

Research Article

Magnetization for Burgers' Fluid Subject to Convective Heating and Heterogeneous-Homogeneous Reactions

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The flow of Burgers' fluid in the magnetic field new mathematical modeling is introduced in this article which is heated convectively and maintained. The thermal energy transport aspects are examined by employing the space- and temperature-related heat source. In the present investigation, the homogeneous-heterogeneous reactions will present the features of scrutiny of the fluid concentration. For the purpose of dimensionless similarity transformations, ordinary differential equations (ODEs) are utilized practically. Developed ODEs are solved by introducing the concepts of Runge-Kutta-Fehlberg's fourth-fifth method. The graphs show the pertinent outcome. The relaxation time parameter is exhibited by diminishing the thermal distribution of Burgers' fluid property, and this will depend on the relaxation time factor. Biot number and retardation time factor behaviors are analyzed by opposing the behavior of the material factor of Burgers' fluid. The response of homogeneous strength is deteriorated by the concentration rate of the fluid, and this will augment the data using the heterogeneous response with greater magnitude. By using already published studies, it is investigated that the present investigation is validated.

1. Introduction

Fundamentally, Burgers' liquid is a non-Newtonian liquid. The non-Newtonian substance has critical significance and parcel of actual applications because of which specialists and designers are giving their consideration towards this subject. A large portion of the materials utilized in the petrochemical, biochemical, and geophysical impacts are non-Newtonian. On account of their various attributes, a few sorts of non-Newtonian models have been set up. These materials are present as differential, fundamental, and rate-type materials. Scientists accomplished a momentous

consideration on discrepancy and rate-type classification of models. The Burgers' liquid model is reflected as the viscoelastic rate-type liquid model which is an extensively evolved model. Burgers' model has a propensity to rearrange pressure unwinding of a few polymeric liquids. Plentiful examinations on non-Newtonian tools can be established; for example, Dong et al. [1] developed an analysis between one-dimensional non-Fourier heat conduction and non-Newtonian flow in nanosystems. Mehryan et al. [2] examined melting heat transfer of power-law fluid in nano-enhanced *n*-octadecane-mesoporous silica (MPSiO₂). Hazeri-Mahmel et al. [3] examined a three-dimensional analysis of

forced convection of Newtonian and non-Newtonian nanofluids through a horizontal pipe using single- and two-phase models.

Ajeeb et al. [4] studied forced convection heat transfer of non-Newtonian MWCNT nanofluids in microchannels under laminar flow. Yadav and Kumar [5] applied an inclined magnetic field effect to study entropy production of nonmiscible Newtonian and micropolar fluid in a rectangular type geometry. Esfe et al. [6] provided a detailed analysis of the rheological behavior of MWCNT- Al_2O_3 (10:90)/5W50 hybrid non-Newtonian nanofluid with viscosity consideration. Saleem et al. [7] and Vishal et al. [8] also studied non-Newtonian fluids with different aspects and conditions. Ali et al. [9] examined G-jitter impact on MHD non-Newtonian fluid over an inclined surface using finite element discretization. Subhas Abel et al. [10] examined MHD flow and heat transfer for the upper-convected Maxwell fluid past a stretching sheet. Waqas et al. [11] examined an Oldroyd-B nanofluid with heat generation.

At first, Maxwell, in 1866, presented the viscoelastic liquid for clarifying the conduct of liquids such as air, instead of polymeric fluids. Burgers [12] introduced a one-dimensional rate kind of liquid model in 1939 that covers the one-dimensional Maxwell model [13] as an extraordinary case to clarify the viscoelastic conduct of liquid materials. Blacktop (asphalt, tarmacadam, or other black material used for surfacing roads) [14–17] gave a discussion about the utilization of Burgers' liquid model to portray the attributes of viscoelastic kind of liquids.

Shehzad et al. [18] concentrated on the convective warmth and mass limit conditions in the MHD stream of nanofluid. Zuo et al. [19] introduced the Taguchi trial plan and dark social investigation to assess the impacts of hydrogen/air proportionality proportion, channel speed, delta temperature, divider warm conductivity, divider emissivity, and convective heat transfer coefficient of the external divider on burning productivity of hydrogen/air premixed fire in a miniature tube-shaped combustor. Madhavi et al. [20] concentrated on Darcy stream in viscoelastic convection from a slanted plate as a reenactment of electroconductive polymer materials preparing with Biot number impacts. Shashikumar et al. [21] investigated the consistent progression of Williamson liquid in a miniature channel going with thick scattering, attractive field, and Joule dissemination. They detailed that liquid temperature declines when there are higher upsides of the Biot number. Rao et al. [22] talked about convective nanofluid stream with gyrotactic microorganisms over an isothermal cone with Biot number impacts. Gangadhar et al. [23] investigated Biot number consequences for a nodal or saddle stagnation point stream of a fluid regular magnesium oxide-gold half-breed nanofluid with the slip system. Ahmad et al. [24] concentrated on the convective limit condition on the unstable progression of 2nd-grade nanofluid.

