield company of Petro-China. There are 9 wells with data from No. 3 coal seam and 6 wells with data from No. 15 coal seam.

3. Geological Setting

The Mabidong block is located in the southwest of Qinshui Basin, Shanxi Province, North China. The main structures in this block include the Qinshui synclinorium with NNE-trending and a series of associated NNE-trending normal faults [20]. According to the direction perpendicular to the synclinorium structural line strike, Mabidong block can be roughly divided into three tectonic units, and they are the western slope zone, the central trough zone and the eastern slope zone (Figure 1). The structure of the west wing is simple, and it is a monocline dipping toward southeast. The faults in this area are mostly small ones with short extension distance and the NNE strike. Compared with the west wing, the overall structure of the east wing is more complex, with more developed faults, generally smaller fault spacing, steeper occurrence, and shorter extension length. The results of structural interpretation show that the central and northern part of the block is relatively simple in structure, with large buried depth and good preservation conditions, and is a sweet spot for further CBM exploration.

The main coal-bearing strata in the block are Taiyuan Formation and Shanxi Formation in the Carboniferous-Permian. The No. 3 coal seam in Shanxi Formation and No. 15 coal seam in Taiyuan Formation are the target strata of CBM development (Figure 2). The burial depth of No. 3 coal seam in the block is 860~1420 m. The burial depth is shallow in the west and deep in the east, and the thickness is 4.6~8.0 m with an average of 6.2 m. The maximum reflectance of vitrinite of No. 3 coal ranges from 2.61% to 3.36%, with an average of 2.96%. The No. 3 coal belongs to

| Table 3: Mechanical parameters of No. 3 and No. 15 coal seams in the Mabidong block.

<table>
<thead>
<tr>
<th>Coal-body structure</th>
<th>Coal seam</th>
<th>Modulus of elasticity</th>
<th>Poisson’s ratio</th>
</tr>
</thead>
<tbody>
<tr>
<td>Primary structure</td>
<td>No. 3</td>
<td>0.593</td>
<td>0.2269</td>
</tr>
<tr>
<td></td>
<td>No. 15</td>
<td>0.660</td>
<td>0.2312</td>
</tr>
<tr>
<td>Cataclastic structure</td>
<td>No. 3</td>
<td>0.635</td>
<td>0.2335</td>
</tr>
<tr>
<td></td>
<td>No. 15</td>
<td>0.610</td>
<td>0.2300</td>
</tr>
<tr>
<td>Granulate structure</td>
<td>No. 3</td>
<td>0.715</td>
<td>0.2279</td>
</tr>
<tr>
<td></td>
<td>No. 15</td>
<td>0.741</td>
<td>0.2305</td>
</tr>
</tbody>
</table>

- Primary structure
- Cataclastic structure
- Granulate structure

The data for Tables 1 and 3 are obtained from the array acoustic logging of a certain coal seam section in a certain block.
anthracite. The burial depth of No. 15 coal seam is 980~1520 m, about 100 m deeper than No. 3 coal seam. The burial depth trend is the same as No. 3 coal seam, shallow in the west and deep in the east. The thickness is mostly between 3.5 and 5.5 m, with an average of 5.1 m. The maximum reflectance of vitrinite of No. 15 coal ranges from 2.65% to 2.71%, with an average of 2.68%. The No. 15 coal also belongs to anthracite.

4. Influencing Factors of Coal Reservoir Brittleness Index in Mabidong Block

4.1. Relationship between Coal-Body Structure and Britteness Index. The coal-body structure has great influence on the physical properties of coal reservoir properties [21, 22]. Due to the complex structural conditions (Figure 1), the tectonic coal is relatively developed in the Mabidong block. According to the characteristics of core shape, photograph, and the description of core characteristics (macrostructure and fracture), the coal core samples are divided into primary structure coal, cataclastic structure coal, and granular structure coal (Table 1). The primary structure coal retains the original sedimentary structure characteristics, while the cataclastic structure coal and granulate structure coal were affected by the Indosinian Movement, Yanshan Movement, and Himalayan Movement and were strongly compressed, uplifted, and eroded. The degree of fragmentation of the cataclastic structure coal is larger than that of the primary structure coal, and the degree of fragmentation of granulate structure coal is the largest.

According to the density logging and array sonic logging data of CBM wells in the Mabidong block, the mechanical parameters are obtained, and the brittleness indexes are calculated according to the mechanical parameters. The brittleness indexes are compared with the coal-body structure types of drilling core samples. The relationship between the coal-body structure and brittleness index is studied and classified statistic (Table 2). The calculation results show that the average interval of the coal brittleness index of the primary structural coal, cataclastic structural coal, and granulate structural coal (Table 1).

