

Research Article

Simultaneous Planning of the Medium and Low Voltage Distribution Networks under Uncertainty: A Bi-Level Optimization Approach

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Received 18 April 2022; Revised 2 July 2022; Accepted 2 September 2022; Published 28 September 2022

Academic Editor: Murthy Cherukuri

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Distribution network expansion planning (DNEP) is one of the important matters in the field of planning and operation of electrical power systems. Since many costs and losses have occurred in the distribution networks, it has increased attention towards this network. The electrical energy distribution network is divided into two parts: the medium voltage (MV) network and the low voltage (LV) network. The main problem in this field is that planning is done either only on the MV network or only on the LV network. While planning in each of these networks has a significant effect on the other networks, this important case has not been considered in most research studies. Therefore, this study has tried to do integrated planning in the form of a bi-level model in the presence of different types of distributed generations (DGs) and consider the uncertainties of renewable sources and load demand in both MV and LV networks so that the planning and operation costs are minimized. In the proposed bi-level model, the upper-level section aims to minimize the investment and the operation cost of the MV network, and the lower-level problem minimizes the investment and the operation cost of the LV network considering the DGs and pollution emission. The obtained results show the effectiveness of the proposed model.

1. Introduction

1.1. Motivation and Aim. The distribution network expansion planning (DNEP) problem is one of the most important issues in the power system planning with the aim of supplying the distribution network's demand through specifying the location and capacity of distribution substations, distribution transformers, and feeders. This problem can be expressed in two ways: expansion planning and reinforcement planning. In the expansion planning problem, the planner selects new rights of ways (feeders) or locations and the capacity for new distribution substations and distributed generations (DGs). In the reinforcement problem, the network is reinforced in some feeders. The DNEP problem can be considered in both medium-voltage (MV) and low-voltage (LV) distribution networks.

In this study, the applied model uses the contradictions that exist in the planning of both MV and LV networks in such a way that each of the MV and LV network, from their point of view, may suggest a specific location and capacity for distribution transformers, and therefore, this view may not be appropriate for another network perspective. Therefore, by using a bi-level model, an attempt has been made to propose a location and capacity for distribution transformers that are acceptable from the point of view of each network. The applied model considers the MV network at the upper level (UL) and LV network planning at the low-level (LL) of the bi-level model. The applied problem is described in Figure 1. The objective of the UL problem is to determine the best decisions about the distribution substations and MV feeders to meet the demand of the system with the minimum investment and operation cost. The LL problem aims to minimize the total cost of the LV system

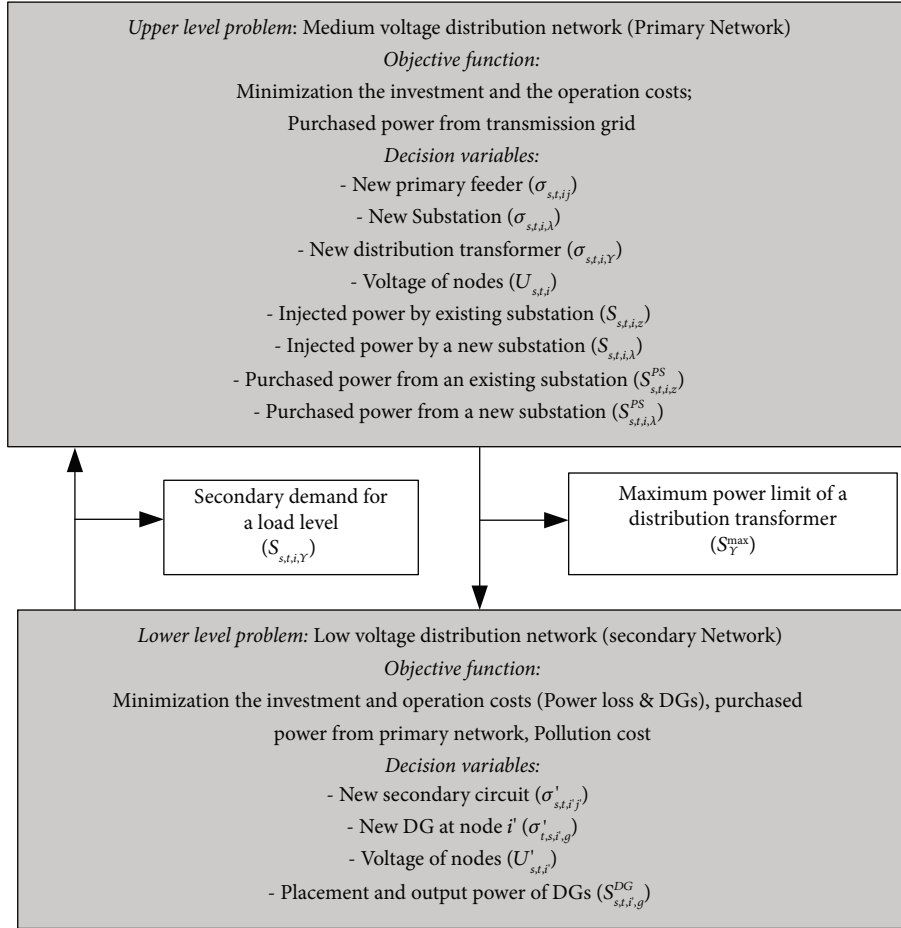


FIGURE 1: The structure of the proposed bi-level optimization framework.

considering the cost of the pollution emissions and the power loss of the network. The general basis of the work is based on the fact that first a location and capacity for the distribution transformers are proposed (S_{γ}^{\max}) by the UL problem, and then, in the LL model, the power injected into the distribution transformers ($S_{s,t,i,\gamma}$) is determined by the demand and the specifications of the DGs. This variable is sent to the UL problem to update the optimal decisions at this level if needed. If the constraints of the problem are not met at any level, then the capacity of the distribution transformers must be changed within the allowed range and the problem will be re-examined. This process continues until an optimal point is reached.

1.2. Literature Review and Contributions. Most previous DNEP studies have been done at the MV level. In [1], an optimal power flow approach is developed to model the DGs in the optimal planning problem of the MV distribution networks. In [2], the reliability of the MV networks increases in the planning problem in the presence of the DGs and storage units. The DNEP problem of the MV networks is mathematically formulated as a multiobjective planning

model in which the first and second objectives aim to improve the costs and reliability, respectively [3]. In [4], a mixed-integer linear programming (MILP) model is proposed to minimize the annualized investment and operation costs by installing new circuits, upgrading existing circuits, and installing capacitor banks in the MV network. The DNEP problem in the MV networks in the presence of DGs is investigated considering the uncertainties of the demand and energy price in [5]. In [6], a new approach is presented for the loss allocation in an MV distribution system in the presence of different models of DGs. A hybrid evolutionary algorithm is proposed to optimize the planning of the DGs in MV networks in [7] to improve the power loss and voltage stability index. In [8], a metaheuristic approach is proposed based on grey wolf optimizer (GWO) and particle swarm optimization (PSO) for the optimal DNP in the MV side, considering DGs and a battery storage system (BSS). In [9], a new approach to the DNEP problem in the MV network under uncertainty in the presence of wind energy is proposed to improve the reliability index. In [10], an MILP model is proposed for the DNEP problem, which chooses a set of candidate feeders with a minimum cost with specified reliability. The DNP problem is formulated in [11] as a

TABLE 1: Relevant features of studies reported in the literature and the model of this paper.