In the present scenario, researchers and designers are worried to experience the issues with regard to streams of liquids joined with synthetic responses. Substance responses could be homogeneous-heterogeneous. In the event that a response emerges inside the whole space, this response is

named as homogeneous response, while the response reactants inside some particular district or inside the limit of the locale that could be heterogeneous response. Homogeneous-heterogeneous responses are likewise participating in various synthetically receptive frameworks. Here, note that a few responses develop on exceptionally low speed, and some of them do not advance by any means, without the presence of an impetus. An assortment of substance responses exist, and a large portion of them has critical utilizations in businesses and in compound architect frameworks. Especially, synthetic responses have generous effects in the creation of polymers, food regulation, pottery fabricating, hydrometallurgical industry, and artificial hardware plans and yield harm through freezing and forests of various trees. Numerous agents used heterogeneous-homogeneous responses in their examinations to research various sorts of stream marvels. At first, Chaudhary and Markin [25] introduced a straightforward model by utilizing heterogeneous-homogeneous responses in the progression of a gooey liquid almost at a stagnation point. Also, Merkin [26] mathematically investigated the limit layer stream by using heterogeneous-homogeneous responses. Khan et al. [27] introduced an altered warm conduction model by utilizing heterogeneous-homogeneous responses in the whirling stream of Maxwell liquid. They additionally examined that the nanoparticles' volume division appropriation debilitates for the homogeneous-heterogeneous responses' boundary. Mathematical recreation of Maxwell liquid stream because of the spiraling surface was done by Ahmed et al. [28]. They broke down that the focus rate lessens for bigger heterogeneous-homogeneous responses' boundary. The analysis for the flow of Williamson fluid with heterogeneous-homogeneous impacts bounded by the sheet and cylinder was examined by Hussain et al. [29]. Waqas [30] presented the heat transfer treatment for non-Newtonian ferromagnetic liquid subject to heterogeneous-homogeneous reactions. Rashid et al. [31] presented the mathematical analysis on the three-dimensional steady incompressible flow of Oldroyd-B fluid in the existence of heterogeneous-homogeneous impacts. Xu and Xu [32] inspected the heterogeneous-homogeneous response in the boundary layer flow of Buongiorno's model over a flat surface. Irfan et al. [33] implemented a theoretical study to investigate the response of homogeneous-heterogeneous in Oldroyd-B liquid with non-Fourier heat flux theory.

The indication of time-nondependent viscous fluid at rest over a hollow nonflatness cylinder was scrutinized by Wang [34]. The slippery flow due to the nonflatness cylinder was investigated by Wang and Ng [35]. Wang [34] introduced the behavior of the time-independent viscous fluid. By using the parameters of fluid and flow, the stretching cylinder was introduced, and this was studied by Crane [36]. Gangadhar et al. [37] scrutinized the flow of a couple of stress fluids over a stretched cylinder with nonuniform heat generation. Ahmed and Alhazmi [38] used FEM simulation to solve the rotation and radiation effects on cylinders within a lid-driven enclosure filled with glass balls. The problem of hydrodynamic and heat transfer of multidroplet impact on the cylindrical surfaces was analyzed by Luo et al. [39]. Kim

and Kim [40] discussed an experimental investigation of natural convection flow features from vertical cylinders with diverged pin fins. Triveni and Panua [41] studied the mixed and natural convection flow of heated isothermal cylinders in a lid-driven square enclosure filled with nanofluid. Li et al. [42] investigated the activation energy and nonlinear thermal radiation in the unsteady flow of bioconvection in Maxwell nanofluid through a stretched cylinder. The stagnation point flow of a hybrid nanofluid above a stretching cylinder with a magnetic field was examined by Abbas et al. [43]. Song et al. [44] performed the unsteady boundary layer flow of Williamson nanofluid over a stretched cylinder. Recent studies have been made in [45–56].

