

Research Article

A Simple Predictive Method of Critical Flicker Detection for Human Healthy Precaution

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Interharmonics and flickers have an interrelationship between each other. Based on International Electrotechnical Commission (IEC) flicker standard, the critical flicker frequency for a human eye is located at 8.8 Hz. Additionally, eye strains, headaches, and in the worst case seizures may happen due to the critical flicker. Therefore, this paper introduces a worthwhile research gap on the investigation of interrelationship between the amplitudes of the interharmonics and the critical flicker for 50 Hz power system. Consequently, the significant findings obtained in this paper are the amplitudes of two particular interharmonics are able to detect the critical flicker. In this paper, the aforementioned amplitudes are detected by adaptive linear neuron (ADALINE). After that, the critical flicker is detected by substituting the aforesaid amplitudes to the formulas that have been generated in this paper accordingly. Simulation and experimental works are conducted and the accuracy of the proposed algorithm which utilizes ADALINE is similar, as compared to typical Fluke power analyzer. In a nutshell, this simple predictive method for critical flicker detection has strong potential to be applied in any human crowded places (such as offices, shopping complexes, and stadiums) for human healthy precaution purpose due to its simplicity.

1. Introduction

In the current century, the voltage flicker happens mainly due to the utilization of nonlinear loads such as arc furnace and motor drive [1]. Voltage flicker is a type of voltage fluctuation with certain frequency and it causes visual sensation made by an unsteadiness luminance (light) that fluctuates with time which can cause headache [2]. At present, flicker severity measurement based on IEC flickermeter is widely used in the industries [3]. Short Term Perceptibility (P_{st}) and Long Term Perceptibility (P_{lt}) are assessed in the IEC flickermeter via instantaneous flicker sensation (P_{inst}). P_{st} and P_{lt} are referred to as a recorded data of P_{inst} under observation of 10 minutes and 2 hours, respectively. A number of research works have been carried out to improve accuracy of the flickermeter [4, 5]. Some researchers did investigation on reducing the observation time of P_{st} [6]. Many of the researchers proposed their methods for flicker mitigation in the power system [7, 8].

Furthermore, flicker detection has been carried out based on wavelet Fourier transform [9], atomic method [10], new modified S-transform algorithm [11], and Chirp-z transform [12].

Based on IEC standard, the critical flicker frequency which is the most sensitive to human eyes is located at 8.8 Hz [3]. To be more precise, when the supplied voltage consists of flicker frequency of 8.8 Hz, it will cause the lamp to flick with 8.8 Hz. Additionally, eye strains, headaches, and in the worst case seizures may happen due to the aforementioned lamp flicking [13]. Although this type of flicker causes such significant impact; however, to date, there is no work yet on developing and implementing algorithm to detect critical flicker.

Therefore, this worthwhile research work is to propose a simple predictive method for critical flicker detection (CFD) for human health awareness. Due to the simplicity of the proposed algorithm, it should have strong potential to be applied later in offices, shopping complexes, and stadiums for human comfy.

From a mathematical point of view, a flicker waveform may inherently give some significant changes on the amplitudes of the particular interharmonics [14]. Moreover, the interrelationship between interharmonics and flicker had been provoked due to the concern of proper power quality (PQ) control [2, 15–18]. Therefore, CFD can be done by detecting the particular interharmonics' amplitudes.

A number of signal processing algorithms based on different techniques for interharmonics detection such as fast Fourier transform (FFT), short-time Fourier transform (STFT) [19], and spectrogram [20] have been reported over the past years [21]. STFT and spectrogram algorithms are generated based on FFT. Interharmonics detection based on FFT is widely used in the industries [22]. However, the operation of the FFT may lead to inaccurate result due to phenomena of aliasing [23], leakage [24], and picket fence effects [24].

As an alternative, presently, artificial intelligent algorithms have received special attention from the researchers due to their simplicity, generalization and learning ability. Based on their advantages, the interharmonics are able to be estimated by several artificial intelligent algorithms such as least absolute value (LAV) [25], Kalman filter (KF) [26], adaptive linear neuron (ADALINE) [27], and simulated annealing (SA) [28]. The main advantage of artificial intelligent algorithms (especially ADALINE) is that they can estimate the amplitude and phase rapidly with the condition that the frequencies of the measurement signal need to be initially defined. Specifically, for this work, the critical interharmonics' frequencies are already defined initially based on calculation as further explained in the following section. Therefore, ADALINE is merited as to be utilized in the proposed algorithm as compared to signal processing methods.

This paper presents a work on a simple predictive method of CFD based on interharmonics via ADALINE for human healthy precaution. The organization of this paper is as follows. In Section 2, critical explanation of the relationship between interharmonics and flicker is discussed. After that, the critical flicker frequency is summarized in Section 3. The background of the ADALINE is explained in Section 4. The description of the proposed algorithm is presented in Section 5. Sections 6 and 7 present the simulation and experimental works, respectively, to further verify performance of the proposed algorithm. Finally, the conclusion is presented in Section 8.

