

Research Article

The Adsorption Capacity and Geotechnical Properties of Modified Clay Containing SSA Used as Landfill Liner-Soil Materials

Haijun Lu,^{1,2} Yiqie Dong,² Jixiang Li,² and Changhong Wang²

¹State Key Laboratory of Geomechanics and Geotechnical Engineering, Institute of Rock and Soil Mechanics, Chinese Academy of Sciences, Wuhan 430071, China

²Institute of Poromechanics, Wuhan Polytechnic University, Wuhan 430023, China

Correspondence should be addressed to Haijun Lu; lhj_whpu@163.com

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The potential of clay containing 0~5% sewage sludge ash (SSA) is assessed for use as a landfill liner-soil material. Low temperature N₂ adsorption, batch adsorption, permeability, and unconfined compressive strength tests are performed to evaluate pore structure, adsorption capacity, hydraulic conductivity, and unconfined compressive strength of the clays. The pore size distribution of the modified clay containing SSA is mainly composed of micropores (<2 nm) and mesopores (2~7 nm). With the increasing of SSA from 0% to 5%, the adsorption capacity of Zn(II) and Cu(II) to the clay increases 37% and 273%, respectively. The hydraulic conductivity of modified clay is from 3.62×10^{-8} to 2.17×10^{-8} cm/s. At SSA = 3%, the unconfined compressive strength of the clay reaches the maximum value of 601.1 kPa. After the clay containing SSA is contaminated by acid and alkali chemical solutions, the amount of mesopores and hydraulic conductivity increase. The adsorption capacity and unconfined compressive strength of contaminated clay decrease about 2~44% and 25.7~38.2%, respectively. The modified clay containing SSA can meet the adsorption and geotechnical requirement of landfill liners.

1. Introduction

The pollution caused by the sewage sludge is one of the most highlighted environmental problems in China. According to related surveys, the national output of the wet sludge is 2.24×10^7 t, namely, 6.14×10^4 t per day. However, half of the sewage sludge is not correctly disposed. The sewage sludge without innocuous treatment easily contaminates atmosphere, water, and soil. Nowadays, the properties of dry sludge and techniques of sludge disposing are investigated comprehensively [1, 2], though there are few researches in the resources utilization of the sewage sludge.

In view of the low cost and good hygiene condition, the liner system composed of the compacted clay is widely applied to design of the landfill. The structural stability of the liner system is one of the key factors to ensure the working of the system safely. He et al. found that the landfill leachate contains plenty of heavy metal elements and its pH values

range from 4.5 to 9 [3]. If the system is under long-period of sustained leachate contamination, the liner system is so badly weakened that it generates potential threats to human health.

Many scholars used some materials to improve adsorption capacity of the liner system [4–6], such as coal ash, red mud, bentonite, and straw fiber. Sewage sludge ash (SSA) is a kind of porous material produced at the high temperature incineration. The SSA has relatively high specific surface area and ion-exchange capacity [7]. Moreover, the ash also has relatively high adsorption capacity on heavy metal ions, such as Cd(II), Ni(II) [8].

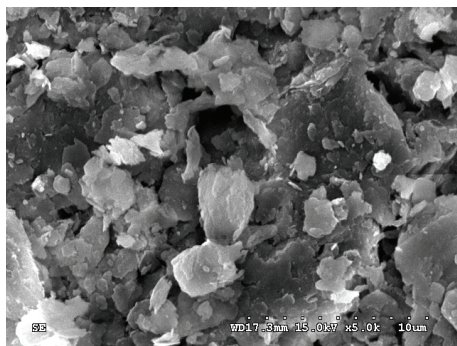
The objective of this paper is to evaluate the feasibility of the modified clay containing SSA used as the landfill liner-soil material. The transformations of pore structure of the modified clay are analyzed using the low temperature N₂ adsorption tests. The adsorption capacity of Zn(II) and Cu(II) to the modified clay is investigated by batch tests. The hydraulic conductivity and strength properties of the

TABLE 1: The physical properties of the clay.