Ref.	Year	Model	Uncertainty	Type of DGs	Losses	Pollution	Network	Power purchased	Structure	Objective
[1]	2012	Dynamic	×	×	✓	×	MV	×	SO *	Cost
[2]	2013	Static	×	In general	✓	×	MV	×	SO	Cost
[3]	2014	Static	×	×	✓	×	MV	×	MO [†]	Cost reliability
[4]	2015	Static	×	×	✓	×	MV	×	SO	Cost
[5]	2015	Dynamic	Demand	In general	✓	×	MV	×	SO	Cost
[6]	2016	Static	×	In general	✓	×	MV	×	SO	Loss
[7]	2017	Static	×	×	✓	×	MV	×	MO	Loss-voltage index
[8]	2017	Static	×	×	×	×	MV	×	MO	Cost reliability
[9]	2020	Static	Demand	Wind	✓	×	MV	×	SO	Reliability
[10]	2020	Static	×	×	✓	×	MV	×	SO	Cost reliability
[11]	2020	Dynamic	DGs	×	✓	×	MV	×	MSP [#]	Cost
[12]	2020	Dynamic	Wind speed	Wind	✓	×	MV	×	SO	Min risk
[13]	2020	Dynamic	Demand RESs	PV	✓	×	MV	×	Bi-level	Cost
[14]	2021	Dynamic	Photovoltaic	PV	✓	×	MV	×	SO	Cost
[15]	2021	Dynamic	Demand	PV/wind	×	×	MV	×	SO	Cost
[16]	2021	Dynamic	Demand RESs	PV/wind	×	✓	MV	×	MO	Cost pollution
[17]	2021	Static	×	×	×	×	MV-LV	×	SO	Reliability
[18]	2022	Dynamic	Demand RESs	PV/wind	×	✓	MV	✓	SO	Cost
[19]	2022	Static	RESs	PV/wind	×	×	MV	×	SO	Capacity
[20]	2013	Dynamic	×	In general	✓	×	LV	×	SO	Cost
[21]	2016	Static	×	In general	×	×	LV	×	SO	Cost
[22]	2018	Dynamic	×	PV	✓	✓	LV	×	SO	Cost
[23]	2015	Dynamic	Demand-RESs energy price	Wind	✓	×	MV	×	SO	Cost reliability
[24]	2016	Static	×	In general	✓	×	Integrated	×	SO	Cost
[25]	2020	Static	Demand RESs	Wind	✓	✓	Integrated	×	MO	Cost
[26]	2019	Static	×	In general	✓	×	Integrated	×	Bi-level	Cost
This paper		Dynamic	Demand RESs	Wind/PV/GT/MT/FC/DE	✓	✓	Integrated	✓	Bi-level	Cost pollution

*, single objective; †, multiobjective; #, multistage stochastic programming.

multistage stochastic programming (MSP) approach considering the uncertainty of DGs. The objective function of this model is to minimize the planning costs subject to the operation and the investment constraints. A stochastic risk-based method is developed in [12] for the resilient DNP problem to model the uncertainties of wind energy, demand, storm duration, and fragility of the system components. In [13], the DENP problem is considered at the MV level in the presence of BSSs and photovoltaic (PV) arrays and uncertainty of the demand. In [14], a mixed-integer second-order con programming is proposed for the DNEP problem at the MV level that tries to search for the optimal decisions for transformer and feeder upgrades and also for PV and BSS. In [15], a flexible multistage planning approach for the DNEP is proposed, and the planning problem is formulated based on the Markov decision process for the MV network. In [16], a multiobjective model for DNEP is proposed in the MV network. Two conflicting objective functions are considered: costs vs. CO₂ emissions, and then, scenario reduction is applied within a two-stage stochastic formulation. In [17], a

new approach for the DNEP problem based on geographic information systems (GIS) is proposed for MV and LV networks, independently. The proposed approach combines Delaunay Triangulation with a MILP model. In [18], a new approach based on spanning tree to solve the expansion of lines and allocation of DGs considering the uncertainty of load demand and RESs is proposed for the MV distribution network. In [19], an improved particle swarm optimization algorithm based on particle swarm optimization for adaptive improvement is proposed for the DNEP problem in the MV part, in which the feasibility and superiority of the algorithm are illustrated.

A few DNEP studies have been done at the LV level. The power loss and reliability of the LV networks improved in the DNP problem considering the DGs in [20]. In [21], new planning principles are described for rural LV networks considering DGs to minimize total costs. In [22], optimal sizing, sitting, and scheduling of BSSs are calculated in an LV distribution system. Some studies investigated the DNEP problem for both the MV and LV (integrated) networks. In

[23], by determining the reinforcement of existing lines and substations, an integrated methodology is proposed for the DNEP problem, in which the objective function is to maximize the reliability of the network. In [24], a single objective function is presented which minimizes the cost of LV circuits, MV substations, MV DGs, MV circuits, and high voltage substations where the problem is solved by the imperialist competitive algorithm (ICA). In [25], a multi-objective mixed-integer nonlinear programming (MINLP) is proposed for the integrated DNEP problem, which tries to minimize the investment cost of feeder routing and substation alternations while maximizing the utilization of the proposed charging stations. The reviewed studies until now are compared with each other in Table 1.

Due to the nonlinear nature of the DNEP problem, many heuristic and metaheuristic methods have been used to investigate this problem, for example, genetic algorithm (GA) [23], particle swarm optimization (PSO) [5, 27, 28], tabu search (TS) [26], harmony search algorithm (HSA) [29–31], imperialist competitive algorithm (ICA) [24, 32], grey wolf optimizer (GWO) [8], firefly algorithm (FA) [33], strength Pareto evolutionary algorithm (SPEA) [34], simulated annealing (SA) [35], perturbation mechanism [36], pseudodynamic programming technique [37], artificial immune systems (AIS) [38], clonal selection algorithm [39], shuffled frog leaping (SFL) [40], and artificial bee colony (ABC) [41]. It should be noted that this problem can be solved using the solution methods available in [42, 43]. The noteworthy point in the mentioned approaches is that planning has been done only at one level of the distribution network, while in the model presented in this study, planning is done simultaneously at both levels of the MV and LV distribution networks.

The main gaps concluded from the previous studies are as follows:

- (i) Although the DNEP problem of the MV and the LV networks should be modeled simultaneously, this issue is only addressed in a few studies [24–26].
- (ii) Determining the location and the size of the distribution transformers is the common decision between the DNEP problems of the MV and LV networks. Therefore, when the DNEP problem is modeled for both the MV and LV networks (integrated), the effect of the decisions in both networks on the location and the size of distribution transformers should be considered. This is considered only in [26].
- (iii) Although modeling the pollution emissions of the nonrenewable DGs and the main grid can change the output decisions of the DNEP problem in the presence of renewable-based DGs, this issue is not considered in [26]. Also, modeling the uncertainties of the demand and the output power of RESs is not investigated in [26].

It needs to be said that power system planning studies are always done in two phases or two steps. In the first phase, with the help of simplified mathematical equations, a general model for network modeling is expressed, in which the program execution time does not matter. In the first phase, the obtained answers are saved. In the second step, the obtained answers in the first step are analyzed in more detail, including reliability and short-circuit studies. What is done in this study and in most studies in this field is in the first phase of planning.

The DNEP problem of the MV network is modeled as an upper-level (UL) problem in which the obtained size and location of the distribution transformers are sent to the lower-level (LL) problem. Then, the DNEP problem of the LV network considering the different DGs, the pollution emissions and the uncertainties are formulated in the LL problem. This problem is optimized by considering the size and location of the distribution transformers obtained in the UL problem. The optimum power injected into the distribution transformers obtained in this stage is sent to the UL problem. In the following, the main problem will be solved using the genetic algorithm (GA) with special coding and division of the model into several subproblems.

For this study, the main contributions are as follows:

- (1) Modeling the DNEP problem of both MV and LV networks, simultaneously considering the uncertainties of the demand and RESs using a bi-level model
- (2) Considering the amount of energy purchased from each upstream grid
- (3) Modeling the pollution emission in the objective function of the LV model
- (4) Applying the GA to solve the proposed bi-level model

1.3. Paper Organization. The mathematical model is presented in Section 2. Modeling and handling the uncertainties are presented in Section 3. A solution approach is presented in Section 4. A numerical study is reported and discussed in Section 5, and finally, the conclusions are given in Section 6.