2. Relationship between Interharmonics and Flicker

Basically, the appearance of interharmonics in a power system may lead to modulated waveform. The fluctuation frequency of the instantaneous voltage is considered as flicker frequency. The flicker frequency [14], f_{flicker} , can be calculated by

$$f_{\text{flicker}} = |f_{\text{IH}} - f_f|, \quad (1)$$

where f_{IH} is the interharmonic frequency and f_f is the fundamental frequency of the power system. For example, if the flicker frequency is defined as 3 Hz and the fundamental frequency is 50 Hz, the interharmonics are 47 Hz and 53 Hz. Practically, the flicker may present due to a single interharmonic (47 or 53 Hz) or a pair of interharmonics (47 and 53 Hz together). Starting from fundamental principle, the relationship is investigated by deriving the formula of flicker produced by single interharmonic. The following equation shows the relation between exponential, sine, and cosine functions:

$$Ae^{j\omega t} = A (\cos(\omega t) + j \sin(\omega t)), \quad (2)$$

where A and ω are represented as amplitude and particular angular frequency, respectively. The following equation represents the instantaneous voltage with combination of single interharmonic ($v_1(t)$) in exponential form:

$$v_1(t) = \alpha_1 e^{j\omega_1 t} + \alpha_2 e^{j\omega_2 t}, \quad (3)$$

where α_1 and ω_1 are represented as fundamental amplitude and its angular frequency. Meanwhile, α_2 and ω_2 are symbolized as the interharmonic amplitude and its angular frequency.

After the elaboration,

$$v_1(t) = e^{j\omega_1 t} (\alpha_1 + \alpha_2 e^{j(\omega_2 - \omega_1)t}). \quad (4)$$

The $e^{j\omega_1 t}$ is represented as factorized exponential form of fundamental frequency. The instantaneous amplitude is summarized as $\alpha_1 + \alpha_2 e^{j(\omega_2 - \omega_1)t}$. Somehow, the instantaneous amplitude can be calculated as follows:

$$\text{Amp}_{\cdot 1H} = |\alpha_1 + \alpha_2 e^{j(\omega_2 - \omega_1)t}|. \quad (5)$$

The equation can be rewritten as follows:

$$\begin{aligned} \text{Amp}_{\cdot 1H} &= |\alpha_1 + \alpha_2 \cos(\omega_2 - \omega_1)t + j\alpha_2 \sin(\omega_2 - \omega_1)t|, \end{aligned} \quad (6)$$

where $\alpha_1 + \alpha_2 \cos(\omega_2 - \omega_1)t$ and $\alpha_2 \sin(\omega_2 - \omega_1)t$ are represented as real and imaginary parts, respectively. In order to calculate the amplitude, the aforementioned real and imaginary parts are set as modulus as follows:

$$\begin{aligned} \text{Amp}_{\cdot 1H} &= \sqrt{[\alpha_1 + \alpha_2 \cos(\omega_2 - \omega_1)t]^2 + [\alpha_2 \sin(\omega_2 - \omega_1)t]^2}. \end{aligned} \quad (7)$$

Thus,

$$\text{Amp}_{\cdot 1H} = \sqrt{\alpha_1^2 + \alpha_2^2 \cos^2(\omega_2 - \omega_1)t + 2\alpha_1\alpha_2 \cos(\omega_2 - \omega_1)t + \alpha_2^2 \sin^2(\omega_2 - \omega_1)t}. \quad (8)$$

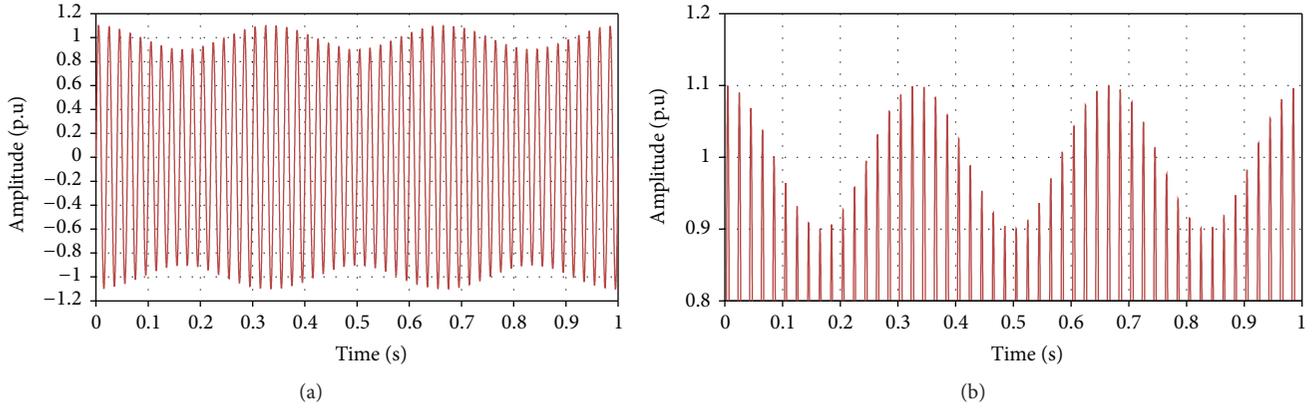


FIGURE 1: Flicker waveform caused by single interharmonic: (a) zoom-out version and (b) zoom-in version.

Finally, the instantaneous amplitude is summarized as follows:

$$\text{Amp}_{.1H} = \sqrt{\alpha_1^2 + \alpha_2^2 + 2\alpha_1\alpha_2 \cos(\omega_2 - \omega_1)t}. \quad (9)$$

In order to estimate the maximum and minimum of the instantaneous voltage, the $\cos(\omega_2 - \omega_1)t$ is substituted to 1 and -1, respectively. Therefore, the formulas for maximum and minimum of the instantaneous voltage are shown as follows:

$$\begin{aligned} \text{Amp}_{.1H}\max &= \sqrt{\alpha_1^2 + \alpha_2^2 + 2\alpha_1\alpha_2(1)} \\ \text{Amp}_{.1H}\min &= \sqrt{\alpha_1^2 + \alpha_2^2 + 2\alpha_1\alpha_2(-1)}. \end{aligned} \quad (10)$$

Thus, as to evaluate the severity of the flicker, relative fluctuation ($\Delta v/v$) is needed to be calculated by using the following formula:

$$\frac{\Delta v}{v} = \frac{\text{Amp}_{.1H}\max - \text{Amp}_{.1H}\min}{\alpha_1} \times 100. \quad (11)$$

