

General introduction

```
In [1]: #The code is developed for OCM and MDA thermally coupled reactors
# The values used are for case 1* in Table 8 of the manuscript
#The code is publicly disclosed and is free to use for educational purposes for advance
#Across each line of the code, the respective unit along a short explanation is mention
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```

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Cell 1.0 Installing and importing required libraries

Cell 1.1 Importing required libraries

```
In [3]: import numpy as np
from sympy import symbols, solve
from scipy.integrate import solve_bvp, odeint
import matplotlib.pyplot as plt
from numpy import trapz
import mpmath as mpm
import statistics as st
import pandas as pd
```

Cell 1.2 Installing thermo library

```
In [4]: pip install thermo
```

Requirement already satisfied: thermo in c:\users\mamoun.al-rawashdeh\anaconda3\lib\site-packages (0.1.40)Note: you may need to restart the kernel to use updated packages.
Requirement already satisfied: fluids>=0.1.77 in c:\users\mamoun.al-rawashdeh\anaconda3\lib\site-packages (from thermo) (1.0.2)
Requirement already satisfied: scipy in c:\users\mamoun.al-rawashdeh\anaconda3\lib\site-packages (from thermo) (1.5.2)
Requirement already satisfied: pandas in c:\users\mamoun.al-rawashdeh\anaconda3\lib\site-packages (from thermo) (1.1.3)
Requirement already satisfied: numpy>=1.5.0 in c:\users\mamoun.al-rawashdeh\anaconda3\lib\site-packages (from fluids>=0.1.77->thermo) (1.19.2)
Requirement already satisfied: python-dateutil>=2.7.3 in c:\users\mamoun.al-rawashdeh\anaconda3\lib\site-packages (from pandas->thermo) (2.8.1)
Requirement already satisfied: pytz>=2017.2 in c:\users\mamoun.al-rawashdeh\anaconda3\lib\site-packages (from pandas->thermo) (2020.1)
Requirement already satisfied: six>=1.5 in c:\users\mamoun.al-rawashdeh\anaconda3\lib\site-packages (from python-dateutil>=2.7.3->pandas->thermo) (1.15.0)

Cell 1.3 Upgrading thermo library

In [5]: `pip install --upgrade pip`

Requirement already satisfied: pip in c:\users\mamoun.al-rawashdeh\anaconda3\lib\site-packages (23.1.2)
Note: you may need to restart the kernel to use updated packages.

Cell 1.4 Importing relevant thermo libraries

In [6]: `from thermo.chemical import Chemical
from thermo.mixture import Mixture`

Cell 2.0 Reactor model

Cell 2.1 Constants

In [7]: `#OCM
Rh = 1.9858775 * (10**-3) #kcal K-1 mol-1 #gas constant
Poh = 1 #atm #initial pressure
Prefh = Poh * 101325 #Pa #reference pressure
Toh = 800 + 273 #K #initial temperature
Tr = 298.15 #K #reference temperature
rhobh = 0.345 #g/cm3 #catalyst bulk density

#MDA
Rc = 101325*0.022414/273 #J/gmol.K #Gas constant
Poc = 1 #atm #initial pressure
Prefc = Poc * 101325 #Pa #reference pressure
Toc = 800 + 273 #K #initial temperature
rhobc = 0.510 #g/cm3 #catalyst bulk density`

Cell 2.2 General tube design parameters

In [8]: `l = 100 #cm #reactor length to design
ntubes = 1000 #number of reactor tubes`

```

lambdaw = 80/100 #J/cm.s.K #thermal conductivity of the wall for steel material
U       = 1200/10000 #W/m2.K #overall coefficient of heat transfer (division by 10000

```

Cell 2.3 Tube design parameters

In [9]:

```

#OCM
voht      = 10000 * (10**6)/3600 #cm3(STP)/s #inlet total volumetric flowrate
voh       = voht/ntubes #cm3(STP)/s #inlet volumetric flowrate per channel

w_h       = 0.12333*10**6 #g #catalyst weight
eps_gash  = 0.5 #gas #void fraction
eps_sh    = 1 - eps_gash #solid fraction
percent_dilh = 0 #percentage of diluent to catalyst within the solid fraction (this is
eps_cath  = eps_sh*(1-percent_dilh) #solid fraction *((solid fraction - diluent f
eps_diluenth = 1 - eps_gash - eps_cath # diluent percentage in total reactor (this is

vol_cat_particles = w_h/rhobh # volume of catalyst particles only
vol_Reac         = vol_cat_particles/eps_cath # volume of total reactor
vol_c            = eps_cath*vol_Reac # volume of catalyst only
vol_g            = eps_gash*vol_Reac # volume of gas only
vol_d            = eps_diluenth*vol_Reac # volume of diluent only
Vtot            = vol_c + vol_g + vol_d # total reactor volume by addition of gas+d

a_rh          = vol_Reac/l #cm2 reactor cross sectional area
d_rh          = 2*((a_rh/np.pi)**0.5) #cm #total reactor diameter
a_th          = a_rh/ntubes #cm2 #cross sectional area of one tube
d_th          = (2*((a_th/np.pi)**0.5)) #cm #tube diameter used in reaction kinetics
vol_th        = a_th*l #volume of one tube

#MDA
voct        = 72320* (10**6)/3600 #cm3(STP)/s total inlet flow rate
voc         = voct/ntubes #cm3(STP)/s inlet flow rate per channel

w_c         = 6.66667*10**6 #g #catalyst weight
eps_gasc    = 0.5 #gas void fraction
eps_sc      = 1 - eps_gasc #solid fraction
percent_dilc = 0 #percentage of diluent to catalyst within the solid fraction
eps_catc    = eps_sc*(1-percent_dilc) #solid fraction *((solid fraction - diluent
eps_diluentc = 1 - eps_gasc - eps_catc #diluent percentage in total reactor

vol_catc     = w_c/rhobc/eps_gasc #cm3 catalyst volume
vol_rc       = vol_catc/(1-eps_diluentc) #cm3 reactor volume based on new calculations

a_rc         = vol_rc/l #cm2 #reactor cross sectional area
d_rc         = 2*((a_rc/np.pi)**0.5) #cm #total reactor diameter
a_tc         = a_rc/ntubes #cm2 #cross sectional area of one tube
d_tc         = (2*((a_tc/np.pi)**0.5)) #cm #tube diameter used in reaction kinetics
vol_tc       = a_tc*l #volume of one tube

# design parameters
dw          = 0.5 #cm #thickness of tube wall
dtu         = dw + d_th #cm #used in heat transfer
d_tco       = dtu + d_tc #cm #total diameter of inner tube
isar        = np.pi * d_th * l #cm2 #heat exchange surface area inside
osar        = np.pi * dtu * l #cm2 #heat exchange surface area outside
lsar        = (osar - isar)/(np.log(osar/isar)) #cm2 #Log mean heat exchange surface

```

```

# OCM side
dph = 0.3 #cm #spherical particle diameter bed side
rph = dph/2 #cm #spherical particle radius bed side
volch = (4/3)*np.pi*(rph**3) #cm3 #volume of catalyst particle
uh = voh/a_th #cm3/s.cm2 reactor #superficial velocity
ghsv_h = voh/vol_th #Flow Rate of gas passing in the reactor/volume of catalyst

# MDA side
dpc = 0.3 #cm #spherical particle diameter heat exchanger side
rpc = dpc/2 #cm #spherical particle radius heat exchanger side
volcc = (4/3)*np.pi*(rpc**3) #cm3 #volume of catalyst particle
uc = voc/a_tc #cm3/s.cm2 reactor #superficial velocity
ghsv_c = voc/vol_tc #flow Rate of gas passing in the reactor/volume of catalyst

```

Cell 2.4 Inlet composition and molar flow rates

```

In [10]: #OCM
yCH4oh = (1-0.178297381)*3/4 #initial CH4 composition
yO2oh = (1-0.178297381)*1/4 #initial O2 composition
yH2Ooh = 0 #initial H2O composition
yC2H6oh = 0 #initial C2H6 composition
yCO2oh = 0 #initial CO2 composition
yHeoh = 0.178297381 #initial He composition