2. Mathematical Model

2.1. UL Model. The objective function of the UL problem is composed of five terms as follows:

$$MVC_s = \sum_{s \in \Lambda_s} \delta_s \sum_{f=1}^5 F_f, \quad (1)$$

where

$$\begin{aligned}
F_1 &= \sum_{t \in T} \sum_{\substack{i, j \in \Lambda_B \\ i \neq j}} \left(\left(\frac{1}{1+d} \right)^t \times C_{ij} \times \sigma_{s,t,ij} \right), \\
F_2 &= \sum_{t \in T} \sum_{i \in \Lambda_B} \sum_{\lambda \in \Lambda_\lambda} \left(\left(\frac{1}{1+d} \right)^t \times C_\lambda \times \sigma_{s,t,i,\lambda} \right), \\
F_3 &= \sum_{t \in T} \sum_{i \in \Lambda_B} \sum_{\lambda \in \Lambda_\gamma} \left(\left(\frac{1}{1+d} \right)^t \times C_\gamma \times \sigma_{s,t,i,\gamma} \right), \\
F_4 &= 365 \times 24 \times \sum_{t \in T} \left(\left(\frac{1}{1+d} \right)^t \times \left(\sum_{\substack{i \in \Lambda_B \\ i \neq j}} \sum_{\substack{j \in \Lambda_{LB} \\ i \neq j}} \left(\frac{(|U_{s,t,i}| - |U_{s,t,j}|)^2}{|Z_{ij}|} \right) \times S_{\text{Base}} \times \pi_s \right) \right), \\
F_5 &= 365 \times 24 \times \sum_{t \in T} \left(\left(\frac{1}{1+d} \right)^t \times \sum_{i \in \Lambda_B} \left(\sum_{\substack{z \in \Lambda_z \\ \lambda \in \Lambda_\lambda}} (S_{s,t,i,z} + S_{s,t,i,\lambda}) \times S_{\text{Base}} \times \pi_s \right) \right).
\end{aligned} \tag{2}$$

In this objective function, F_1 is the investment cost of installing a new line or feeder between nodes i and j in the MV network, F_2 is the investment cost of installing a new substation, F_3 is the investment cost of installing a new distribution substation, F_4 is the cost of losses, and F_5 is the cost of purchase power from the transmission network. The constraints of the UL problem are described in (3)–(8):

$$\begin{aligned}
&\sum_{\lambda \in \Lambda_\lambda} (S_{s,t,i,\lambda} + S_{s,t-1,i,\lambda}) + \sum_{z \in Z} S_{s,t,i,z} = \sum_{\gamma \in \Lambda_\gamma} (S_{s,t,i,\gamma} + S_{s,t-1,i,\gamma}) \\
&\quad + \sum_{\substack{i \in \Lambda_B \\ i \neq j}} \sum_{\substack{j \in \Lambda_{LB} \\ i \neq j}} \left[\left(\frac{|U_{s,t,i}| - |U_{s,t,j}|}{|Z_{ij}|} \right) \right], \\
&\forall s \in \Lambda_s, \forall t \in T, \forall i \in \Lambda_B,
\end{aligned} \tag{3}$$

$$\begin{aligned}
&S_{s,tij} \times (\sigma_{s,t,ij} + \sigma_{s,t-1,ij}) \times S_{\text{Base}} \leq S_{ij}^{\text{max}}, \\
&\forall s \in \Lambda_s, \forall t \in T, \forall i \neq j, j \in \Lambda_B,
\end{aligned} \tag{4}$$

$$\begin{aligned}
&\{S_{s,t,i,z}, S_{s,t,i,\lambda}, S_{s,t-1,i,\lambda}\} \leq S^{\text{PS-max}}, \\
&\forall s \in \Lambda_s, \forall t \in T, \forall i \in \Lambda_B, \forall \lambda \in \Lambda_\lambda,
\end{aligned} \tag{5}$$

$$\begin{aligned}
&\{S_{s,t,i,\gamma}, S_{s,t-1,i,\gamma}\} \leq S_\gamma^{\text{max}}, \\
&\forall s \in \Lambda_s, \forall t \in T, \forall i \in \Lambda_B, \forall \gamma \in \Lambda_\gamma,
\end{aligned} \tag{6}$$

$$\begin{aligned}
&U_i^{\text{min}} \leq U_{s,t,i} \leq U_i^{\text{max}}, \\
&\forall s \in \Lambda_s, \forall t \in T, \forall i \in \Lambda_B.
\end{aligned} \tag{7}$$

$$\begin{aligned}
&\text{Radial Structure of medium – voltage part} = 1, \\
&\forall s \in \Lambda_s, \forall t \in T.
\end{aligned} \tag{8}$$

Equation (3) shows the nodal balance in the MV network. The operation limitations of the MV feeders, substations, and distribution transformers are modeled in (4)–(6), respectively. The voltage limitations in all nodes of the MV network are modeled in (7), and equation (8) is used to ensure that the radial structure of the MV network is maintained.

2.2. LL Model. The objective function of the LL problem is composed of six terms as follows:

$$\text{LVC}_s = \sum_{s \in \Lambda_s} \delta_s \sum_{f=1}^6 F'_f, \tag{9}$$

where

1:	Begin
	Set initial sample times $NS=0$
2:	for sample of system state X_i
3:	while error is in allowable range
4:	$NS=NS+1$
5:	As to State X_i
6:	Calculate test function $F(X_i)$
7:	Estimate expectation of test function by $\frac{1}{NS} \sum_{t=1}^{NS} F(X_i)$
8:	Estimate the error by $\beta = \frac{\sqrt{V(\hat{E}(F))}}{\hat{E}(F)}$
9:	end while
10:	end for
11:	end

FIGURE 2: Pseudocode for handling the uncertainties based on the Monte Carlo method.

$$F'_1 = \sum_{t \in T} \sum_{\substack{i, j \in \Lambda_B \\ i \neq j}} \left(\left(\frac{1}{1+d} \right)^t \times C_{ij} \times \sigma_{s,t,ij} \right), \quad (10)$$

$$F'_2 = \sum_{t \in T} \sum_{i \in \Lambda_B} \sum_{g \in \Lambda_{DG}} \left(\left(\frac{1}{1+d} \right)^t \times C_{i,g}^{INV} \times \sigma_{s,t,i,g}^{DG} \times S_{Base} \times S_{s,t,i,g}^{DG} \right), \quad (11)$$

$$F'_3 = 365 \times 24 \times \sum_{t \in T} \sum_{i \in \Lambda_B} \sum_{g \in \Lambda_{DG}} \left(\left(\frac{1}{1+d} \right)^t \times C_{i,g}^{OP} \times \sigma_{s,t,i,g}^{DG} \times S_{Base} \times S_{s,t,i,g}^{DG} \right), \quad (12)$$

$$F'_4 = 365 \times 24 \times \sum_{t \in T} \left(\frac{1}{1+d} \right)^t \left(\sum_{\substack{i \in \Lambda_B \\ i \neq j}} \sum_{\substack{i \in \Lambda_{LB} \\ i \neq j}} \left(\frac{(|U_{s,t,i}| - |U_{s,t,j}|)^2}{|Z_{ij}|} \right) \times S_{Base} \times \pi_s \right), \quad (13)$$

$$F'_5 = \left(\frac{1}{1+d} \right)^t \times \sum_{t \in T} \sum_{\gamma \in \Lambda_\gamma} \left(S_{s,t,i,\gamma} + \left[S_\gamma^{Fe} + S_\gamma^{Cu} \left(\frac{S_{s,t,i,\gamma}}{S_\gamma^{max}} \right)^2 \right] \times \pi'_s \right), \quad (14)$$

$$F'_6 = \left(\frac{1}{1+d} \right)^t \times \left(pf \times S_{Base} \times \left\{ \left(\sum_{t \in T} \sum_{i \in \Lambda_B} \sum_{g \in \Lambda_{DG}} S_{s,t,i,g}^{DG} \times \sum_{e \in \Lambda_{DG}} E_{g,e}^{DG} \right) + \left(\sum_{t \in T} \sum_{\gamma \in \Lambda_\gamma} (S_{t,i,\gamma}) \times \sum_{e \in \Lambda_{DG}} E_e^G \right) \right\} \right). \quad (15)$$

In this objective function, F'_1 is the investment cost of installing new LV circuits between nodes i' and j' in the LV network. F'_2 and F'_3 are the investment and operation costs of installing DGs, respectively. F'_4 is the cost of line and F'_5 is the cost of purchasing power from the UL network, and finally, F'_6 is the cost of pollution emission. It

is Northway that the term in the bracket in equation (14) denotes the distribution transformer's losses, and the first and second terms in equation (15) denote the cost of pollution associated with nonrenewable DGs and the cost of pollution associated with the main grid, respectively. The constraints of the UL problem are described in (16)–(20):

```

1: Begin
2: for each topic from a topics set
3: begin
4:   Generate a population
5:   while not terminated condition
6:     for each chromosome from population
7:       Compute the fitness function
8:       Make next population
9:       Select parents
10:      Recombine pairs of parents
11:      Apply mutation to offspring
12:     end while
13:     Store the chromosome that obtained the best fitness
14:   end for
15:   Talk all stored chromosomes
16: end

```

FIGURE 3: Pseudocode of the applied GA.