In relation to 50 Hz voltage supply, it consists of single interharmonic of 47 Hz with 0.1 p.u. (α_2), as shown in Figure 1. In more detail, Figures 1(a) and 1(b) show the zoom-out and zoom-in versions of the waveform, respectively. Based on Figure 1(b), flicker frequency of 3 Hz can be seen obviously. At the same time, the flicker frequency can be calculated manually via (1). Based on Figure 1, the maximum and minimum of the fluctuation voltage are 1.1 and 0.9 p.u., respectively. Assume the amplitude of fundamental (α_1) and interharmonic (α_2) are already determined, which are 1 and 0.1 p.u., respectively. After that, the maximum and minimum of the instantaneous voltage can be obtained by (10), which are 1.1 and 0.9 p.u., respectively. The values that are calculated via (10) are proven to be similar to the maximum and minimum of the instantaneous values in Figure 1. Furthermore, the $\Delta v/v$ can be calculated by (11) and the $\Delta v/v$ for Figure 1 as can be seen obviously is 20%. Based on the explanation above, the amplitudes of fundamental (α_1) and interharmonic (α_2) are the key values to identify $\Delta v/v$.

In more practical situation, flicker waveform may occur due to a pair of interharmonics. Therefore, the derivation of formula for aforementioned situation is shown as follows:

$$v_2(t) = \alpha_3 e^{j\omega_3 t} + \alpha_1 e^{j\omega_1 t} + \alpha_2 e^{j\omega_2 t}. \quad (12)$$

The $v_2(t)$, α_1 , and ω_1 are represented as the instantaneous voltage for a pair of interharmonics, fundamental amplitude, and angular frequency (fundamental), respectively. Meanwhile, the α_2 and ω_2 are symbolized as the first interharmonic amplitude and its angular frequency. Finally, the α_3 and ω_3 are represented as the second interharmonic amplitude and its angular frequency. The relationship of ω is assumed as $\omega_3 < \omega_1 < \omega_2$.

After that, the aforementioned instantaneous voltage becomes

$$v_2(t) = e^{j\omega_1 t} (\alpha_1 + \alpha_2 e^{j(\omega_2 - \omega_1)t} + \alpha_3 e^{j(\omega_3 - \omega_1)t}). \quad (13)$$

The $e^{j\omega_1 t}$ is represented as factorized exponential form of fundamental frequency. The amplitude is represented as $\alpha_1 + \alpha_2 e^{j(\omega_2 - \omega_1)t} + \alpha_3 e^{j(\omega_3 - \omega_1)t}$. Therefore, the amplitude can be calculated as follows:

$$\text{Amp}_{.2H} = |\alpha_1 + \alpha_2 e^{j(\omega_2 - \omega_1)t} + \alpha_3 e^{j(\omega_3 - \omega_1)t}|. \quad (14)$$

After the expansion,

$$\begin{aligned} \text{Amp}_{.2H} &= |\alpha_1 + \alpha_2 \cos(\omega_2 - \omega_1)t \\ &\quad + j\alpha_2 \sin(\omega_2 - \omega_1)t + \alpha_3 \cos(\omega_3 - \omega_1)t \\ &\quad + j\alpha_3 \sin(\omega_3 - \omega_1)t|. \end{aligned} \quad (15)$$

In order to calculate the amplitude, the aforementioned real and imaginary parts are set as modulus as follows:

$$\begin{aligned} \text{Amp}_{.2H} &= \left[[\alpha_1 + \alpha_2 \cos(\omega_2 - \omega_1)t + \alpha_3 \cos(\omega_3 - \omega_1)t]^2 \right. \\ &\quad \left. + [\alpha_2 \sin(\omega_2 - \omega_1)t + \alpha_3 \sin(\omega_3 - \omega_1)t]^2 \right]^{1/2}. \end{aligned} \quad (16)$$

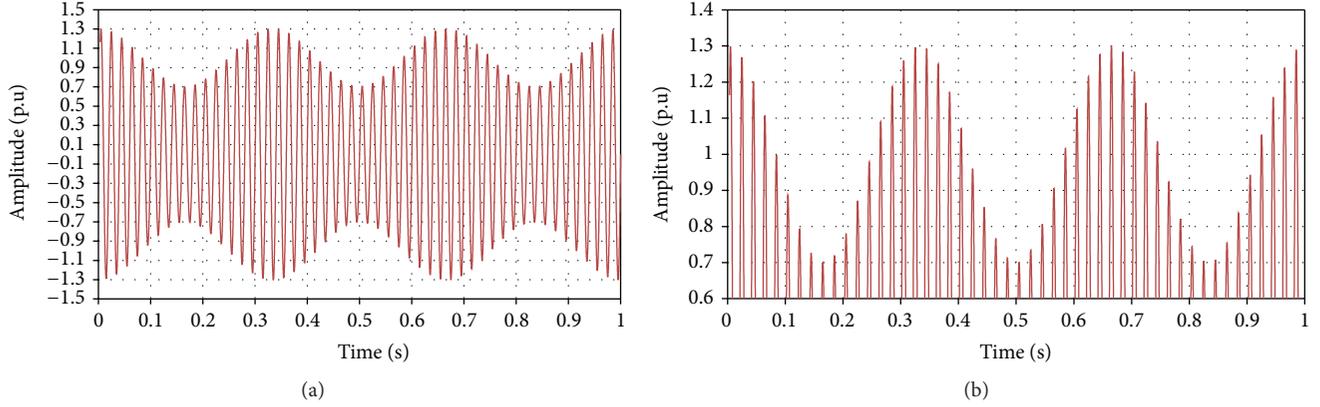


FIGURE 2: Flicker waveform caused by a pair of interharmonics: (a) zoom-out version and (b) zoom-in version.