$\rho_{d\max}$ (g/cm ³)	W_{opt} (%)	W_L (%)	W_p (%)	I_p	Particle size distribution (%)			
					>0.05 (mm)	0.05~0.005 (mm)	0.005~0.002 (mm)	<0.002 (mm)
1.65	19	48.5	26.2	22.3	12	32	45	11

TABLE 2: The chemical constituents of the clay (%).

SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	MgO	K ₂ O	Na ₂ O
58.42	25.23	0.24	0.51	0.12	5.32	2.67

FIGURE 1: The microstructure of SSA (5.0 k, 10 μm).

modified clay are systematically determined by permeability and unconfined compressive strength tests.

2. Materials and Methods

2.1. Testing Materials. The clay and sewage sludge used in tests were obtained from a construction site and the Han-xi sewage treatment plant in Wuhan, China, respectively. The physical properties and chemical constituents of the clay and the basic physical properties of the sewage sludge are listed in Tables 1–3, respectively.

The sludge was dried in the thermostatic temperature dry box at 105°C for 24 h. After that, the sludge was incinerated in the Muffle furnace (Tianjin Mafuer Sci. & Tech. Co., Ltd.) under the anaerobic condition at 850°C for 3 h. The red-brown and grainy ash was sieved through the 200-mesh screen [9]. The chemical constituents of SSA are listed in Table 4. The microstructure, pore volume, and pore size distribution of SSA are shown in Figures 1 and 2, respectively. It can be seen from Figures 1 and 2 that the SSA is irregular and porous, and every relic of SSA has small volume. The distribution of pore volume is uniform, and the pores from 2 to 4 nm have greater proportion.

2.2. Testing Methods

2.2.1. Low Temperature N₂ Adsorption Tests. The clay was firstly broken into pieces and selected through the 2 mm screen. After that, the clay was mixed with 5% SSA as modified clay [10, 11]. According to the pH value of leachate, the chemical solutions (pH = 5, 7 and 9) were confected by the

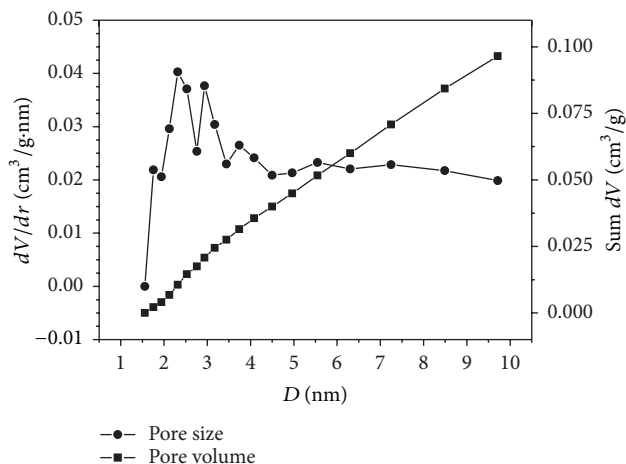


FIGURE 2: The pore volume and pore size distributions of SSA.

hydrochloric acid and sodium hydroxide. The modified clay was soaked in the solutions for 30 days. The clay was selected through the 2 mm round hole screen. The pore structure of the clay was investigated by JW-BK static nitrogen adsorption instrument (Beijing JWGB Sci. & Tech. Co., Ltd.).

2.2.2. Batch Tests. Dry clay of 50.0 g was equally divided into four parts, and the four parts were mixed with 0%, 1%, 3%, and 5% SSA, respectively. The mixed clay was soaked in 50 mL ZnCl₂ (aq) and CuCl₂ (aq), respectively. To keep the range of pH value at 5–9, the HCl and NaOH solutions were added into the ZnCl₂ (aq). Similarly, the pH value of CuCl₂ (aq) was kept at the range from 4 to 8. The mixture was shaken in water bath instrument under the condition of 25°C, 150 r/min. The concentrations of Zn(II) and Cu(II) in suspension solutions after centrifugation were measured by spectrophotometry (Shanghai Third Analytical Instruments Factory) according to GB 7467-87 DPC. The error of the colorimetric measurements was smaller than 4%. The amount of Zn(II) and Cu(II) adsorbed by the soil particles was calculated based on the mass balance.