$$\sum_{\gamma \in \Lambda_\gamma} (S_{s,t,i,\gamma} + S_{s,t-1,i,\gamma}) = D - \sum_{\substack{i_l \in \Lambda_B' \\ g \in \Lambda_{DG}}} (S_{i_l',g}^{DG}) + \sum_{t \in T} \left(\sum_{\substack{i_l \in \Lambda_B' \\ i_l \neq j_l}} \sum_{\substack{j_l \in \Lambda_{LB} \\ i_l \neq j_l}} \left(\frac{|U_{s,t,i_l}| - |U_{s,t,j_l}|}{Z_{i_l'j_l}} \right)^2 \times S_{Base} + \sum_{\gamma \in \Lambda_\gamma} \left[S_\gamma^{Fe} + S_\gamma^{Cu} \left(\frac{S_{s,t,i,\gamma} + S_{s,t-1,i,\gamma}}{S_\gamma^{\max}} \right)^2 \right] \times \pi_s' \right), \quad (16)$$

$$\forall s \in \Lambda_s, \forall t \in T, \forall i \in \Lambda_B,$$

$$S_{s,t,i_l,j_l} \times (\sigma_{s,t,i_l'} + \sigma_{s,t-1,i_l'}) \times S_{Base} \leq S_{i_l'}^{\max}, \quad (17)$$

$$\forall s \in \Lambda_s, \forall t \in T, \forall i_l \neq j_l, i_l, j_l \in \Lambda_B,$$

$$U_i^{\min} \leq U_{s,t,i} \leq U_i^{\max}, \quad (18)$$

$$\forall s \in \Lambda_s, \forall t \in T, \forall i \in \Lambda_B,$$

$$\{S_{s,t,i',g}^{DG}, S_{s,t-1,i',g}^{DG}\} \leq S_g^{\max}, \quad (19)$$

$$\forall s \in \Lambda_s, \forall t \in T, \forall i_l \in \Lambda_B', \forall g \in \Lambda_{DG},$$

$$\text{Radial Structure of low - voltage part} = 1, \quad (20)$$

$$\forall s \in \Lambda_s, \forall t \in T.$$

Constraint equation (16) shows the nodal balance of the LV network. The operation limitations of LV circuits, node voltage, and DGs are modeled in equations (17)–(19), respectively. Finally, equation (20) is used to ensure that the radial structure of the LV network is maintained.

3. Modeling of Uncertainties

In this section, the uncertainties of the demand and the output power of renewable energy sources are modeled.

According to [44], three qualitatively different types of uncertainty ethical, option, and state space uncertainty are distinct from state uncertainty, the empirical uncertainty that is typically measured by a probability function on states of the world. Ethical uncertainty arises if the agent cannot assign precise utilities to consequences. Option uncertainty arises when the agent does not know what precise consequence an act has in every state. Finally, state space uncertainty exists when the agent is unsure of how to construct an exhaustive state space. These three types of uncertainty are characterized

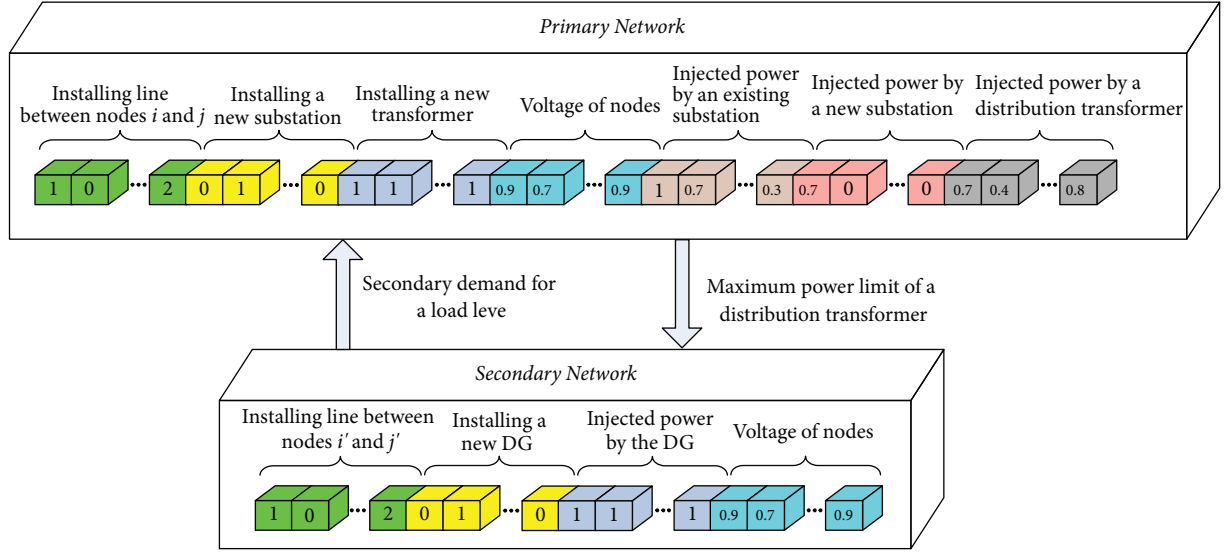


FIGURE 4: Structure of the proposed chromosome.

along three dimensions, natures, object, and severity, and the relationship between them is examined.

In this study, the uncertainties include the uncertainty related to load demand and renewable energy resources that have specific probability density functions (PDF). The Monte Carlo simulation method is a simulation approach based on probability and statistics theory and methodology. At present, the Monte Carlo simulation method has been applied to many fields of engineering and scientific theory, with the advantages of simple principles and realization, insensitivity to the dimension of problems, avoidance of any constraining assumptions, and strong adaptability. In the Monte Carlo simulation method, the state of each component in the system is obtained by sampling. The components include various system equipment, such as generators, transmission lines, transformers, and different load levels. Therefore, the MCS is applied to handle the uncertainties.

3.1. Modeling the Uncertainty of Demand. In general, the electric charge and energy price are estimated by the normal probability distribution function (PDF). Since this ordinary PDF is a continuous function, therefore, the probability of each point is not shown. To overcome this problem, the continuous function must be estimated with a normal discontinuous function. In this approximation, if the intended steps are smaller, the approximation error will be smaller.

The next step is to generate PDF-based loading scenarios. For this purpose, the roulette wheel mechanism (RWM) is applied. Thus, the load surfaces are normalized to the range and then a random number is generated. If, among the load levels, a random number, generated in the normalized probability region of a load prediction level, is placed on the roulette wheel, the load prediction level is selected by RWM

as the scenario. This process is repeated until scenarios called RW/MCS are generated [45].

3.2. Modeling the Uncertainties of WT and PV. One of the functions used to model wind speed is to use the Weibull PDF. The output power of a WT is shown as follows [45]:

$$P^{\text{WT}} = \begin{cases} 0, & \forall V^w \leq V_{\text{cutin}}^w, V^w \geq V_{\text{cutout}}^w \\ 0.5 \times \rho_w \times A_w \times \eta_w \times \min(V^w, V_R^w), & \forall V_{\text{cutin}}^w \leq V^w \leq V_{\text{cutout}}^w \end{cases} \quad (21)$$

The output power of a photovoltaic array is shown as follows [45]:

$$P^{\text{PV}} = \left[P_{\text{pv,STC}} \times \frac{G_T}{G_{T,\text{STC}}} \times (1 - \gamma \times (T_j - T_{j,\text{STC}})) \right], \quad (22)$$

where

$$T_j = T_{\text{Amp}} + \frac{G_T}{G_{T,\text{STC}}} \times (\text{NOCT} - 20). \quad (23)$$

In this formulation, the parameter G_T is an uncertain parameter that is based on the Beta PDF.