Ftotoh = voh/22414 #mol/s #initial molar flowrate per channel
FCH4oh = yCH4oh * Ftotoh #initial CH4 molar flowrate
FO2oh = yO2oh * Ftotoh #initial O2 flowrate
FH2Ooh = yH2Ooh * Ftotoh #initial H2O flowrate
FC2H6oh = yC2H6oh * Ftotoh #initial C2H6 composition
FCO2oh = yCO2oh * Ftotoh #initial CO2 composition
FHeoh = yHeoh * Ftotoh #initial He composition

#MDA
yCH4oc = 0.95 #initial CH4 composition
yHeoc = 1 - yCH4oc #initial He composition
yC2H4oc = 0 #initial C2H4 composition
yC6H6oc = 0 #initial C6H6 composition
yC10H8oc = 0 #initial C10H8 composition
yH2oc = 0 #initial H2 composition

Ftotoc = voc/22414 #mol/s #initial molar flowrate per channel
FCH4oc = yCH4oc * Ftotoc #initial CH4 molar flowrate
FHeoc = yHeoc * Ftotoc #initial He flowrate

```

Cell 2.5 Defining chemical names for thermodynamic properties

```

In [11]: #OCM
methh = Chemical('methane', Toh, Prefh)
oxyh = Chemical('oxygen', Toh, Prefh)
carbdh = Chemical('carbon dioxide', Toh, Prefh)
ethah = Chemical('ethane', Toh, Prefh)
wath = Chemical('water', Toh, Prefh)
helh = Chemical('helium', Toh, Prefh)
mh = Mixture(['methane', 'oxygen', 'carbon dioxide', 'ethane', 'water', 'helium'],

```

```

#MDA
methc = Chemical('methane', Toc, Prefc)
ethc  = Chemical ('ethylene', Toc, Prefc)
benzc = Chemical ('benzene', Toc, Prefc)
naphc = Chemical ('naphthalene', Toc, Prefc)
hydc  = Chemical ('hydrogen', Toc, Prefc)
helc  = Chemical ('helium', Toc, Prefc)
mc    = Mixture(['methane', 'ethylene', 'benzene', 'naphthalene', 'hydrogen', 'helium

```

Cell 2.6 Heat of formation

```

In [12]: #OCM
mHfh    = methh.Hf #J/mol
oHfh    = 0 #J/mol #zero since pure component
cdHfh   = carbdh.Hf #J/mol
eaHfh   = ethah.Hf #J/mol
wHfh    = wath.Hf #J/mol
heHfh   = 0 #J/mol

#MDA
mHfc    = methc.Hf #J/mol
eHfc    = ethc.Hf #J/mol
bHfc    = benzc.Hf #J/mol
nHfc    = naphc.Hf #J/mol
hHfc    = 0 # #J/mol
heHfc   = 0 #J/mol

```

Cell 2.7 Specific heat

```

In [13]: #OCM
mCph    = methh.Cpm #J/mol.K
oCph    = oxyh.Cpm #J/mol.K
cdCph   = carbdh.Cpm #J/mol.K
eaCph   = ethah.Cpm #J/mol.K
wCph    = wath.Cpm #J/mol.K
heCph   = helh.Cpm #J/mol.K

#MDA
mCpc    = methc.Cpm #J/mol.K
eCpc    = ethc.Cpm #J/mol.K
bCpc    = benzc.Cpm #J/mol.K
nCpc    = naphc.Cpm #J/mol.K
hCpc    = hydc.Cpm #J/mol.K
heCpc   = helc.Cpm #J/mol.K

```

Cell 2.8 Gas mixture physical properties

```

In [14]: #OCM
meuh    = mh.mu * 10 #Pa.s to g/cm.s #viscosity
rhoh    = mh.rho * 0.001 #kg/m3 to g/cm3 #density
Cph     = mh.Cpm #J/mol.K #specific heat
Reh     = dph*rhoh*uh/meuh #reynold's number
Cphn    = mh.Cp/1000 #J/g.K #specific heat
lembdah = (mh.k)/100 #J/cm.s.K #thermal conductivity of the bed fluid
Prh     = Cphn * meuh/lembdah #prandtl number

```