Further elaboration is

$$\begin{aligned}
 \text{Amp}_{2H} = & \left[2\alpha_1\alpha_2 \cos(\omega_2 - \omega_1)t \right. \\
 & + 2\alpha_1\alpha_3 \cos(\omega_3 - \omega_1)t \\
 & + 2\alpha_2\alpha_3 \cos(\omega_2 - \omega_1)t \cos(\omega_3 - \omega_1)t + \alpha_1^2 \\
 & + \alpha_2^2 \cos^2(\omega_2 - \omega_1)t + \alpha_3^2 \cos^2(\omega_3 - \omega_1)t \\
 & + \alpha_2^2 \sin^2(\omega_2 - \omega_1)t \\
 & + 2\alpha_2\alpha_3 \sin(\omega_2 - \omega_1)t \sin(\omega_3 - \omega_1)t \\
 & \left. + \alpha_3^2 \sin^2(\omega_3 - \omega_1)t \right]^{1/2}. \quad (17)
 \end{aligned}$$

Since

$$\begin{aligned}
 \omega_3 & < \omega_1 < \omega_2, \\
 \omega_3 - \omega_1 & = \omega_2 - \omega_1, \quad (18)
 \end{aligned}$$

then,

$$\begin{aligned}
 \text{Amp}_{2H} = & \left[2\alpha_1\alpha_2 \cos(\omega_2 - \omega_1)t \right. \\
 & + 2\alpha_1\alpha_3 \cos(\omega_3 - \omega_1)t + 2\alpha_2\alpha_3 \cos^2(\omega_2 - \omega_1)t \\
 & + \alpha_1^2 + \alpha_2^2 \cos^2(\omega_2 - \omega_1)t + \alpha_3^2 \cos^2(\omega_3 - \omega_1)t \\
 & + \alpha_2^2 \sin^2(\omega_2 - \omega_1)t + 2\alpha_2\alpha_3 \sin^2(\omega_2 - \omega_1)t \\
 & \left. + \alpha_3^2 \sin^2(\omega_3 - \omega_1)t \right]^{1/2}. \quad (19)
 \end{aligned}$$

By simplifying using trigonometry identity,

$$\begin{aligned}
 \text{Amp}_{2H} = & \left[2\alpha_1\alpha_2 \cos(\omega_2 - \omega_1)t \right. \\
 & + 2\alpha_1\alpha_3 \cos(\omega_3 - \omega_1)t + 2\alpha_2\alpha_3 + \alpha_1^2 + \alpha_2^2 \\
 & \left. + \alpha_3^2 \right]^{1/2}. \quad (20)
 \end{aligned}$$

Therefore, the simplified version is

$$\begin{aligned}
 \text{Amp}_{2H} \\
 = & \sqrt{[2\alpha_1(\alpha_2 + \alpha_3) \cos(\omega_2 - \omega_1)t + 2\alpha_2\alpha_3 + \alpha_1^2 + \alpha_2^2 + \alpha_3^2]}. \quad (21)
 \end{aligned}$$

The maximum of the instantaneous voltage is

$$\begin{aligned}
 \text{Amp}_{2H\text{max}} \\
 = & \sqrt{[2\alpha_1(\alpha_2 + \alpha_3)(1) + 2\alpha_2\alpha_3 + \alpha_1^2 + \alpha_2^2 + \alpha_3^2]}. \quad (22)
 \end{aligned}$$

The minimum of the instantaneous voltage is

$$\begin{aligned}
 \text{Amp}_{2H\text{min}} \\
 = & \sqrt{[2\alpha_1(\alpha_2 + \alpha_3)(-1) + 2\alpha_2\alpha_3 + \alpha_1^2 + \alpha_2^2 + \alpha_3^2]}. \quad (23)
 \end{aligned}$$

The maximum and minimum of the instantaneous voltage can be calculated by substituting the $\cos(\omega_2 - \omega_1)t$ to 1 and -1, respectively. In another application of 50 Hz voltage supply, where it consists of interharmonics of 47 Hz (ω_3) with 0.1 p.u. (α_3) and 53 Hz (ω_2) with 0.2 p.u. (α_2), the flicker waveform is shown in Figure 2. Based on Figure 2, the maximum and minimum of the instantaneous voltage are 1.3 and 0.7 p.u., respectively. Assume the amplitudes of first interharmonic (α_3), fundamental (α_1), and second interharmonic (α_2) are already determined, which are 0.1, 1, and 0.2 p.u., respectively. The maximum and minimum of the instantaneous voltages can be calculated by (22) and (23), which are 1.3 and 0.7 p.u., respectively. Therefore, the formulas that are generated in this paper ((22) and (23)) are proven to be correct via comparing the calculation's values and the values in Figure 2.

For Figure 2, the relative fluctuation voltage ($\Delta v/v$) is

$$\frac{\Delta v}{v} = \frac{\text{Amp}_{2H\text{max}} - \text{Amp}_{2H\text{min}}}{\alpha_1} \times 100. \quad (24)$$

The calculated value is 60%. Again, the amplitudes of fundamental (α_1) and two interharmonics (α_2 and α_3) are crucial to identify $\Delta v/v$.