Figure 3: Relationship between mechanical parameters and the brittleness index of No. 3 and No. 15 coal: (a, c) No. 3 coal and (b, d) No. 15 coal.
coal is 63.3-71.48, 73.01-74.85, and 77.41-82.77, respectively. It reveals that, according to the coal-body structure, the order of the coal brittleness index is primary structural coal < cataclastic structural coal < granulate structural coal (Table 2). The results are consistent with previous studies [15, 16]. It reveals that as the brittleness index generally is increasing, the degree of coal fragmentation increases. The reason may lie in the influence of Young’s modulus. Previous studies have shown that Young’s modulus of coal is closely related to density, porosity, and effective stress of the coal [23, 24]. The Mabidong block is located in the core of syncline of Qinshui Basin, and the regional tectonic stress field is dominated by compression stress. Therefore, in the process of tectonic coal formation, the pores and fractures in coal seams were compressed and closed, the porosity decreases, and Young’s modulus increases. There are a certain crossover and overlap between the brittleness indexes of different coal-body structures, which are affected by the characteristics of coal seam structure, heterogeneity, resolution of logging tools, continuity of logging response values, well bore, well section, and roof and floor lithology [15].

4.2. Influence of Mechanical Parameters on Coal Brittleness Index. The main mechanical parameters that affect the coal brittleness index are Young’s modulus and Poisson’s ratio. The relevant parameters based on statistics are shown in Table 3. In the study area, Young’s modulus of granulate structure coal is relatively high, and Poisson’s ratio of cataclastic structure coal is relatively high. Young’s modulus and Poisson’s ratio of No. 15 primary structure coal are both greater than that of No. 3 primary structure. The possible reason is that in the deeper coal-forming and water-covered environment of No. 15 coal, the gelation of peat is more thorough, and there are more homogeneous vitrinite and matrix vitrinite content [25]. The correlation among the brittleness index, Young’s modulus, and Poisson’s ratio of No. 3 coal seam and No. 15 coal seam is shown in Figure 3. Young’s modulus has a good positive correlation with the brittleness index. Young’s modulus and the brittleness index of primary structure coal of No. 3 coal seam have the best correlation, followed by the primary structure coal of No. 15 coal seam (Figures 3(a) and 3(b)). This is because the coal body of the primary structural coal is complete and its mechanical properties are more stable. Poisson’s ratio and brittleness index are negatively correlated in No. 3 coal seam (Figure 3(c)) but are positive correlated in No. 15 coal seam (Figure 3(d)). The correlation coefficient between Poisson’s ratio and the coal brittleness index is small. The difference in the correlation between the same mechanical parameter and the brittleness index is comprehensively affected by the coal-body structure, coal macerals, and coal quality parameters.

4.3. Influence of Macerals on Coal Brittleness Index. The brittleness index is a complex function of lithology, composition, temperature, and porosity [26]. Due to the different mechanical properties of different coal macerals, the composition of coal macerals has an important influence on the coal brittleness index. According to some of the measurement results of coal macerals of 13 wells (15-layer coal seams) in the Mabidong block, the macerals and the brittleness index data of coal with different coal-body structures are obtained.

As shown in Table 4, the macerals of high metamorphic anthracite is mainly vitrinite. The vitrinite content and the mineral content of No. 15 coal seam is generally higher than that of No. 3 coal seam, and the inertinite content is lower than that of No. 3 coal seam, which is caused by deep water covering of the coal formation environment of No. 15 coal seam [25]. The average vitrinite content of primary structure, cataclastic structure, and granulate structure coals is 84.49%, 81.98%, and 83.94%, respectively. The average inertinite content of primary structure, cataclastic structure, and granulate structure coals is 14.81%, 18.02%, and 16.06%. The average mineral content of primary structure, cataclastic structure, and granulate structure coals is 4.50%, 4.58%, and 5.86%. There is no exinite in coal of this block, because aliphatic components in the exinite will be converted into gaseous hydrocarbons in the middle to high coalification stage.

The brittleness index varies with changes in the maceral and microlithotype composition of coal. In the Mabidong block, the vitrinite content is positively correlated with the coal brittleness index (Figure 4(a)), while the inertinite content is negatively correlated with the coal brittleness index (Figure 4(b)). The correlation between the brittleness index and macerals in the primary structure coal is better than that of the cataclastic and granulate structure coal (Figures 4(a) and 4(b)). Previous studies have shown that different components of coal have different effects on brittleness, grindability, and breakability of coal, and the brittleness of the coal structure rather than its hardness dominates coal grindability [19, 27, 28]. The vitrinite is the brittleness component in coal, and the inertinite is the hardness component in coal. As a result, for the primary structure coal, the coal brittleness index is positively correlated with the vitrinite content, but negatively correlated with the inertinite content obviously. The correlations between the mineral and brittleness index of different coal-body structures are poor (Figure 4(c)). The main reason is that the content of minerals in coal is relatively low, and it is easily affected by the deformation of coal structure. Nevertheless, it can be seen that there is a certain positive correlation between the brittleness index and mineral content in primary structural coal (Figure 4(c)). Because Young’s
modulus of inorganic minerals is generally higher than that of organic coal, the presence of inorganic minerals can increase Young’s modulus of the coal.