```

#MDA
meuc    = mc.mu * 10 #Pa.s to g/cm.s #viscosity
rhoc    = mc.rho * 0.001 #kg/m3 to g/cm3 #density
Cpc     = mc.Cpm #J/mol.K #specific heat
Rec     = dpc*rhoc*uc/meuc #reynold's number
Cpcn    = mc.Cp/1000 #J/g.K #specific heat
lmbdac  = (mc.k)/100 #J/cm.s.K #thermal conductivity of the bed fluid
Prc     = Cpcn * meuc/lmbdac #prandtl number

```

Cell 2.9 Model simulation parameters

```

In [15]: n          = 400 #number of iterations for the model simulation
         z1         = np.linspace(0, 1, n) #cm #catalyst bed length points
         gheatc, rheatex, gheatc, zed, epch, epdh, epgh, epcc, epdc, epgc = [], [], [], [], [], [

```

Cell 2.10 Reactor model

```

In [16]: #define reactor model
         def model (F,z):

         #####

         #statements to make sure molar flow rates can not be smaller than zero
         if F[0] < 0:
             F[0] = 0
         if F[1] < 0:
             F[1] = 0
         if F[2] < 0:
             F[2] = 0
         if F[3] < 0:
             F[3] = 0
         if F[4] < 0:
             F[4] = 0
         if F[5] < 0:
             F[5] = 0
         if F[6] < 0:
             F[6] = 0
         if F[7] < 0:
             F[7] = 0
         if F[8] < 0:
             F[8] = 0
         if F[9] < 0:
             F[9] = 0
         if F[10] < 0:
             F[10] = 0
         if F[11] < 0:
             F[11] = 0
         if F[12] < 0:
             F[12] = 0
         if F[13] < 0:
             F[13] = 0
         if F[14] < 0:
             F[14] = 0
         if F[15] < 0:
             F[15] = 0

```

#statements to make sure no nan values in the solution

```
F[1] = np.where(np.isnan(F[1]), 0, F[1])
F[2] = np.where(np.isnan(F[2]), 0, F[2])
F[3] = np.where(np.isnan(F[3]), 0, F[3])
F[4] = np.where(np.isnan(F[4]), 0, F[4])
F[5] = np.where(np.isnan(F[5]), 0, F[5])
F[6] = np.where(np.isnan(F[6]), 0, F[6])
F[7] = np.where(np.isnan(F[7]), 0, F[7])
F[8] = np.where(np.isnan(F[8]), 0, F[8])
F[9] = np.where(np.isnan(F[9]), 0, F[9])
F[10] = np.where(np.isnan(F[10]), 0, F[10])
F[11] = np.where(np.isnan(F[11]), 0, F[11])
F[12] = np.where(np.isnan(F[12]), 0, F[12])
F[13] = np.where(np.isnan(F[13]), 0, F[13])
F[14] = np.where(np.isnan(F[14]), 0, F[14])
F[15] = np.where(np.isnan(F[15]), 0, F[15])
```

#####

#OCM

#constants for rate equation

```
K1o = 2.472 * 10**7 * np.exp(-49.64/(Rh*Toh)) #Ea units (kcal/mol)
K2o = 10.10 * np.exp(-23.15/(Rh*Toh)) #Ea units (kcal/mol)
K3o = 1.103 * 10**-3 * np.exp(-4.548/(Rh*Toh)) #Ea units (kcal/mol)
K4o = 2.093 * 10**-4 * np.exp(27.94/(Rh*Toh)) #Ea units (kcal/mol)

K1 = K1o * np.exp((-49.64/Rh)*((1/F[12])-(1/Toh))) #Ea units (kcal/mol)
K2 = K2o * np.exp((-23.15/Rh)*((1/F[12])-(1/Toh))) #Ea units (kcal/mol)
K3 = K3o * np.exp((-4.548/Rh)*((1/F[12])-(1/Toh))) #Ea units (kcal/mol)
K4 = K4o * np.exp((27.94/Rh)*((1/F[12])-(1/Toh))) #Ea units (kcal/mol)
```

#total flowrate

```
FTh = F[0]+F[1]+F[2]+F[3]+F[4]+F[5] #mol/s
vh = FTh * 22414 #cm/s #total velocity
```

#compositions

```
yCH4h = F[0]/FTh #CH4
yO2h = F[1]/FTh #O2
yCO2h = F[2]/FTh #CO2
yC2H6h = F[3]/FTh #C2H6
yH2Oh = F[4]/FTh #H2O
yHeh = F[5]/FTh #He
```

#partial pressures