To recap, the voltage flicker happens mainly due to overload condition. From a mathematical point of view, any generated flicker may produce significant effect to the amplitudes of the particular inter-harmonics [14]. Therefore, the relationship between interharmonics and flicker frequency is discussed clearly above. In addition, the formula for maximum and minimum of instantaneous voltage and relative fluctuation voltage is being discussed too. Finally, the amplitudes

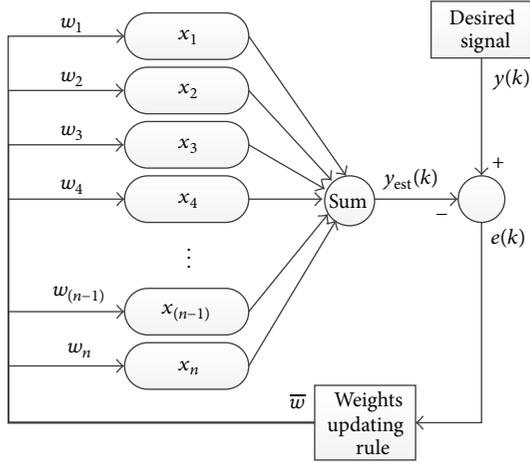


FIGURE 3: Block diagram of the ADALINE configuration.

of fundamental (α_1) and two interharmonics (α_2 and α_3) are found to be crucial in order to identify $\Delta v/v$. The usage of $\Delta v/v$ will be discussed in the next section.

3. Critical Flicker Frequency

Based on IEC standard, the critical flicker frequency which is the most sensitive to human eyes is located at 8.8 Hz sinusoidal wave with relative fluctuation voltage ($\Delta v/v$) of 0.25% [3]. To be more precise, when the supplied voltage consists of flicker frequency of 8.8 Hz sinusoidal wave with $\Delta v/v$ of 0.25%, it will cause the lamp to flick with 8.8 Hz and it may cause human headache. From a mathematical point of view, any flicker waveform may increase the amplitudes of the particular interharmonics [14]. Based on (1), when the critical flicker (8.8 Hz) happens, it will cause amplitudes of 41.2 Hz ($50 - 8.8$) and 58.8 Hz ($50 + 8.8$) to increase indirectly for 50 Hz power system. As discussed above, detection of amplitudes for 41.2, 50, and 58.8 Hz is crucial to identify the maximum and minimum of the instantaneous voltage so that the $\Delta v/v$ can be calculated precisely. If the $\Delta v/v$ is greater than 0.25%, the critical flicker will be detected. Last but not least, eye strains, headaches, and in the worst case seizures [13] may happen due to the critical voltage flicker. Therefore, a simple predictive method for CFD is needed for human health awareness.

4. Background of ADALINE

ADALINE is operated upon on learning rule and it can learn accurately with multiple loops by reducing the error between the estimation and input signals [29]. Figure 3 shows the structure of the ADALINE. The desired signal $y(k)$ can be represented as Fourier series equation, or

$$y(k) = \sum_{n=1,2,3,\dots}^N A_n \sin(nk\omega t_s + \theta_n). \quad (25)$$

After being simplified by trigonometry identity,

$$y(k) = \sum_{n=1,2,3,\dots}^N w_{1n} \sin(nk\omega t_s) + w_{2n} \cos(nk\omega t_s). \quad (26)$$

The formula of weights updating rule is

$$w(k+1) = w(k) + \frac{\alpha e(k) x(k)}{x^T(k) x(k)}, \quad (27)$$

where α is the learning rate, $x(k)$ is the sine and cosine vector for reference signal, $e(k)$ is the error between desired signal ($y(k)$) and estimation ($y_{\text{est}}(k)$) signal, and $w(k)$ is the estimation amplitude for $x(k)$.

First, the $w(k)$ in the weights updating rule starts with zero (initial value) and a large value of error occurs at the first iteration. After some number of iterations, the $e(k)$ will be lesser since the estimation signal will be almost similar to the desired signal. The learning rate is the heart of the weights updating rule as it can control the learning speed of the system. Thus, a suitable learning rate is needed to be determined. A large value of learning rate increases the learning speed but decreases the accuracy and vice versa. In addition, the sampling frequency of the entire system can influence the learning speed. Through this method, the estimation signal will be similar to the desired signal after some looping processes. After that, the real and imaginary values of the desired signal can be extracted from $w(k)$. Finally, the amplitude for harmonic and inter-harmonic signals can be calculated via the following formula:

$$A_n = \sqrt{w_{n-1}^2 + w_n^2} = \sqrt{A_n \cos^2 \theta_n + A_n \sin^2 \theta_n}. \quad (28)$$

5. Proposed Algorithm

As discussed above, the amplitudes of the particular interharmonics are the key values to determine the severity of the flicker level. Therefore, the proposed algorithm utilizes the ADALINE as the amplitudes detector for the fundamental component and interharmonics component. The design of the ADALINE for CFD is shown in Figure 4. After that, the particular amplitudes are substituted into (22) and (23) for determining the maximum and minimum of the fluctuation voltage. Next, the relative fluctuation voltage ($\Delta v/v$) is calculated via (24). If the percentage of $\Delta v/v$ is greater than 0.25%, critical flicker will be detected. Block diagram of the proposed algorithm is shown in Figure 5.

6. Simulation Results

The proposed algorithm is developed, configured, and simulated in MATLAB Simulink. The learning rate of the ADALINE is 0.01. The simulation work is separated into 3 parts. The first part is to determine the most suitable sampling frequency for the ADALINE algorithm. Next, the critical flicker signal with noiseless condition is analyzed. Lastly, the critical flicker signal with signal noise ratio (SNR) of 30~10 dB condition is analyzed. Subsequently, based on IEC standard

TABLE 1: Data analysis for the response waveforms obtained from the fundamental voltage via ADALINE.