2.2.3. Permeability and Unconfined Compressive Strength Tests. The contents of SSA were 1%, 3%, and 5% in the modified clay, respectively. The diameter and height of the clay sample were 61.8 mm and 40 mm in the permeability test, respectively. Additionally, the diameter and height of the soil samples were 39.1 mm and 80 mm in the unconfined compressive strength test, respectively. The density of the clay was 1.60 g/cm³ and its moisture content was 19%. The HCl and NaOH were applied to adjust the pH values (5, 6, 8, and 9) of the chemical solutions, respectively. The modified clay was soaked in chemical solutions for 30 days.

TABLE 3: The basic physical properties of sludge.

pH	Proportion (g/ml)	Content of organic matter (%)	Moisture content (%)	Porosity
6.96	1.24	43.2	80.3	3.36

TABLE 4: The chemical constituents of SSA (%).

SiO ₂	Al ₂ O ₃	Fe ₂ O ₃	CaO	SO ₃	P ₂ O ₅	K ₂ O	MgO	TiO ₂	Na ₂ O	Others
45.5	16.6	8.11	6.64	6.61	5.72	4.45	3.90	0.98	0.83	0.66

According to the standard of soil tests SL237-1999, the hydraulic conductivity and unconfined compressive strength were measured by the TST-55 permeameter and YYW-2 strain controlled unconfined pressure apparatus (Nanjing Ningxi Soil Instrument Co., Ltd.), respectively. All of the tests were repeated three times.

3. Results and Discussion

3.1. Pore Structure. Figure 3 shows the adsorption-desorption isotherm of the modified clay containing SSA. According to IUPAC classification method, the isotherm of clay belongs to the IV category. It is seen from Figure 3 that the adsorption isotherm is a bit of salient when the ratio of P/P_0 is smaller than 0.1. In this stage, the adsorption mainly happens at the micropore wall of clay particles and SSA, and the adsorption amount also gradually achieves saturation in single layer. The adsorption amount gradually increases with the increase of the relative pressure from 0.1 to 0.65. This elucidates the increase of the monolayer molecular amount of the large pore wall and multilayer adsorption in modified clay. The adsorption amount increases dramatically when P/P_0 is larger than 0.65 because the capillary condensation of N₂ occurs in the macropores. The adsorption amount is unable to reach the ultimately saturated level owing to the existence of the pores larger than 10 nm.

The hysteresis loop exists between the adsorption and desorption isotherms, and the differences of the loop shape stand for the differences of the pore structure. The two curves of the adsorption and desorption coincide with each other when P/P_0 is smaller than 0.25, indicating that the micropores of the size of less than 1.38 nm (according to the Kelvin formula [12]) are sealed in one side and opened in the other side, and those of the size of more than 1.38 nm are opened in two sides [13]. Moreover, the adsorption amount of the clay contaminated by alkali solution with pH = 9 is apparently greater than that of the modified clay with contaminated acid solution with pH = 5. The area of the circular adsorption membrane of the clay in alkali solution is greater than that of the acid solution. The capillary condensation of the adsorption appears on the circular adsorption membrane of the pore wall.

On the basis of the standards from the International Theory and Application of Chemical Association (IUPAC), the pore sizes of porous media can be divided into three categories, that is, macropore (>50 nm), mesopore (2 nm~50 nm), and micropore (<2 nm) [14]. Figure 4 depicts the

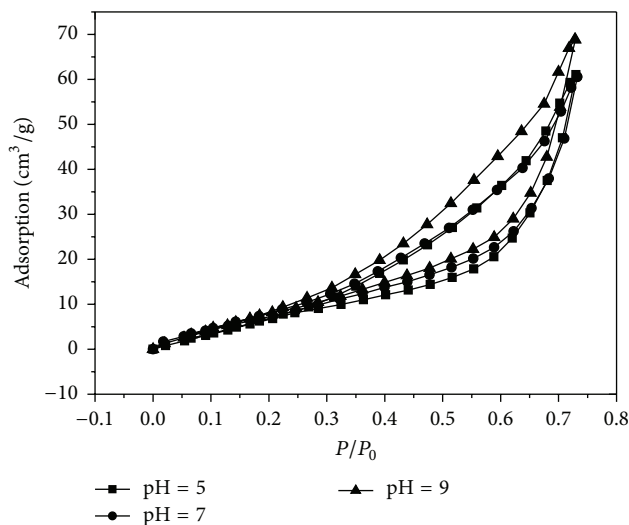


FIGURE 3: The adsorption-desorption isotherm of the modified clay containing SSA.