```
pCH4h = F[14] * yCH4h #atm #CH4
pO2h = F[14] * yO2h #atm #O2
pCO2h = F[14] * yCO2h #atm #CO2
pC2h = F[14] * yC2H6h #atm #C2H6
pH2Oh = F[14] * yH2Oh #atm #O2
pHeh = F[14] * yHeh #atm #He
```

#reactions #derived from stoichiometry of the rate equations

```
#step 1: CH4 + 2O2 -> CO2 + 2H2O
#step 2: 2CH4 + 0.5O2 -> C2H6 + H2O
```

#net rate Equations

#rate parameters

```
Z = (K1 * ((pO2h)**0.5)) / ((K1 * ((pO2h)**0.5)) + (K1 * K2 * K4) + (K2 * p
So = 2 / (((1 + (8 * Z * ((K2 * pCH4h))/ (K3 * ((pO2h)**1.251)))) ** 0.5) +
CPCT = (K1 * (pO2h ** 0.5)) / ((K1 * (pO2h ** 0.5)) + (K1 * K2 * K4) + (K2 * (
```

```

#rate equations
frac = vol_c/l/ntubes #FRACTION needed for calculating OCM rate of reactio
r1h = frac * ((K3 * (pO2h**1.251))/4)*(((1 + ((8 * K2 * (CPCT) * pCH4h) / (K
r2h = frac * ((K3 * (pO2h**1.251))/16)*(((1 + ((8 * K2 * (CPCT) * pCH4h) /

#delHro
delHro1h = (cdHfh + (2*wHfh)) - (mHfh + (2*oHfh)) #J/mol carbon dioxide
delHro2h = (eaHfh + (wHfh)) - ((2*mHfh) + (0.5*oHfh)) #J/mol ethane

SFCph = (F[0]*mCph) + (F[1]*oCph) + (F[2]*cdCph) + (F[3]*eaCph) + (F[4]*wCph) +

#delCp
delCpr1h = (cdCph + (2*wCph)) - (mCph + (2*oCph)) #J/mol carbon dioxide
delCpr2h = (eaCph + (wCph)) - ((2*mCph) + (0.5*oCph)) #J/mol ethane

#delHr
delHr1h = delHro1h + (delCpr1h*(F[12]-Tr)) #J/mol carbon dioxide
delHr2h = delHro2h + (delCpr2h*(F[12]-Tr)) #J/mol ethane

#####

#MDA
#constants for rate equation
A1 = 500.3 #mole, h, g cat, atm
A2 = 7.837 #mole, h, g cat, atm
A3 = 0.420 #mole, h, g cat, atm

Ea1 = 65.58 * 1000 #J/mol
Ea2 = 30.84 * 1000 #J/mol
Ea3 = -19.74 * 1000 #J/mol

Kp1 = 3.219*10**-5 * np.exp(4.4184 * (49.92*10**3/ Rc) * ((1/973) - (1/F[13]))
Kp2 = 1.478*10**5 * np.exp(4.4184 * (-13.978*10**3/ Rc) * ((1/973) - (1/F[13]))
Kp3 = 9.985*10**3 * np.exp(4.4184 * (-4.485*10**3/ Rc) * ((1/973) - (1/F[13]))

kf1o = A1 * np.exp(-Ea1/(Rc*Toc)) #mole, h, g cat, atm
kf2o = A2 * np.exp(-Ea2/(Rc*Toc)) #mole, h, g cat, atm
kf3o = A3 * np.exp(-Ea3/(Rc*Toc)) #mole, h, g cat, atm

kf1 = kf1o * np.exp((-Ea1/Rc)*((1/F[13])-(1/Toc))) #mole, h, g cat, atm
kf2 = kf2o * np.exp((-Ea2/Rc)*((1/F[13])-(1/Toc))) #mole, h, g cat, atm
kf3 = kf3o * np.exp((-Ea3/Rc)*((1/F[13])-(1/Toc))) #mole, h, g cat, atm

#total flowrate
FTc = F[6]+F[7]+F[8]+F[9]+F[10]+F[11] #mol/s
vc = FTc * 22414 #cm/s #velocity