3.3. Handling the Uncertainties by Monte Carlo Simulation. Monte Carlo methods are a set of computational algorithms based on random sampling iterations to calculate results. Monte Carlo methods are generally used when it is impossible to calculate the exact result with a definite algorithm. Therefore, due to the reliance of this method on the repetition of calculations and random numbers, it is suitable for calculation by a computer. Monte Carlo methods are, in fact, one of the most comprehensive tools for evaluating uncertain studies [46]. The general pseudocode for handling the uncertainties-based Monte Carlo

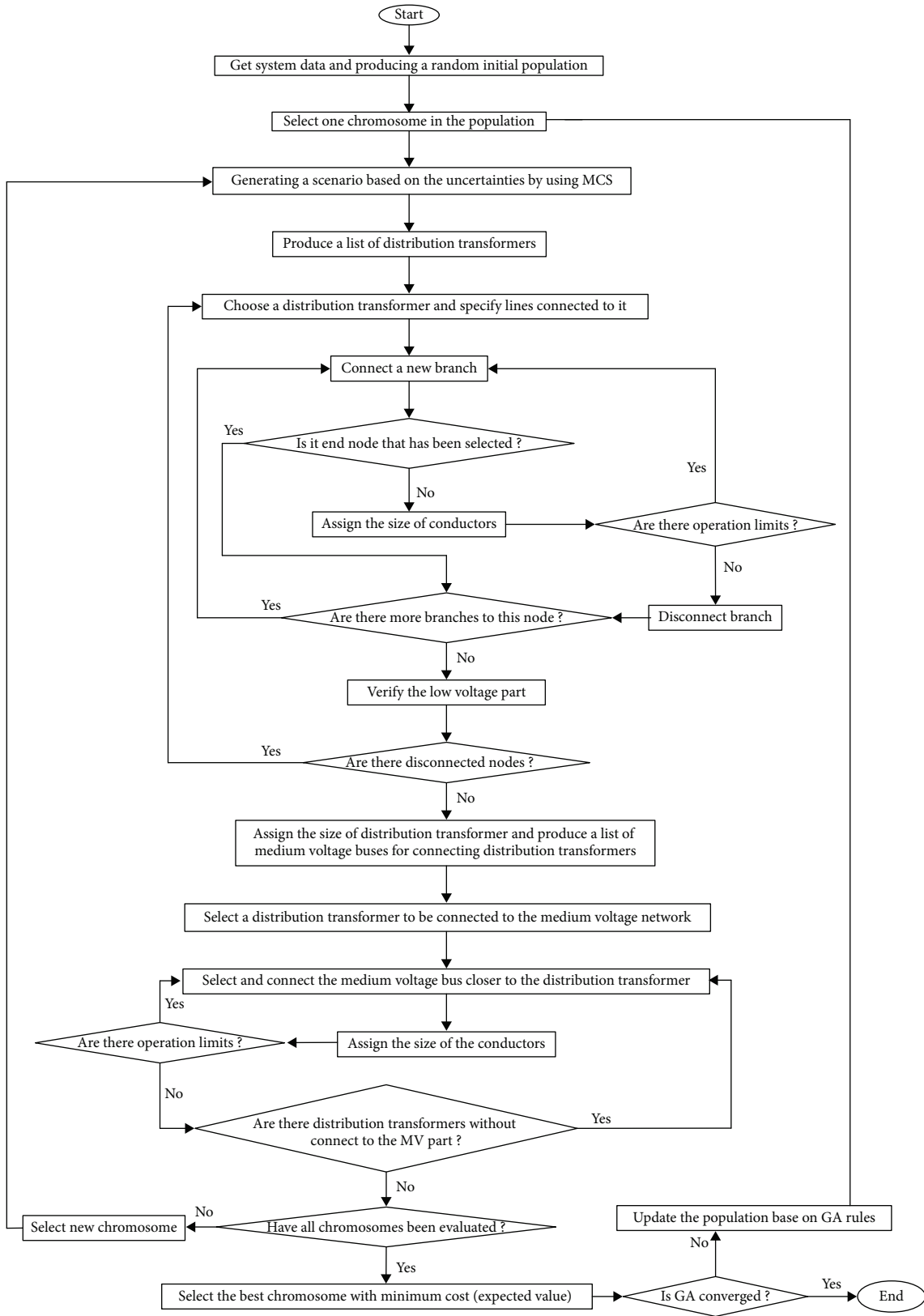


FIGURE 5: Flowchart of the proposed methodology.

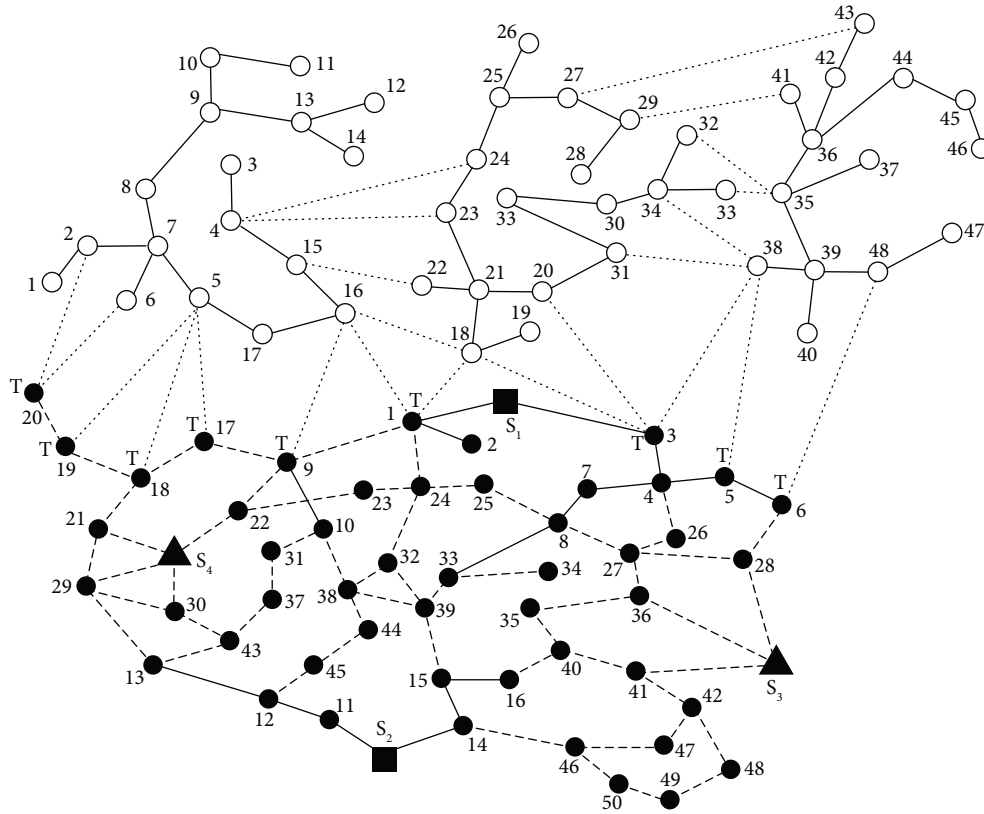


FIGURE 6: The studied distribution network.

methods is shown in Figure 2, where $F(X_i)$, β , $\hat{E}(F)$, and V represent experiment function, variance coefficient, estimated value, and variance index, respectively.

4. Solution Approach

To solve the proposed MINLP model, the GA is employed. This algorithm is inspired by the process of natural selection that belongs to the larger class of evolutionary algorithms. The GA is commonly applied to produce high-quality solutions to optimize and search problems by relying on biologically inspired operators such as mutation, crossover, and selection.

The GA makes it possible to look for optimal solutions in a nonconvex space, which can be achieved with an initial configuration. This configuration is also achievable in a heuristic way. After evaluating the configuration, specific topologies are suggested. These topologies are called neighbors, and due to the high number of topologies, a specific number of them are selected according to the conditions of the problem. The best configuration is selected from the topologies. This strategy continues until the end condition is reached to obtain a global optimal point, which is the best answer in terms of minimum cost. The pseudocode of the GA is shown in Figure 3. Subsequently, other parameters of the algorithm are explained.

The coding system can be in the form of a string, array, list, or tree. The choice of each of these methods is made according to the type of problem and the search required to

solve and optimize it. Meanwhile, string coding is more useful than other methods due to its ability to create a more chromosome diversity in less space. The encoding of the UL chromosome and LL is shown in Figure 4. In this study, to handle the constraints, Deb's method [47] is employed. Deb's method is actually a parameterless penalty strategy based on the following three rules:

- (i) Any feasible solution is preferred to any infeasible solution
- (ii) Between two feasible solutions, the one having the better objective value is preferred
- (iii) Between two infeasible solutions, one having the smaller constraint violation is preferred

After applying genetic actuators (crossover and mutation) to chromosomes, new answers are obtained that may not be true in the problem's constraints. This happens in many cases with constraints. The simplest solution is to use the penalty function for the objective function. As a result, the selection process tends to the true chromosomes. After deciding how to encode chromosomes, the initial population must be created. This step is usually done by randomly selecting values within the allowable range.

First, it is required to determine the location, capacity, and amount of power injected into the transformers, which is suggested by the UL problem. However, load distribution equations in the MV network cannot be calculated due to the

TABLE 2: Specification of load nodes in MV part.