pore volume and pore size distribution of the modified clay containing SSA. It is observed from Figure 4 that the pore size distributions of the modified clay have wide double shoulder peaks, and the proportions of pore between 2 nm and 7 nm are relatively greater. The curves of the total pore volume of the modified clay tend to the straight lines. When the modified clays are contaminated by acid and alkali chemical solutions, the total pore volume slightly increases at the broad peak. The volumes of the pores between 3 nm and 7 nm increase significantly. However, the volumes of the pores smaller than 2 nm have no apparent changes. The amount of micropore (<2 nm) is decided by the interplanar crystal spacing, and the acid and alkali solutions have a little influence on the mineral lattice [13]. The distributions of the pores from 3 nm to 7 nm are uniform, and the double shoulder peaks of the clay are unobvious. This is attributed to the reason that the acid solution can easily corrode and destroy the mode of the lattice connection inside the minerals.

3.2. Adsorption Capacity. Figures 5 and 6 present the adsorption isotherms for the Zn(II) and Cu(II). The adsorption of Zn(II) and Cu(II) to all specimens is modeled as a Langmuir isotherm, and coefficients of determination (R^2) are greater

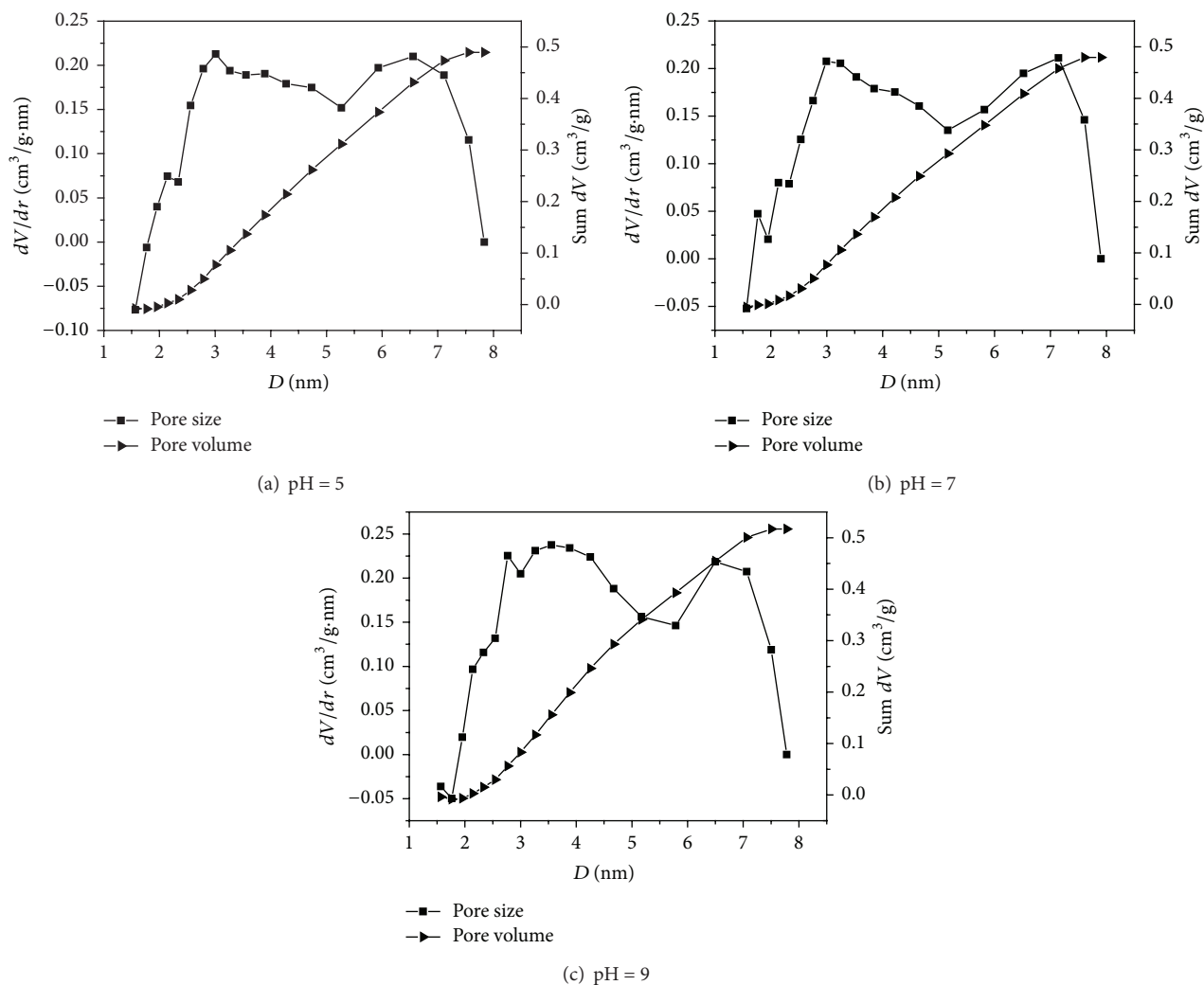


FIGURE 4: The pore volume and pore size of the modified clay containing SSA.

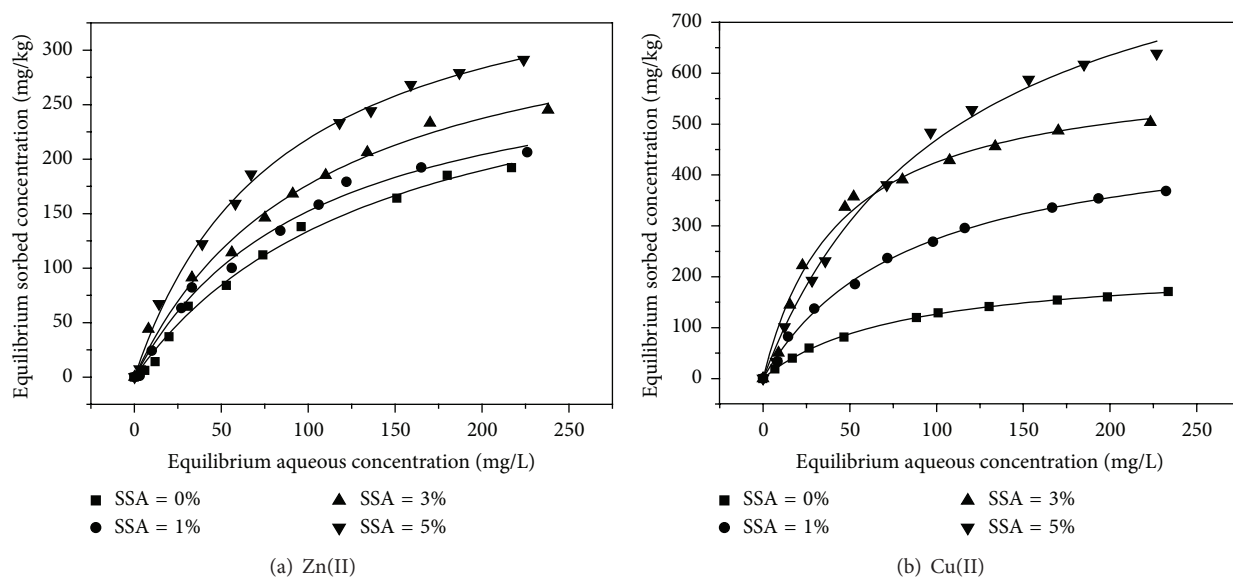


FIGURE 5: Adsorption isotherms for Zn(II) and Cu(II) on the modified clay containing SSA.