#compositions
yCH4c = F[6]/FTc #CH4
yC2H4c = F[7]/FTc #C2H4
yC6H6c = F[8]/FTc #C6H6
yC10H8c = F[9]/FTc #C10H8
yH2c = F[10]/FTc #H2
yHec = F[11]/FTc #He

#partial pressures
pCH4c = F[15] * yCH4c #atm #CH4

```



```

pC2H4c    = F[15] * yC2H4c #atm #C2H4
pC6H6c    = F[15] * yC6H6c #atm #C6H6
pC10H8c   = F[15] * yC10H8c #atm #C10H8
pH2c      = F[15] * yH2c #atm #H2
pHec      = F[15] * yHec #atm #He

#reactions
#Step 1: 2CH4 <-> C2H4 + 2H2
#Step 2: 3C2H4 <-> C6H6 + 3H2
#Step 3: C6H6 + 2C2H4 <-> C10H8 + 3H2

#Rate Equations
n1        = (pC2H4c*pH2c**2) / (10**-6+((pCH4c**2)*Kp1))
n2        = (pC6H6c*pH2c**3) / (10**-6+((pC2H4c**3)*Kp2))
n3        = (pC10H8c*pH2c**3) / (10**-6+(pC6H6c*(pC2H4c**2)*Kp3))

r1c      = (eps_catc) * rhobc * a_tc * kf1 * pCH4c * (1-n1)/3600 #mol/cm.s
r2c      = (eps_catc) * rhobc * a_tc * kf2 * pC2H4c * (1-n2)/3600 #mol/cm.s
r3c      = (eps_catc) * rhobc * a_tc * kf3 * pC2H4c * pC6H6c * (1-n3)/3600 #mol/cm.

#delHro
delHro1c = (eHfc + (2*hHfc)) - (2*mHfc) #J/mol ethylene
delHro2c = (bHfc + (3*hHfc)) - (3*eHfc) #J/mol benzene
delHro3c = (nHfc + (3*hHfc)) - (bHfc + (2*eHfc)) #J/mol naphthalene

SFCpc    = (F[6]*mCpc) + (F[7]*eCpc) + (F[8]*bCpc) + (F[9]*nCpc) + (F[10]*hCpc) + (

#delCp
delCpr1c = (eCpc + (2*hCpc)) - (2*mCpc) #J/mol.K
delCpr2c = (bCpc + (3*hCpc)) - (3*eCpc) #J/mol.K
delCpr3c = (nCpc + (3*hCpc)) - (bCpc + (2*eCpc)) #J/mol.K

#delHr
delHr1c  = delHro1c + (delCpr1c*(F[13]-Tr)) #J/mol ethylene
delHr2c  = delHro2c + (delCpr2c*(F[13]-Tr)) #J/mol benzene
delHr3c  = delHro3c + (delCpr3c*(F[13]-Tr)) #J/mol naphthalene

#####

#heat balance
Qgh      = (-r1h * delHr1h) + (-r2h * delHr2h) #J/cm.s
Qex      = (U*np.pi*dtu)*(F[12]-F[13]) #J/cm.s #(Uh*a*Ah)
Qgc      = (-r1c * delHr1c) + (-r2c * delHr2c) + (-r3c * delHr3c) #J/cm.s

#net rates
#OCM
dFch4hdz = -(r1h + (2*r2h)) #mol/cm.s
dFo2hdz   = -((2*r1h) + (0.5*r2h)) #mol/cm.s
dFco2hdz  = (r1h) #mol/cm.s
dFc2h6hdz = (r2h) #mol/cm.s
dFh2ohdz  = ((2*r1h) + (r2h)) #mol/cm.s
dFhehdz   = 0 #mol/cm.s

#MDA
dFch4cdz  = -2*r1c # mol/cm.s
dFc2h4cdz = r1c - (3*r2c) - (2*r3c) #mol/cm.s
dFc6h6cdz = r2c - r3c #mol/cm.s
dFc10h8cdz = r3c #mol/cm.s
dFh2cdz   = (2*r1c) + (3*r2c) + (3*r3c) #mol/cm.s
dFhecdz   = 0 #mol/cm.s

```