4.4. Influence of Coal Quality Parameters on Coal Brittleness Index. The proximate analysis of coal is the most common experimental analysis method in coal quality analysis. The proximate analysis indexes of coal include ash, moisture, volatile, and fixed carbon. Based on the proximate analysis of coal samples from CBM wells, coal quality parameters of No. 3 and No. 15 coal seams in the Mabidong block are obtained. As shown in Table 5, the coal quality parameters of No. 3 and No. 15 coal seams have little differences. The moisture content of No. 15 coal seam is less than that of No. 3 coal seam, the volatile of primary structural coal and cataclastic structural coal of No. 15 coal seam is both larger than that of No. 3 coal seam, and the volatile of granulate structural coal are smaller than that of No. 3 coal seam. The ash content of granular structure coal is the highest, which is consistent with the highest mineral content of granular structure coal.

The correlation between coal quality parameters and brittleness index data of different coal-body structure in Mabidong block of Qinshui Basin is obtained by statistical analysis (Figure 5). It is obvious that the correlation between the brittleness index and coal quality parameters is obviously affected by the coal-body structure, showing different correlation rules. For the primary structure coal and cataclastic structure coal, the content of ash and volatile is positively correlated with the brittleness index, while the content of fixed carbon is negatively correlated with the brittleness index. However, for the granulate structure coal, these correlation rules are just opposite (Figures 5(a), 5(b), and 5(d)). The positive correlation between ash content and coal brittleness is consistent with the results in Figure 4(a), because the presence of inorganic minerals increases Young’s modulus of the coal [24]. The correlation between the brittleness index and coal quality parameters in the primary structure coal is significantly better than that of the cataclastic and granulate structure coals. This phenomenon reveals that the influence of the coal-body structure on the brittleness index is higher than that of coal quality parameters. The higher the failure
degree of coal-body structure, the more complex the factors affecting the coal brittleness index. The correlations between moisture and the brittleness index of different coal-body structures are poor (Figure 5(c)). The reason is that the differences of moisture (intrinsic water) in the coal seam within the same block are very tiny, and the brittleness index calculated by logging may be more affected by external water in coal fissures.

5. Conclusion

(1) The calculation results of coal brittleness by elastic parameter method show that, according to the coal-body structure, the order of the coal brittleness index is primary structural coal < cataclastic structural coal < granulate structural coal. This may be because under the background of compressive stress field,
pores and fractures in coal seam are compressed and closed, porosity decreases, and Young's modulus increases. There is a good correlation between mechanical parameters and the coal brittleness index, and the brittleness index is more affected by Young's modulus than Poisson's ratio.

(2) Coal macerals are closely related to Young's modulus and Poisson's ratio, which can influence the brittleness of coal. The vitrinite content is positively correlated with the brittleness index, while the content of inertinite is negatively correlated in different types of coal-body structures. The vitrinite and inertinite content in primary structure coal has the best correlation with brittleness index. In addition, the mineral content of coal also affects the brittleness of coal in different degrees.

(3) For the primary and cataclastic structure coals, the ash and volatile is positively correlated with the brittleness index. However, for the granulate structure coal, these correlation rules are just opposite. The correlation of the brittleness index and coal quality parameters in the primary structure coal is significantly better than that of cataclastic and granulate structure coals. It reveals that the influence of the coal-body structure on the brittleness index is higher than that of coal quality parameters.

(4) The mechanical parameters, macerals, and coal quality index of coal are closely related to each other, and together affect the coal brittleness index. This study can provide a useful reference for brittleness characteristics and the relationship between brittleness index and composition of high-rank coal with different coal-body structures. The results are helpful to guide the application of the coal brittleness index and coal-body structure prediction in fracturing of CBM wells. More research on the influencing mechanism of microstructure on the coal brittleness index needs to be carried out in the future.

Data Availability

All data are derived from field logging and sampling test data from CBM Wells of Huabei Oilfield Company of PetroChina, which are given in the article and described in Acknowledgements.

Conflicts of Interest

The authors declare that they have no conflicts of interest.

Acknowledgments

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References

[14] Y. J. Lu, Z. Z. Yang, V. V. Shelepov, J. X. Han, X. G. Li, and W. Han, "Evaluation and research of brittleness on simulated