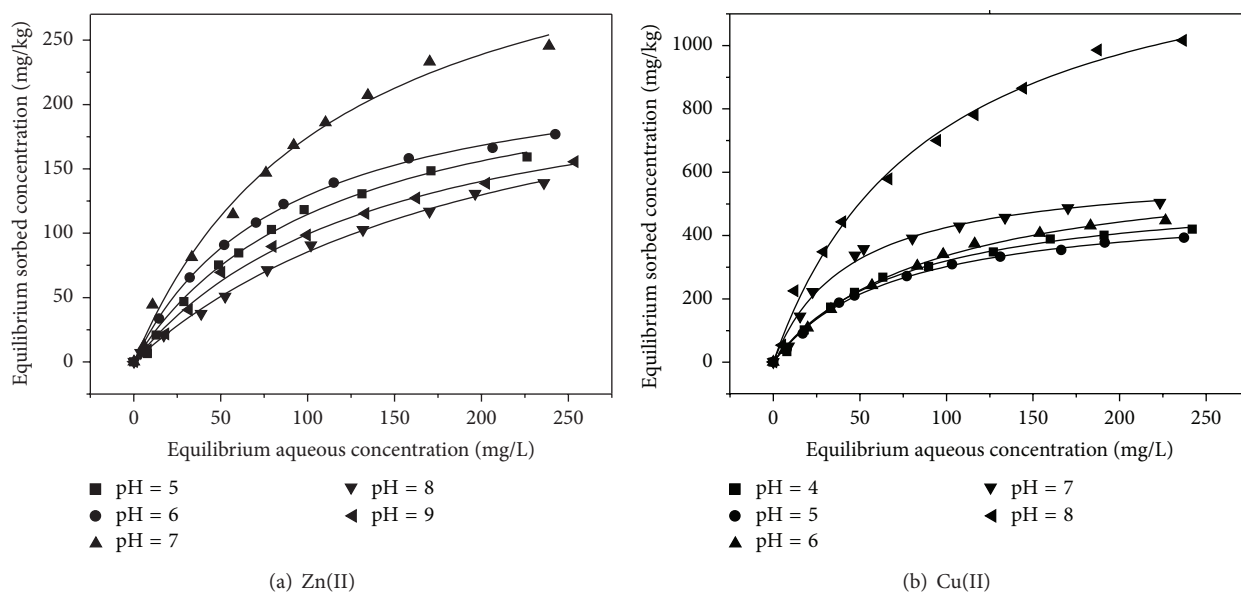


FIGURE 6: Adsorption isotherms for Zn(II) and Cu(II) on the modified clay under acid and alkali chemical solutions.

TABLE 5: The values of isotherm parameters for the modified clay containing SSA.

Elements	0%	1%	3%	5%
Zn(II)				
b (L/mg)	0.00702	0.00966	0.00885	0.0119
q_m (mg/kg)	324.633	309.325	378.250	401.959
R^2	0.993	0.993	0.991	0.997
Cu(II)				
b (L/mg)	0.0126	0.0118	0.0228	0.00913
q_m (mg/kg)	226.925	505.206	610.856	982.218
R^2	0.999	0.997	0.986	0.995

than 0.98. The isotherm parameters for the Zn(II) and Cu(II) are given in Tables 5 and 6.

It can be found from Figures 5(a) and 5(b) that the adsorption capacity of Zn(II) and Cu(II) increases with the content of SSA increasing. In Figure 5(a), the adsorption capacity of Zn(II) increases from 212.44 to 291.99 mg/kg when the equilibrium aqueous concentration is 250 mg/L. Meanwhile, it is also seen from Figure 5(b) that the adsorption capacity of Zn(II) and Cu(II) increases from 171.04 to 638.08 mg/kg under the same equilibrium aqueous concentration. The amount of mesopores with one sealed in a side is large in the SSA. The specific surface area of the SSA is $11.31 \text{ m}^2/\text{g}$. Since there also exist a lot of adsorptive sites on surface, the modified clay has relatively high adsorption capacity of Zn(II) and Cu(II). By the configuration of the extranuclear electrons, Zn(II) is full electronic shell and has swell effect. The amount of extranuclear electrons outside Zn(II) ($[\text{Ar}]3d^{10}$) is larger than that of Cu(II) ($[\text{Ar}]3d^9$), and the radius of Zn(II) is also less than that of Cu(II).