No.	Load (kW)
1	700
2	600
3	500
4	500
5	600
6	700
7	500
8	900
9	500
10	900
11	300
12	400
13	400
14	700
15	800
16	900
17	700
18	500
19	600
20	800
21	800
22	600
23	400
24	500
25	900
26	500
27	500
28	700
29	800
30	900
31	700
32	600
33	500
34	400
35	900
36	300
37	800
38	700
39	700
40	400
41	500
42	400
43	500
44	600
45	800
46	800
47	400
48	800
49	500
50	800

uncertainty in the amount of power injected into the transformers. In other words, the UL objective function, equation (1), is specified with the UL constraints when the amount of power injected into each transformer is determined. When the location and capacity of the transformers are determined in the UL problem, the LL problem is solved to determine the amount of power injected into the transformers. After determining the amount of power injected into the transformers, the amount of the UL objective

TABLE 3: Specification of load nodes in LV part.

No.	Load (kW)
1	620
2	640
3	770
4	520
5	620
6	400
7	600
8	600
9	640
10	400
11	530
12	700
13	700
14	600
15	450
16	770
17	750
18	750
19	600
20	600
21	720
22	700
23	700
24	680
25	600
26	400
27	740
28	400
29	400
30	400
31	700
32	750
33	720
34	740
35	750
36	600
37	600
38	250
39	400
40	350
41	580
42	790
43	700
44	680
45	600
46	680
47	620
48	620

function can also be calculated. The flowchart of the proposed algorithm is shown in Figure 5.

5. Numerical Study

To demonstrate the effectiveness of the proposed model and validate the solving approach, it is applied to a sample distribution network shown in Figure 6. The proposed planning has been executed in a MATLAB programming environment (R2016a) on a laptop with an Intel Core i7-

TABLE 4: Specification of wires.

Type	Resistance (Ω)	Reactance (Ω)	Maximum capacity (MVA)	Cost (\$)
1	7.500	17.46	1.16	17000
2	4.794	16.73	1.6	22000
3	3.038	15.96	2.17	30000
4	3.972	14.96	2.97	42000
5	4.208	14.42	3.96	54000
6	5.723	12.62	5.77	85000
7	5.487	12.17	7.62	125000
8	6.405	11.96	8.63	140000
9	4.350	11.80	9.53	165000
10	4.247	11.40	12.29	220000
11	5.19	11	13.34	270000
12	5.17	9	16.19	310000

TABLE 5: Specification of substations.

Substation	Existing capacity (MVA)	Expandable capacity (MVA)
S_1	3×15	5×15
S_2	2×15	5×15
S_3	0	4×15
S_4	0	4×15

TABLE 6: Specification of the distribution transformers.

Transformer	Maximum capacity (MVA)	Cost (k\$)
1	4	500
2	6	800
3	8	1000
4	10	1100

TABLE 7: Data of six DG technologies.

DG technology	Unit size (MVA)	Investment cost (k\$/MVA)	Operation cost (\$/MVA-h)
DE	1	500	42
FC	1.5	450	47
GT	1	400	46
MT	0.8	470	52
PV	1	800	10
WT	1	800	10

6500 and 8 GB RAM. After running the program (GA) several times, it was found that the best values for the number of chromosomes, crossover, and mutation were 100, 0.72, and 0.06, respectively. To maintain the most suitable chromosomes during the optimization approach and to improve GA efficiency, the elite selection approach is applied. Thus, the current 10% of the worst population is replaced by the previous 10% of the previous generation. Of course, this replacement is done if 10% of the previous generation is more qualified in terms of objective function than the current generation.

The MV part is a 54-node 33 kV network consisting of 50 load points, which are shown by solid circles with the specifications of Table 2. The LV part is a 48-node 11 kV network consisting of 48 load points, which are shown by white circles with the specifications of Table 3. It is

TABLE 8: Pollution emission rates of the DG technologies.

Type	NO _x	SO ₂	CO ₂	CO	PM ₁₀
DE	0.00213	0.00125	0.625	0.0028	0.00036
FC	0.000015	0.000024	0.447	0	0
GT	0.00029	0.000032	0.625	0.0004	0.00004
MT	0.0002	0.000037	0.725	0.0005	0.00004
PV	0	0	0	0	0
WT	0	0	0	0	0
Grid	0.0022952	0.0035834	0.92125	—	—

TABLE 9: Some other parameters of the studied network.

Number of MCS iteration	200
T	5
d	3%
U^{\min}	0.95 p.u
U^{\max}	1.05 p.u
π	70 \$/MVA-h
π'	72 \$/MVA-h
Base MVA	100
pf	10000
NOCT	45.5°C
T_{amp}	20°C
V_{cutin}^w	4 (m/s)
V_{cutout}^w	25 (m/s)
V_R^w	14 (m/s)
ρ_w	0.8 kg/m ³
$A_{\omega Z}$	10 m ²
η_w	0.45
$G_{T,STC}$	1 kW/m ³
$T_{j,STC}$	25°C
$P_{PV,STC}$	0.165 kW
Stop criterion for GA	100
Annual load increase rate	0.1%
Cost of installing one 15 MVA substation	2 M\$

noteworthy that the power factor ($\cos\phi$) of loads is considered 0.8.

In this study, proposed (S_3 and S_4) and existing (S_1 and S_2) distribution substations are shown as solid triangles and solid squares, respectively. The MV system has 17 existing feeders (type 1) and 56 new lines as candidates for installation. The LV system has 44 existing lines (type 1) and 22 new lines as candidates for installation. Proposed and exiting

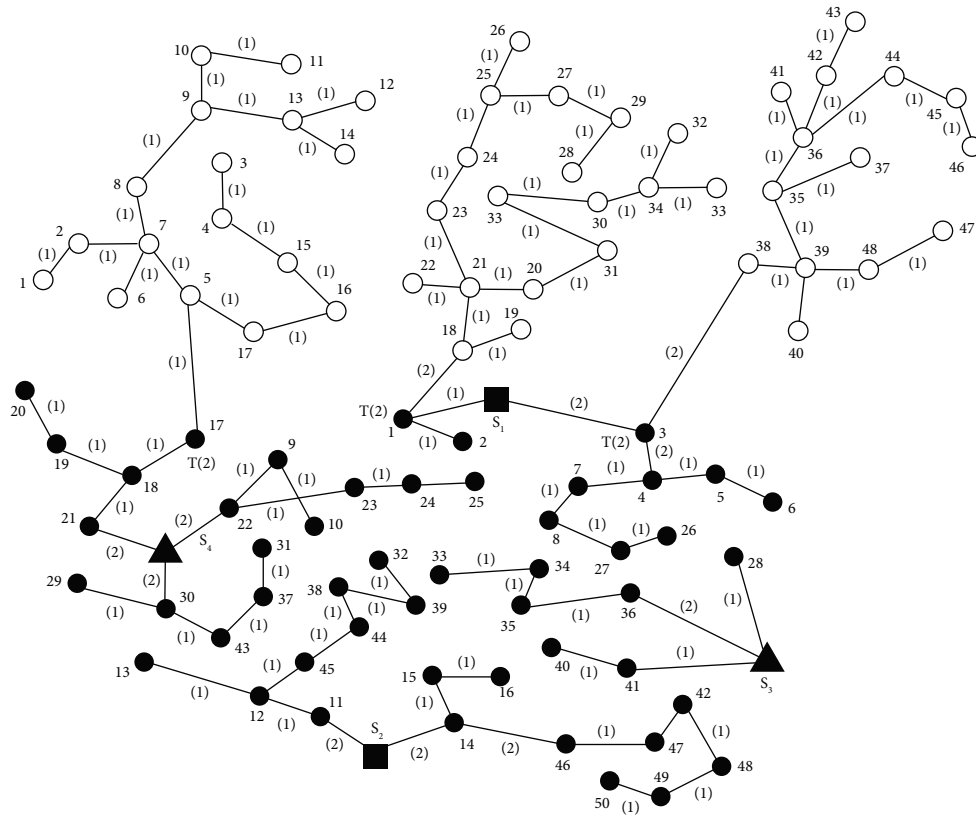


FIGURE 7: Configuration of the network in case#1.