In the applications of petrochemical, biochemical, engineering, and geophysical advances, the non-Newtonian fluid is most widely utilized based on the Burgers' fluid [57–61]. Homogeneous-heterogeneous reactions are impacted by employing the mass transfer rate features in the flow of Burgers' fluid by stretching the cylinder. Heat source impacts are dependent on the space and temperature parameters which are incorporated by using the convective heat flux model. Similarly, a feature of thermal properties is studied in a detailed manner. By using the PDEs, the phenomenon of mathematical modeling is performed. Transformations of similarity are converted into the ODEs. By using the distributions of flow, temperature, and solutal parameters, the RKF-45 method is developed, and this will

explore the parameters based on the behavior of physical properties. In Section 2, the mathematical model is divided into two sections. RKF-45 method I is utilized in Section 3 by solving the nonlinear differential equations. In Section 4, results are discussed. In Section 5, the discussion of conclusion remarks is studied finally.

2. Mathematical Formulation

The following four sections present a two-dimensional formulation using the axis of the present flow.

2.1. Flow Profile. A cylinder of radius R is induced by stretching the model with two-dimensional flow. z_1 -axis is obtained when the coordinates of the cylinder are settled along the cylinder. The radial direction is considered in the r_1 -axis. $V = [u, 0, w]$ is considered as the present flow for the field of velocity. For the axis of r_1 and z_1 , components of velocity are taken as u and w . All this will be done by using the uniform magnetic field $B = [B_0, 0, 0]$. This is applied to the flow of direction when applied in the normal condition. Stretching velocity of the cylinder in the z_1 -axis is taken from $w_s = U_0 z_1 / l$. Reference velocity is represented as U_0 , and specific length is represented as l (Figure 1).

Khan et al. [17] showed and governed the present flow of equations for continuity and momentum:

$$\frac{\partial u}{\partial r_1} + \frac{u}{r_1} + \frac{\partial w}{\partial z_1} = 0, \tag{1}$$

$$\begin{aligned} & u \frac{\partial w}{\partial r_1} + w \frac{\partial w}{\partial z_1} + \lambda_1 \left[u^2 \frac{\partial^2 w}{\partial r_1^2} + w^2 \frac{\partial^2 w}{\partial z_1^2} + 2uw \frac{\partial^2 w}{\partial z_1 \partial r_1} \right] \\ & + \lambda_2 \left[u^3 \frac{\partial^3 w}{\partial r_1^3} + w^3 \frac{\partial^3 w}{\partial z_1^3} + 2u^2 \left(\frac{\partial u}{\partial r_1} \frac{\partial^2 w}{\partial r_1^2} + \frac{\partial w}{\partial r_1} \frac{\partial^2 w}{\partial r_1 \partial z_1} \right) - u^2 \left(\frac{\partial w}{\partial r_1} \frac{\partial^2 u}{\partial r_1^2} + \frac{\partial w}{\partial z_1} \frac{\partial^2 w}{\partial r_1^2} \right) \right. \\ & \left. + 2w^2 \frac{\partial u}{\partial z_1} \frac{\partial^2 w}{\partial r_1 \partial z_1} + w^2 \left(\frac{\partial w}{\partial z_1} \frac{\partial^2 w}{\partial z_1^2} - \frac{\partial w}{\partial r_1} \frac{\partial^2 u}{\partial z_1^2} \right) + 3uw \left(u \frac{\partial^3 w}{\partial r_1^2 \partial z_1} + w \frac{\partial^3 w}{\partial z_1^2 \partial r_1} \right) \right. \\ & \left. + 2uw \left(\left(\frac{\partial^2 w}{\partial z_1 \partial r_1} \right) \frac{\partial u}{\partial r_1} + \left(\frac{\partial u}{\partial z_1} \right) \frac{\partial^2 w}{\partial r_1^2} + \left(\frac{\partial w}{\partial r_1} \right) \frac{\partial^2 w}{\partial z_1^2} - \left(\frac{\partial^2 u}{\partial r_1 \partial z_1} \right) \frac{\partial w}{\partial r_1} \right) \right] \\ & = v \lambda_3 \left[u \frac{\partial^3 w}{\partial r_1^3} + w \frac{\partial^3 w}{\partial r_1^2 \partial z_1} + \frac{u}{r_1} \frac{\partial^2 w}{\partial r_1^2} - \frac{\partial w}{\partial r_1} \frac{\partial^2 u}{\partial r_1^2} \right] + w_e \frac{\partial w_e}{\partial r_1} + v \left[\frac{\partial^2 w}{\partial r_1^2} + \frac{1}{r_1} \frac{\partial w}{\partial r_1} \right] \\ & - \frac{\sigma B_0^2}{\rho} \left[(w - w_e) + \lambda_1 u \frac{\partial w}{\partial r_1} + \lambda_2 \left(w \frac{\partial u}{\partial z_1} \frac{\partial^2 w}{\partial r_1^2} - u \frac{\partial w}{\partial z_1} \frac{\partial^2 w}{\partial r_1^2} + uw \frac{\partial^2 w}{\partial r_1 \partial z_1} + u^2 \frac{\partial^2 w}{\partial r_1^2} \right) \right], \tag{2} \end{aligned}$$