Number	Sampling frequency (Hz)	Rise time (s)	Overshoot (%)	Settling time (s)	Condition
1	51200	0.06	44.64	1	Underdamped
2	25600	0.07	27.64	0.5	Underdamped
3	12800	0.1	4.11	0.25	Optimum
4	6400	0.57	0	0.57	Overdamped
5	3200	1.08	0	1.08	Overdamped
6	1600	2	0	2	Overdamped

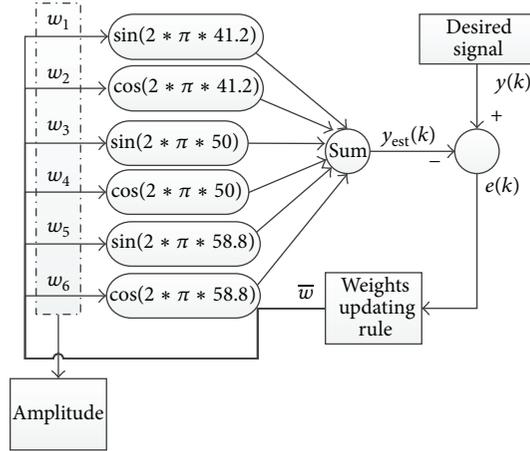


FIGURE 4: Block diagram of the ADALINE for critical flicker detection.

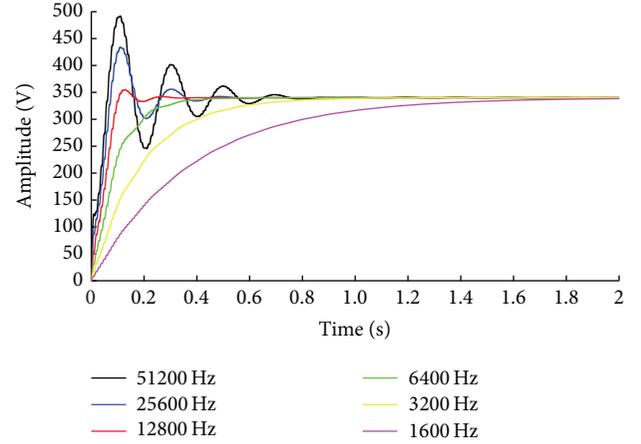


FIGURE 6: Response waveforms obtained from the fundamental voltage via ADALINE.

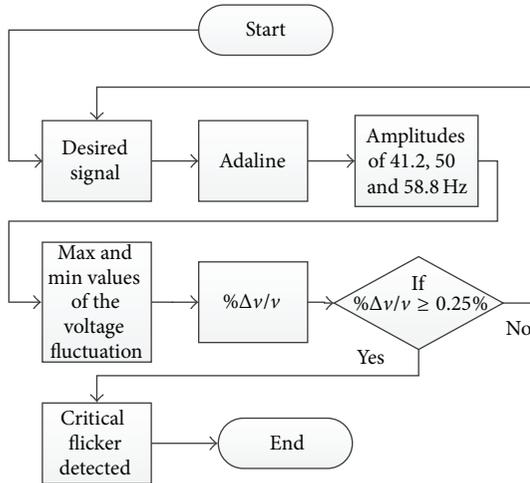


FIGURE 5: Block diagram for the proposed algorithm.

[3], the formula of the critical voltage flicker shown as follows will be used in the simulation work:

$$u(t) = V_1 \times \sqrt{2} \sin(2\pi f_1 t) \times \left\{ 1 + \frac{\Delta v/v}{100} (0.5) \sin(2\pi f_f t) \right\}, \quad (29)$$

where V_1 is the supplied voltage (rms), f_1 is the fundamental frequency, f_f is the flicker frequency, and $\Delta v/v$ is the relative fluctuation voltage.

Based on the equation above, V_1 , f_1 , f_f , and $\Delta v/v$ are configured as 240 V, 50 Hz, 8.8 Hz, and 0.25%, respectively.

Part 1: Sampling Frequency of the ADALINE Algorithm. The critical flicker waveform (29) is analyzed via ADALINE algorithm with various sampling frequencies from 1600 Hz to 51200 Hz. The response waveforms obtained from the fundamental voltage are shown in Figure 6. Ideally, the steady state value for the fundamental voltage is 340 V. Based on the aforementioned response waveforms, the sampling frequencies of 51200 Hz and 25600 Hz are considered as underdamped condition. Meanwhile, overdamped condition is represented by response waveforms for sampling frequencies of 6400 Hz, 3200 Hz, and 1600 Hz. Table 1 shows the data analysis for the response waveforms obtained from the fundamental voltage via ADALINE, as shown in Figure 6. Subsequently, the sampling frequency of 12800 Hz is considered as optimum sampling frequency as it is able to operate the ADALINE with finest rise time, overshoot, and settling time. Therefore, the sampling frequency of 12800 Hz is justified to be used later in both simulation and experiment works.

Part 2: Critical Voltage Flicker Generation (Noiseless). The critical flicker waveform generated from (29) is shown in Figure 7. The zoom-in version of the critical flicker waveform

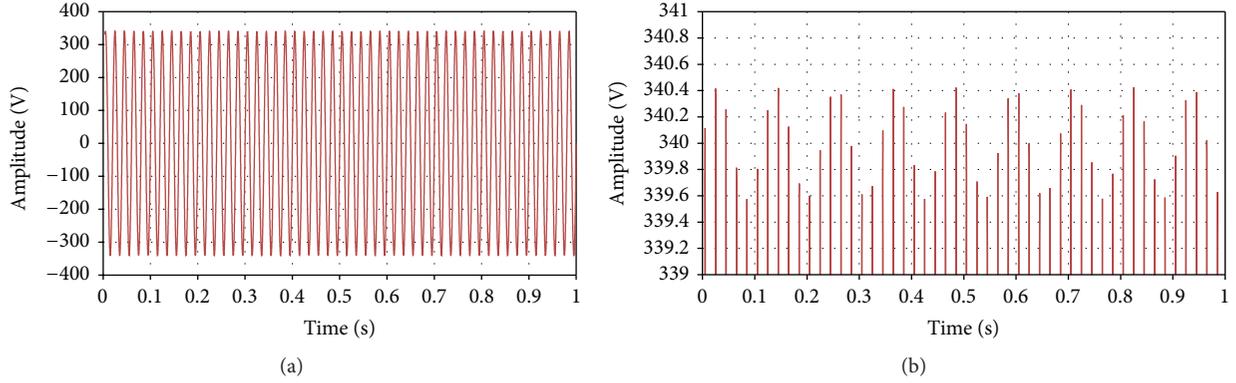


FIGURE 7: Critical flicker waveform (29): (a) zoom-out version and (b) zoom-in version.