```

#temperature profile
dThdz      = (Qgh - Qex) / SFCph #negative for exothermic
dTcdz      = (Qgc + Qex) / SFCpc #positive for endothermic

#pressure profile
dphdz      = -((1-eps_gash)*uh/(dph*eps_gash**3))*((150*meuh*(1-eps_gash)/dph)+(1.75
dpcdz      = -((1-eps_gasc)*uc/(dpc*eps_gasc**3))*((150*meuc*(1-eps_gasc)/dpc)+(1.75

#flowrate profile
dFdz       = [dFch4hdz, dFo2hdz, dFco2hdz, dFc2h6hdz, dFh2ohdz, dFhehdz, dFch4cdz, d

#appending values for result outputs
gheath.append(Qgh)
gheatc.append(Qgc/3600)
rheatex.append(Qex/3600)
zed.append(z)
epch.append(eps_cath)
epdh.append(eps_diluenth)
epgh.append(eps_gash)
epcc.append(eps_catc)
epdc.append(eps_diluentc)
epgc.append(eps_gasc)

#return model values
return dFdz

```

Cell 2.11 Solve reactor model

```

In [17]: F0      = [FCH4oh, F02oh, 0, 0, 0, FHeoh, FCH4oc, 0, 0, 0, 0, FHeoc, Toh, Toc, Poh, Po
F1      = odeint(model,F0,z1) #reactor model

```

Cell 2.12 Reactor outputs

```

In [18]: #OCM
x_ch4h   = 100*(FCH4oh-F1[-1,0])/FCH4oh %% #CH4 conversion
mconvh   = 100*(FCH4oh-F1[:,0]) / FCH4oh %% #CH4 conversion
x_o2h    = 100*(F02oh-F1[-1,1])/F02oh %% #O2 conversion
oconvh   = 100*(F02oh-F1[:,1]) / F02oh %% #O2 conversion %
s_c2h    = 100 * (2*F1[-1,3])/(F1[0,0]-F1[-1,0]) %% #C2 selectivity
c2sh     = 100 * (2*F1[1:,3])/(F1[0,0]-F1[1:,0]) %% #C2 selectivity
y_c2h    = x_ch4h * s_c2h/100 %% #C2 yield
c2yh     = x_ch4h * c2sh/100 %% #C2 yield
del1Ph   = 100*(Poh-F1[-1,14])/Poh %% #pressure drop
Thpeak   = max(F1[:,12]) - Toh #C #temperature peak
Thlower  = Toh - min(F1[:,12]) #C #temperature dip
sdth     = st.pstdev(F1[:,12]) #measures the amount of variation or dispersion of a set

#MDA
x_ch4c   = 100*(FCH4oc-F1[-1,6])/FCH4oc %% #CH4 conversion
mconvc   = 100*(FCH4oc-F1[:,6]) / FCH4oc %% #CH4 conversion
s_c6c    = 100 * (2*F1[-1,8])/(F1[0,6]-F1[-1,6]) %% #C6 selectivity
c6sc     = 100 * (2*F1[1:,8])/(F1[0,6]-F1[1:,6]) %% #C6 selectivity
y_c6c    = x_ch4c * s_c6c/100 %% #C6 yield
c6yc     = x_ch4c * c6sc/100 %% #C6 yield
del1Pc   = 100*(Poc-F1[-1,15])/Poc %% #pressure drop
Tcpeak   = max(F1[:,13]) - Toc #C #temperature peak

```

```
Tclower = Toc - min(F1[:,13]) #C #temperature dip
sdctc = st.pstdev(F1[:,13]) #measures the amount of variation or dispersion of a set
```

Cell 2.13 Printing reactor outputs