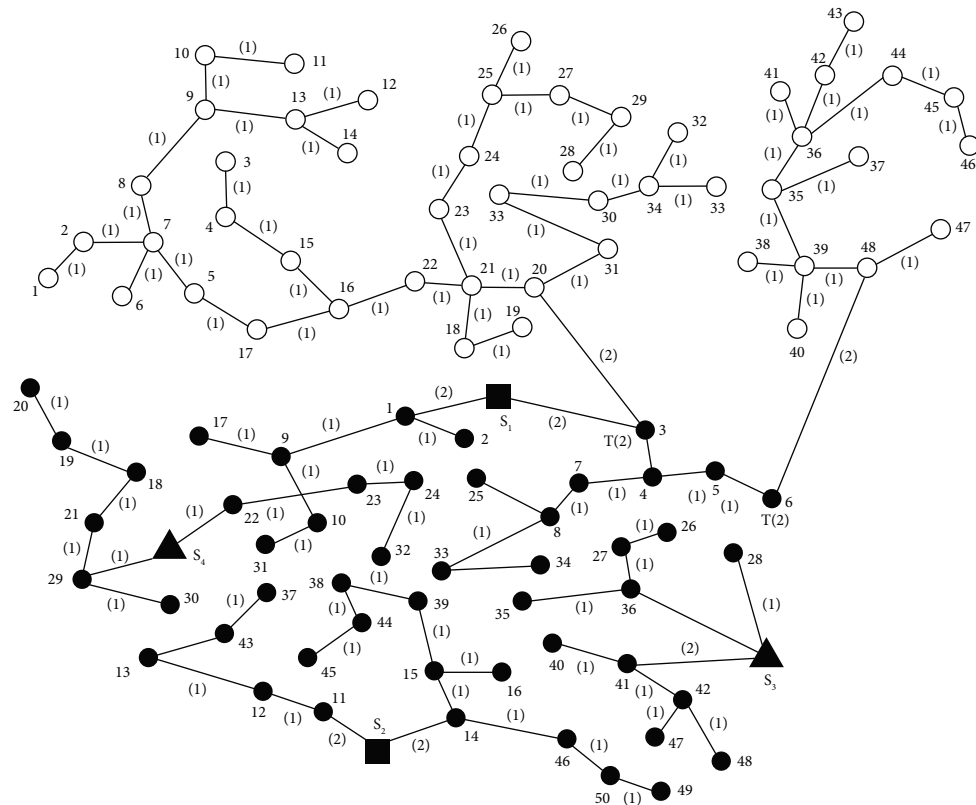


FIGURE 8: Configuration of the network in case#2.

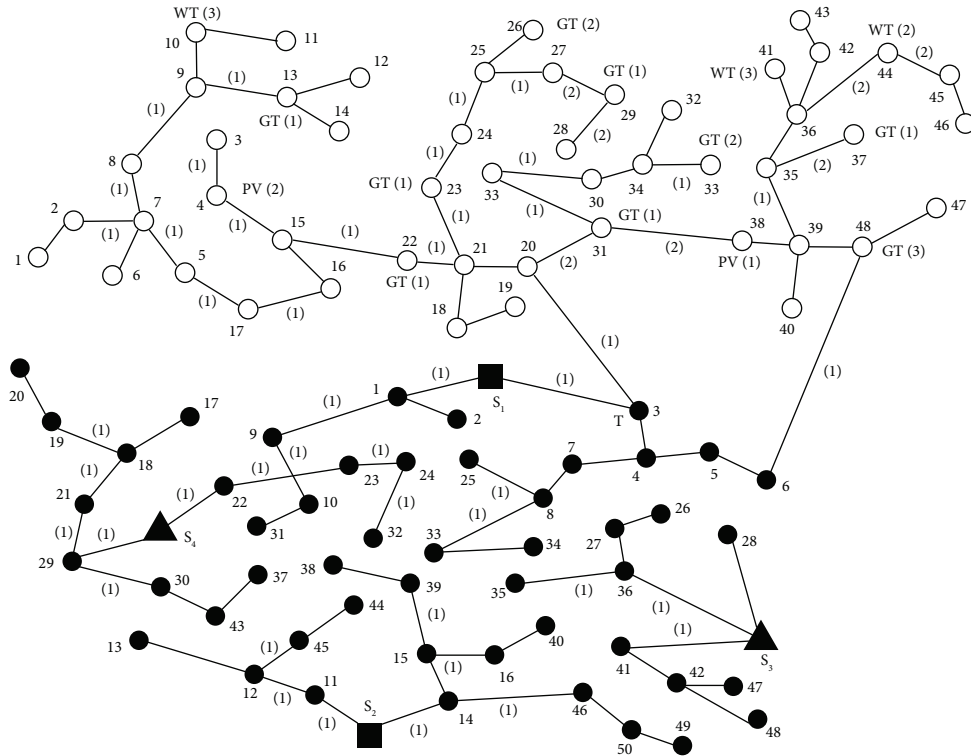


FIGURE 9: Configuration of the network in case #3.

TABLE 10: The obtained results for the case studies.

Item	MV part		
	Case #1	Case #2	Case #3
Substation installation cost (M\$)	36	36	34
Distribution transformer cost (M\$)	2.4	1.6	1.3
Feeders cost (M\$)	10.38	9.89	5.3
Purchased power from main grid (M\$)	74.52	74.52	69.48
Losses cost (M\$)	3.86	3.17	2.12
Total (M\$)	127.16	125.18	112.2
<i>Item</i>	<i>LV part</i>		
Feeders' cost (M\$)	5.06	4.59	2.25
DG installation cost (M\$)	0	0	12.4
DG operation cost (M\$)	0	0	8.046
Purchased power from MV part (M\$)	34.83	34.83	29.58
Losses cost (M\$)	5.425	4.213	2.332
Emission cost (M\$)	24.74	24.74	12.52
Total (M\$)	70.056	68.373	67.128
Total cost (M\$)	197.216	193.553	179.328

lines are illustrated by dotted and solid lines, respectively, in Figure 6. The candidate nodes for installing distribution transformers are shown by the letter “T” beside them. All the low-voltage nodes are candidates for installing DGs. Twelve different types of conductors (Table 4), three types of substations (Table 5), five types of distribution transformers (Table 6), and six types of DGs, including WT, PV, GT, MT, FC, and DE, are considered (Table 7). The pollution emissions of the DGs and the grid are shown in Table 8.

Uncertainty in electrical loads is calculated by a normal probability function with the mean values listed in Tables 2

and 3 and a standard deviation value of 3%. Other required specifications and information about the studied network are given in Table 9.

To validate the proposed methodology, three different cases are considered as follows:

- (i) Planning of the MV and LV networks independently considering uncertainty in demand and energy price (case #1)
- (ii) Integrated planning considering uncertainty in demand (case #2)

TABLE 11: The obtained results for the case studies.

Ref.	Total cost (M\$)	Pollution	Losses	Transformers
[23] in scenario 1	204.72	×	✓	×
[23] in scenario 2	180.80	×	✓	×
[15] in case #1	18.72	×	×	×
[15] in case #2	18.93	×	×	×
[15] in case #3	19.28	×	×	×
This paper (bi-level model)	179.328	✓	✓	✓

TABLE 12: Sensitivity analysis on load demand.

Load percent (%)	Costs (M\$)			
	DGs (installation and operation)	Losses (MV and LV)	Emission	Total
80	19.774	4.002	9.26	159.117
90	20.036	4.212	10.57	168.209
100	20.446	4.452	12.52	179.328
110	20.866	4.773	14.65	190.984
120	21.652	4.925	16.85	203.016
150	22.055	5.324	19.04	215.197

TABLE 13: Sensitivity analysis on price of electric energy.

Price percent (%)	Costs (M\$)			
	DGs (installation and operation)	Losses (MV and LV)	Emission	Total
80	16.929	3.606	13.489	142.449
90	18.810	4.007	12.921	159.808
100	20.446	4.452	12.52	179.328
110	23.513	4.898	11.894	199.054
120	26.805	5.387	11.549	223.339
150	32.434	6.678	10.856	273.474

(iii) Integrated planning considering DGs in the LV system with uncertainty in demand and RESs (case #3)

In case #1, the planning is executed while the medium- and low-voltage networks are two independent networks. The results of all the case studies are shown in Figures 7–9 and Table 10.

The types of lines and transformers installed on the network are marked with parentheses on them. The overall results from Table 10 show that the minimum total cost is obtained in case studies 2 and 3, which actually use the proposed algorithm; as expected, the minimum planning cost was obtained for the third study, in which DGs were used. Figure 10 shows a good comparison between the cost components in both networks.

The highest planning cost was obtained for the first case study, which shows that the bi-level model reduces expansion plans.