TABLE 2: Summary of data analysis for the proposed algorithm (Simulation).

	Ref.	SNR (dB)				
		30	25	20	15	10
ADALINE output						
41.2 Hz	0.213	0.214	0.214	0.216	0.218	0.223
ϵ (%)		0.485	0.861	1.567	2.791	4.909
50 Hz	340.000	340.000	340.000	340.000	340.000	340.000
ϵ (%)		0.000	0.000	0.000	0.000	0.000
58.8 Hz	0.213	0.214	0.214	0.216	0.218	0.222
ϵ (%)		0.235	0.610	1.174	2.254	4.131
Calculation						
Max	340.426	340.427	340.429	340.431	340.436	340.445
ϵ (%)		0.000	0.000	0.000	0.000	0.000
Min	339.574	339.573	339.571	339.569	339.564	339.555
ϵ (%)		0.000	0.001	0.002	0.003	0.006
$\% \Delta v/v$	0.251	0.251	0.252	0.254	0.257	0.262
ϵ (%)		0.235	0.610	1.244	2.394	4.390

is shown in Figure 7(b). Based on Figure 7, the voltage waveform is fluctuated between 340.426 and 339.574 V. Therefore the Δv is 0.852 V and the relative $\Delta v/v$ is 0.25%.

For the proposed algorithm, the output of the ADALINE for critical flicker waveform (Figure 7) is 0.213, 340, and 0.213 V for 41.2, 50, and 58.8 Hz, respectively. The values of 0.213, 340, and 0.213 V that represent α_3 , α_1 , and α_2 are substituted into (22) and (23). The maximum and minimum amplitudes values based on calculation are 340.426 and 339.574 V. The obtained maximum and minimum amplitudes are proven to be similar as the values obtained in the simulation work (Figure 7).

Part 3: Voltage Flicker Generation (with Signal Noise Ratio (SNR) of 30~10 dB). The robustness of the proposed algorithm is further analyzed in this part. The critical flicker waveform (equation (29)) is added with SNR of 30 dB to 10 dB. SNR of 30 dB is able to simulate the noise level for practical measurement [30]. Figure 8 shows the aforementioned critical flicker waveform with SNR of 30 dB and 10 dB. Critical flicker waveform in Figure 8 with SNR of 10 dB is more noisy than

30 dB as the value of SNR is inverse proportional with the noise level. The performance index (ϵ) is utilized in this simulation for measuring the accuracy of the detection which is calculated by

$$\epsilon = \frac{|\text{reference} - \text{measurement}|}{\text{reference}} \times 100\%, \quad (30)$$

where the reference value is the actual value (without noise) and the measurement is the measurement with SNR. In this case, small value of ϵ represents higher accuracy of the measurement and vice versa. The summary of data analysis for the proposed algorithm is listed in Table 2. The ϵ of the analysis is not more than 5%. Therefore, the proposed algorithm has potential to be applied in any threatening power quality condition.

7. Experimental Results

The experimental setup (Figure 9) for CFD is conducted by using a programmable AC source model 6590. The flicker waveform with 8.8 Hz flicker frequency is generated by

TABLE 3: Summary of data analysis for the proposed algorithm (experimental).

Amplitude level (V)	ADALINE output			Calculation			Critical Flicker	Fluke (P_{inst})	Accuracy
	41.2 Hz	50 Hz	58.8 Hz	Max (22)	Min (23)	$\% \Delta v/v$ (24)			
239.00	0.20	336.10	0.43	336.73	335.47	0.37	YES	4.22	100%
239.10	0.18	336.10	0.39	336.68	335.52	0.34	YES	3.52	100%
239.20	0.27	336.20	0.27	336.74	335.66	0.32	YES	2.50	100%
239.30	0.29	336.30	0.27	336.86	335.74	0.33	YES	2.05	100%
239.40	0.31	336.40	0.19	336.90	335.90	0.30	YES	1.55	100%
239.50	0.08	336.50	0.25	336.83	336.17	0.19	NO	0.90	100%
239.60	0.21	336.50	0.13	336.84	336.16	0.20	NO	0.61	100%
239.70	0.25	336.60	0.05	336.90	336.30	0.18	NO	0.39	100%
239.80	0.18	336.70	0.12	337.00	336.40	0.18	NO	0.10	100%
239.90	0.10	336.70	0.16	336.96	336.44	0.16	NO	0.03	100%
240.00	0.14	336.80	0.17	337.11	336.49	0.18	NO	0.00	100%

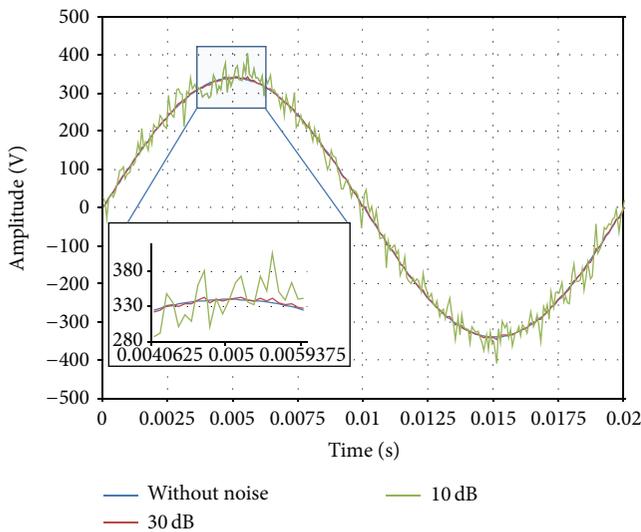


FIGURE 8: Critical flicker waveform of (29) with SNR of 30 dB and 10 dB.