Figure 6 suggests that when the equilibrium aqueous concentration is 250 mg/L, with the increase of the acid and

alkali concentration, the adsorption capacity of Zn(II) to the modified clay declines from 245.62 to 138.14 mg/kg. When the pH value is between 4 and 7, the adsorption capacity of Cu(II) is between 392.25 and 503.27 mg/kg. At pH = 8, the adsorption capacity of Cu(II) to the modified clay rapidly is increased to 1015.67 mg/kg. With the increasing of acid and alkali concentration, the micropore and the gap between the pores are damaged, resulting in mesopores or macropores increases. The amount of pores and specific surface area decline rapidly.

The charges on the surface of the adsorbent are determined by pH value of solutions [15]. With the increase of pH, the concentration of OH^- in the solution increases, which strengthens the repulsive force between the ions and weakened the adsorption capacity of Zn(II) to clay. At pH = 9, it is easy to produce the precipitate $\text{Zn}(\text{OH})_2$. The influence of pH on the adsorption of Cu(II) to the modified clay is unobvious. When the temperature is 25°C , the precipitating equilibrium constant of $\text{Cu}(\text{OH})_2$ (2.2×10^{-20}) is much less than that of $\text{Zn}(\text{OH})_2$ (1.2×10^{-17}). Therefore, it is much easier for the Cu(II) to produce the $\text{Cu}(\text{OH})_2$ precipitate. At pH = 4.5, the precipitating procedure of Cu(II) gradually begins, and $\text{Cu}(\text{OH})_2$ precipitate appears.

3.3. Hydraulic Conductivity. Figure 7 shows the hydraulic conductivity of the modified clay containing SSA. It can be observed from Figure 7 that the hydraulic conductivity of the modified clay declines from 3.62×10^{-8} to 2.17×10^{-8} cm/s with the increasing of SSA at pH = 7. Since the SSA has small particles and rough surface, when the water molecules contacted with the SSA particles, the catapult effect occurs and the water molecules enter the pore which is sealed in a side. Hence, the permeating distance of water molecules becomes longer and the outflow in unit time becomes smaller.

TABLE 6: The values of isotherm parameters for the modified clay under acid and alkali chemical solutions.

Elements	pH = 4	pH = 5	pH = 6	pH = 7	pH = 8	pH = 9
Zn(II)						
b (L/mg)		0.00878	0.0116	0.00885	0.00464	0.00705
q_m (mg/kg)		244.983	240.535	378.250	269.093	239.488
R^2		0.995	0.996	0.994	0.998	0.996
Cu(II)						
b (L/mg)	0.0135	0.0145	0.0108	0.0228	0.0111	
q_m (mg/kg)	566.992	508.639	646.465	610.856	1410.663	
R^2	0.996	0.998	0.998	0.986	0.995	

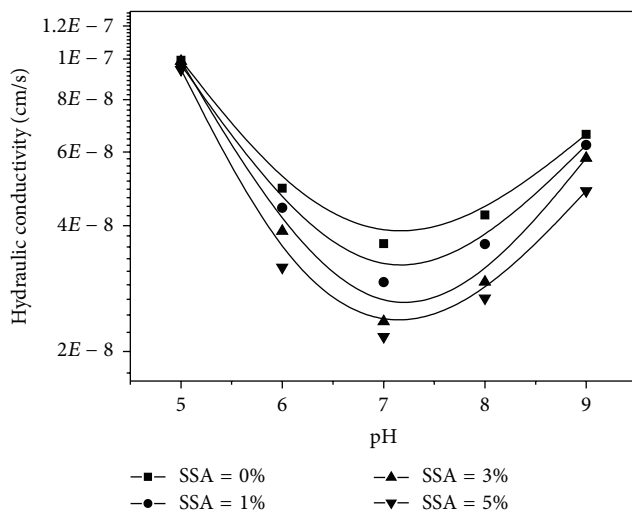


FIGURE 7: The hydraulic conductivity of the modified clay containing SSA.