```
In [19]: print('eps_cath', eps_cath, 'eps_catc', eps_catc, 'dph', '%.1f' %(dph*10), 'dpc', '%.1f'
print('d_th', '%.1f' %d_th, 'd_tc', '%.1f' %d_tc, 'd_tco', '%.1f' %d_tco, 'len', '%.1f'
print('delp_h %', '%.3f' %delPh, 'delp_c %', '%.3f' %delPc)
print('X_CH4 ', '%.1f' %x_ch4h, 'X_O2 ', '%.1f' %x_o2h, 'S_C2 ', '%.1f' %s_c2h, 'Y_C2 ',
print('X_CH4 ', '%.1f' %x_ch4c, 'S_C6 ', '%.1f' %s_c6c, 'Y_C6 ', '%.1f' %y_c6c)
print('Tpeak_H ', '%.1f' %Thpeak, 'Tlower_H ', '%.1f' %Thlower, 'Tstd_H ', '%.1f' %stdh,
print('Tpeak_C ', '%.1f' %Tcpeak, 'Tlower_C ', '%.1f' %Tclower, 'Tstd_C ', '%.1f' %stdc,
print('eps_diluenth', '%.3f' %eps_diluenth)
```

```
eps_cath 0.5 eps_catc 0.5 dph 3.0 dpc 3.0 d_rh 1.0 d_rc 5.8
d_th 3.0 d_tc 18.2 d_tco 21.8 len 100.0 tubes 1000
delp_h % 13.643 delp_c % 0.947
X_CH4 52.8 X_O2 100.0 S_C2 78.2 Y_C2 41.3 Uov1 1200.0
X_CH4 11.1 S_C6 18.4 Y_C6 2.0
Tpeak_H 84.3 Tlower_H 0.0 Tstd_H 20.7 ghsv_h 13987 sTh 0.3 uh 388.5
Tpeak_C 9.3 Tlower_C 60.3 Tstd_C 23.4 ghsv_c 2766 sTc 1.3 uc 76.8
eps_diluenth 0.000
```

Cell 2.14 Plotting simulation results

```
In [20]: #pressure across the catalyst bed
plt.plot(z1/100,F1[:,14], '-', color='darkgray', label = r'OCM')
plt.plot(z1/100,F1[:,15], '--', color='dimgray', label = r'MDA')
plt.ylabel('Pressure, atm')
plt.xlabel('Catalyst bed length, m')
plt.grid(alpha=0.5)
plt.legend(loc='best')
plt.rcParams["figure.figsize"]=(8,5)
plt.show()

#temperature across the catalyst bed
plt.plot(z1/100,F1[:,12], '-', color='darkgray', label = r'OCM')
plt.plot(z1/100,F1[:,13], '--', color='dimgray', label = r'MDA')
plt.ylabel('Temperature, K')
plt.xlabel('Catalyst bed length, m')
plt.grid(alpha=0.5)
plt.legend(loc='upper right')
plt.rcParams["figure.figsize"]=(8,5)
plt.show()

#reactor performance % across the catalyst bed
plt.plot(z1/100,mconvh, '-', color='darkgray', label = r'OCM CH4 conversion')
plt.plot(z1/100,mconvc, ':', color='dimgray', label = r'MDA CH4 conversion')
plt.plot(z1[1:]/100,c2yh, '-.', color='darkgray', label = r'OCM C2 yield')
plt.plot(z1[1:]/100,c6yc, '--', color='dimgray', label = r'MDA C6 yield')
plt.ylabel('Reactor performance, %')
plt.xlabel('Catalyst bed length, m')
plt.grid(alpha=0.5)
plt.legend(loc='upper left')
plt.rcParams["figure.figsize"]=(8,5)
plt.show()

#solid fraction across OCM bed
```

```

plt.plot(np.array(zed)/100, np.multiply(epch,2), '-', color='darkgray', label = r'Catal')
plt.plot(np.array(zed)/100, np.multiply(epdh,2), ':', color='dimgray', label = r'Dilue')
plt.ylim(0,1)
plt.ylabel('Solid fraction')
plt.xlabel('OCM Catalyst bed length, m')
plt.grid(alpha=0.5)
plt.legend(loc='best')
plt.rcParams["figure.figsize"]=(8,5)
plt.show()

```

#solid fraction across MDA bed

```

plt.plot(np.array(zed)/100, np.multiply(epcc,2), '-', color='darkgray', label = r'Catal')
plt.plot(np.array(zed)/100, np.multiply(epdc,2), ':', color='dimgray', label = r'Diluen')
plt.ylim(0,1)
plt.ylabel('Solid fraction')
plt.xlabel('MDA Catalyst bed length, m')
plt.grid(alpha=0.5)
plt.legend(loc='best')
plt.rcParams["figure.figsize"]=(8,5)
plt.show()

```