As can be seen, case #3 has the lowest costs, and this is due to the undeniable fact that the penetration of distributed generation sources in the low voltage network allows the installation of transformers and lines of smaller sizes, and that the medium voltage network is also affected, which has the lowest operating costs. This shows that the bi-level model reaches the planning point at a lower cost by considering

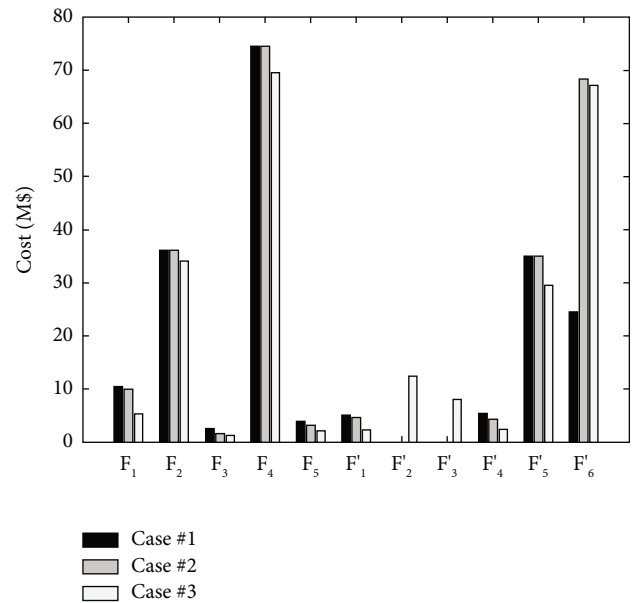


FIGURE 10: Comparison of the cost components in MV and LV networks.

DGs and, in fact, proposes a topology that also has lower losses.

In case #1, the existing initial lines are more chargeable, and therefore, the existing substation will have a higher chargeability than the proposed substation, and this topology has more technical losses than the other two cases due to the increase in current circulating through the network. The same is true for the medium voltage network, which in case #2 and case #3 causes the electric current of the lines to decrease, and this in turn will reduce the losses of electrical energy. Therefore, it can be said that the bi-level model finds solutions that better distribute the current flow in the network.

Table 11 compares the material in this study with other studies in this field, and as seen, the proposed algorithm is very efficient.

In Tables 12 and 13, sensitivity analysis was performed on load demand and electric energy price, respectively, and their impact on the total cost, pollution cost, and the cost of DGs has been determined. The results showed that, with the decrease in the price of electric energy, the use of DGs decreased and caused more pollution.

6. Conclusion

In this study, a bi-level model is presented to simultaneously perform expansion planning in both medium voltage and low voltage distribution networks. To this end, a control variable called the capacity of distribution transformers was used. Therefore, first a capacity is selected for the distribution transformers, and then, according to the constraints of the problem, the low-level problem or low-voltage network planning is done in such a way that if the low-level constraints are not satisfied, the capacity and location of the distribution transformers must be changed, and if the constraints are satisfied, then the high-level problem is solved, and again, if the constraints of the high-level problem are satisfied, the result is checked to check the optimality of the overall solution; otherwise, the location and capacity of the distribution transformers must be changed again. This process continues until reaching an optimal solution. Therefore, by using a bi-level model, an attempt has been made to propose a location and capacity for distribution transformers that is acceptable from the point of view of each network. The proposed problem was solved by a genetic algorithm, and the results illustrate the efficiency of this method because it allows finding good quality settings for the experimental system under study. According to the results, it was particularly clear that planning separately in each medium-voltage or low-voltage network alone cannot be an optimal solution for the entire network. Therefore, it is better to consider planning in both medium-voltage and low-voltage networks so that the requirements of each network are met, and in better words, the conflict between the two networks, which is the optimal placement of transformers, is resolved. It should be mentioned that the application of distributed generators is also undeniable in the optimal operation of the network. As a suggestion for future work, the following items can be mentioned:

- (i) Use of electric vehicles at a low voltage level
- (ii) Involve private owners and expression new objective functions
- (iii) Conflict analysis when private owner's express different objectives
- (iv) Consider correlation among the scenarios in the stochastic approach

Nomenclature

Sets and Indices

f :	Index for objective functions
S :	Index for scenario
t :	Index for time
i, j :	Index for nodes in the medium voltage part
i', j' :	Index for nodes in the low voltage part
B :	Index for nodes
LB :	Index for load nodes
γ :	Index for distribution transformer
λ :	Index for candidate substation
z :	Index for existing substation
g :	Index for DGs
e :	Index for pollution
T :	Set of time period
Λ_B :	Set of nodes in medium voltage part
$\Lambda_{B'}$:	Set of nodes in low voltage part
Λ_{LB} :	Set of load nodes in medium voltage part
Λ'_{LB} :	Set of nodes in low voltage part
Λ_λ :	Set of candidate substations
Λ_z :	Set of existing substations
Λ_γ :	Set of candidate distribution transformers
Λ_s :	Set of scenarios
Λ_{DG} :	Set of DGs
Λ_E :	Set of pollutant gases.

Parameters

d :	Discount rate
Z_{ij} :	Impedance between nodes i and j in the medium voltage part
$Z_{i'j'}$:	Impedance between nodes i' and j' in the low voltage part
C_{ij} :	Cost of installing a new line between nodes i and j in the medium voltage network
$Z'_{i'j'}$:	Cost of installing a new line between nodes i' and j' in the low voltage network
C_λ :	Cost of installing a new substation
C_γ :	Cost of installing a new distribution transformer
$C_{i,g}^{INV}$:	Cost of installing a new DG of type g in node i
$C_{i,g}^{OP}$:	Operation cost of a new DG of type g in node i
S_{Base} :	Base kVA of the network
π_s :	Energy price in medium voltage part in scenario s
π'_s :	Energy price in low voltage part in scenario s
U_i^{\min} :	Minimum voltage of node i in medium voltage part
U_i^{\max} :	Maximum voltage of node i in medium voltage part
$U_{i'}^{\min}$:	Minimum voltage of node i' in low voltage part

U_i^{\max}	: Maximum voltage of node i' in low voltage part
$S^{\text{PS-max}}$: Maximum capacity of existing and candidate substations
S_{γ}^{\max}	: Maximum capacity of a distribution transformer γ
S_{ij}^{\max}	: Maximum capacity of a line between nodes i and j
$S_{i'j'}^{\max}$: Maximum capacity of line between nodes i' and j'
pf:	: Penalty factor for pollution emission
V_{cutin}^w	: Minimum wind speed (m/s)
V_{cutout}^w	: Maximum wind speed (m/s)
V^w	: Wind speed (m/s)
ρ_w	: Air density (kg/m^3)
A_w	: Wind turbine blade area (m^2)
η_w	: Wind turbine power coefficient
G_T	: Solar radiation (kW/m^2)
$G_{T,\text{STC}}$: Solar radiation in standard test conditions (STC) (kW/m^2)
T	: Cell temperature ($^{\circ}\text{C}$)
P^{WT}	: Output power of wind turbine (kW)
P^{PV}	: Output power of photovoltaic (kW)
$P_{\text{PV,STC}}$: Maximum test power in STC (kW)
T_{amp}	: Environmental temperature ($^{\circ}\text{C}$)
NOCT:	: Normal operating cell temperature ($^{\circ}\text{C}$)
γ :	: Power-temperature coefficient
S_{γ}^{Fe}	: Iron losses of a distribution transformer γ
S_{γ}^{Cu}	: Copper losses of a distribution transformer γ
$E_{g,e}^{\text{DG}}$: Pollution emission of type e from DG type g
E_e^G	: Pollution emission of type e from the main grid
δ_s	: Probability of scenario s

Variables

$\sigma_{s,t,i,j}$: Integer variable for a new line between nodes i and j in scenario s and time period t in medium voltage part
$\sigma'_{s,t,i',j'}$: Integer variable for a new line between nodes i' and j' in scenario s and time period t in low voltage part
$\sigma_{s,t,i,\lambda}$: Binary variable for a new substation λ in scenario s and time period t in node i
$\sigma_{s,t,i,\gamma}$: Binary variable for a new distribution transformer γ in scenario s and time period t in node i
$\sigma'_{s,t,i',g}$: Integer variable for a new DG type g in scenario s and time period t in node i'
$U_{s,t,i}$: Voltage of node i in scenario s and time period t in medium voltage part
$U'_{s,t,i'}$: Voltage of node i' in scenario s and time period t in low voltage part
$S_{s,t,i,\lambda}$: Injected power by a substation λ in scenario s and time period t
$S_{s,t,i,z}$: Injected power by an existing substation z in scenario s and time period t
$S_{s,t,i,\gamma}$: Injected power by a distribution transformer γ in scenario s and time period t
$S_{s,t,i',g}^{\text{DG}}$: Injected power by a DG of type g at node i' in scenario s and time period t .

Data Availability

No data were used to support the findings of the study.

Conflicts of Interest

The authors declare that they have no conflicts of interest.

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