After the clay containing SSA is contaminated by acid and alkali solutions, the hydraulic conductivity of modified clay increases about 2.2~4.3 times greater than before. And the increase degree of hydraulic conductivity of modified clay contaminated by acid chemical solution is much more obvious and the maximum value of it is 9.93×10^{-8} cm/s. The results of the micropore structure tests indicate that the pore size of SSA is about 8~100 times that of the water molecules [16]. With the increased acid and alkali concentration, the pore structure of SSA shifts from seal in a side to open in both ends, which provides convenient conditions for the pore permeating. Besides, the space skeleton of clay particles also becomes looser, making the flowing of water molecules between the particles pores much easier [17].

3.4. Unconfined Compressive Strength. It is found that the unconfined compressive strength of modified clay increases with an increase of the content of SSA (Figure 8). The unconfined compressive strength of the clay first increases and then decreases with the increase of pH. The modified clay containing 3% SSA has the maximum unconfined compressive strength value of 601.1 kPa. The unconfined compressive strength of modified clay becomes weaker after the action

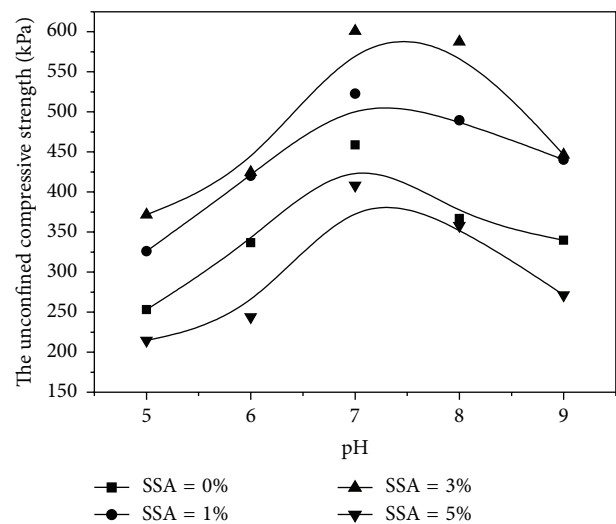


FIGURE 8: The unconfined compressive strength of the modified clay containing SSA.

of acid and alkali solution. For the modified clay containing 3% SSA contaminated by solutions with pH = 5 and pH = 9, the unconfined compressive strength separately declines to 371.6 kPa and 446.4 kPa.

The unconfined compressive strength has relation with factors, such as mineral component, shape, particle size, and cementation property [18, 19]. After the clay is contaminated by acid and alkali solutions, the colloidal matter in the particles, such as organic-inorganic compounded colloid, free oxide, and soluble salt, is corroded. The structural bond force between the clay particles is weakened.

Daniel and Wu suggested that compacted soils used for landfill liners should have a minimum unconfined compressive strength of 200 kPa [20]. As shown in Figure 8, the strength of all specimens meets the engineering requirement of 200 kPa. Thus, the method of adding SSA into compacted clay liners is effective measure to improve compressive strength of the liners.

4. Conclusions

The pores of the modified clay mainly have the micropores smaller than 2 nm and mesopores smaller than 7 nm.

The modified clay containing SSA has obvious adsorption capacity of heavy metal ions. With the increasing of SSA content from 0% to 5%, the adsorption capacity of Zn(II) and Cu(II) increases 37% and 273%, respectively. The hydraulic conductivity of the modified clay range from 3.62×10^{-8} to 2.17×10^{-8} cm/s. When the SSA content is 3%, the unconfined compressive strength peak is 601.1 kPa.

After the clay is contaminated by acid and alkali chemical solutions, the distribution of pore size of clay becomes more uniform and the amount of pore between 2 and 7 nm increases. The adsorption of Zn(II) is declined 35~44%, and the influence on the adsorption of Cu(II) is weakened. The hydraulic conductivity of modified clay increases about 2.2~4.3 times. But the hydraulic conductivity of all soil samples is still smaller than 1×10^{-7} cm/s. The unconfined compressive strength of modified clay becomes smaller, but still larger than 200 kPa.

According to technical code for municipal soil waste sanitary landfill (CJJ17-2004), the modified clay containing SSA can meet the antiseepage and strength requirement of landfill liners. Consequently, improved clay containing SSA can be potentially used as landfill liner-soil materials.

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

Acknowledgments

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