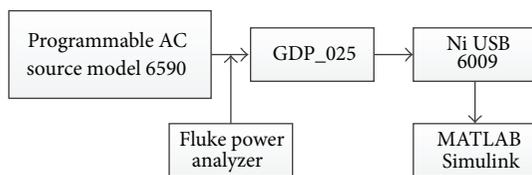


FIGURE 9: Configuration block for the experimental work.

aforementioned programmable AC. In order to evaluate the robustness of the proposed algorithm, various amplitudes of flicker are investigated. Typical Fluke power analyzer (P_{inst}) is employed as the benchmarking tool. Ni USB 6009 and Gw Instek differential probe GDP_025 are utilized as data acquisition. The sampling frequency of the experimental work is 12800 Hz with fundamental frequency of 50 Hz. The learning rate of the ADALINE is 0.01. Finally, the data is exported to MATLAB Simulink to be further analyzed by the proposed algorithm.

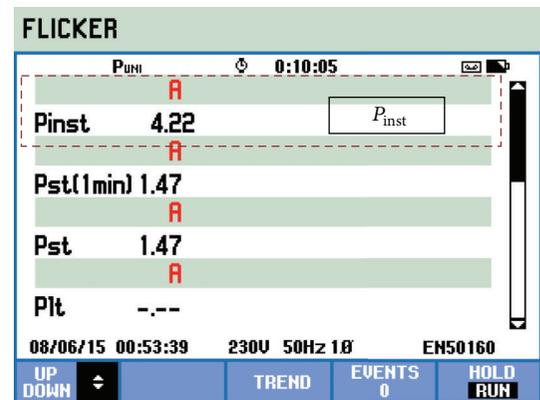


FIGURE 10: Fluke power analyzer's results for flicker voltage amplitude (rms) of 239 V.

The voltage supply (rms) is 240 V. After that, the voltage waveform is interrupted by an envelope pulse (8.8 Hz) which is generated by the programmable AC source model 6590. The amplitude of the envelope pulse is varied voltage (rms) from 239 to 240 V with increasing step size of 0.1 V. Therefore, 11 sets of test are conducted. Based on Table 3, the flicker waveform is analyzed by the ADALINE. After that, the outputs of the ADALINE are substituted into (22), (23), and (24) accordingly for determining the maximum, minimum, and relative fluctuation voltage, respectively. If the value of relative fluctuation voltage is more than 0.25%, the critical flicker is detected. At the same time, the flicker waveforms are analyzed by the typical Fluke power analyzer (P_{inst}) (Figure 10). P_{inst} is utilized as the suitable benchmarking parameter in this experimental part. According to IEC flickermeter's calibration procedure, P_{inst} must show 1 when 8.8 Hz sinusoidal voltage with relative fluctuation voltage 0.25% is injected to the flickermeter [31]. Therefore, when P_{inst} is more than or equal to 1, critical flicker is detected. Figure 11 shows the data analysis for the experimental work. The proposed algorithm is able to detect the critical flicker accurately. In a nutshell, the accuracy of the proposed algorithm is similar, as compared with the typical Fluke power analyzer.

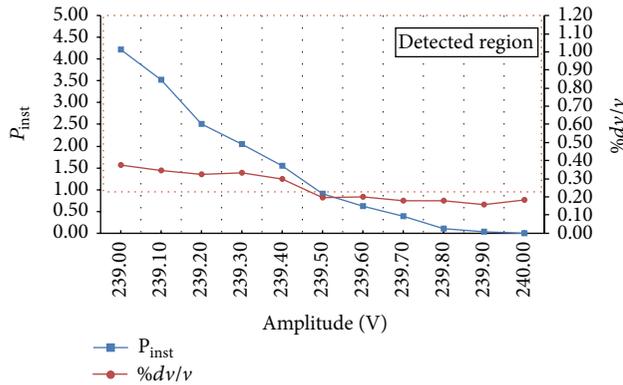


FIGURE 11: Data analysis for the experimental work.

8. Conclusion

This paper has presented a simple predictive method of critical flicker detection algorithm for human health precaution based on amplitude of the particular interharmonics. The interrelationship between amplitude level for the particular interharmonics and critical flicker is explained and the related formulas are derived clearly in this paper. The significant findings obtained in this paper are the amplitudes of two particular interharmonics are able to identify the severity of the critical flicker. Based on the aforementioned findings, 41.2 and 58.8 Hz are summarized as the critical interharmonics for the critical flicker. After that, the amplitude of the aforementioned interharmonics are substituted into (22), (23), and (24) accordingly for determining the severity of the critical flicker. The robustness of the proposed algorithm is evaluated in both simulation and experimental works. Additionally, typical Fluke power analyzer (P_{inst}) is utilized as benchmarking for the proposed algorithm. Finally, the accuracy of the proposed algorithm is similar, as compared to typical Fluke power analyzer. Last but not least, the proposed algorithm has potential to be applied in any crowded human places (such as office, shopping complex, and stadium) for human healthy precaution purpose.

Conflict of Interests

The authors declare that there is no conflict of interests regarding the publication of this paper.

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