subject to the boundary conditions

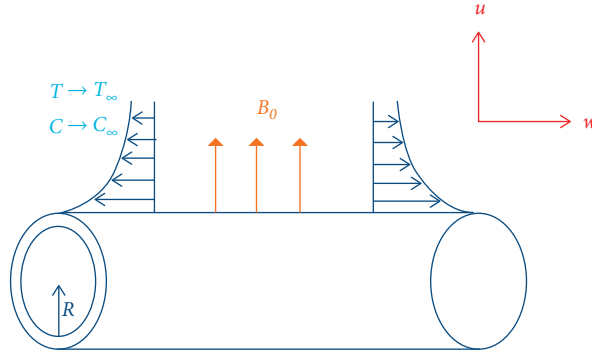


FIGURE 1: Physical sketch.

$$\begin{aligned} w(r_1, z_1) &= w_s = \frac{U_0 z_1}{l}, \\ u(r_1, z_1) &= 0 \text{ at } r_1 = R. \end{aligned} \quad (3)$$

$$w(r_1, z_1) \longrightarrow w_e = \frac{U_\infty z_1}{l}, \quad \frac{\partial w}{\partial r_1} \longrightarrow 0 \text{ as } r \longrightarrow \infty. \quad (4)$$

Here, λ_1 is the fluid relaxation time, λ_2 is the material factor of Burgers' fluid, λ_3 ($\leq \lambda_1$) is the fluid relaxation time, and ν is the kinematic viscosity of the fluid.

Transformations of similarity are shown in the following equation:

$$\begin{aligned} u &= -\frac{R}{r_1} \sqrt{\frac{U_0 \nu}{l}} f_1(\eta), \\ w &= \frac{U_0 z_1}{l} f_1'(\eta), \\ \eta &= \sqrt{\frac{U_0}{\nu l}} \left(\frac{r_1^2 - R^2}{2R} \right). \end{aligned} \quad (5)$$

(1) automatically satisfies when (5) is substituted into equations (1)–(4). The following form shows equations (2)–(4):

$$\begin{aligned} &(1 + 2\eta\alpha)^2 \beta_1 \left[2f_1'' f_1 f_1' - f_1'' f_1'^2 \right] - (1 + 2\eta\alpha) \beta_1 \alpha f_1'^2 f_1'' \\ &+ (1 + 2\eta\alpha)^3 f_1''' - 4\alpha^2 \beta_2 f_1'' f_1' - 4\alpha \beta_3 (1 + 2\eta\alpha)^2 f_1'' f_1' \\ &- (1 + 2\eta\alpha)^2 \beta_2 \left[3f_1''^2 f_1^2 + 2f_1'' f_1 f_1'^2 - f_1^3 f_1^{iv} \right] \\ &+ (1 + 2\eta\alpha) \alpha \beta_2 \left[3f_1'' f_1^2 f_1' + f_1^3 f_1'' \right] \\ &+ (1 + 2\eta\alpha)^2 \left[2\alpha f_1'' + f_1 f_1'' - f_1'^2 \right] \\ &+ (1 + 2\eta\alpha)^3 \beta_3 \left[f_1''^2 - f_1 f_1^{iv} \right] \\ &- (1 + 2\eta\alpha)^2 M^2 \left[\beta_2 f_1'' f_1 - \beta_1 f_1'' f_1 + f_1' - A \right] \\ &+ (1 + 2\eta\alpha)^2 A^2 = 0, \end{aligned} \quad (6)$$

$$f_1' = 1, f_1 = 0 \text{ at } \eta = 0 \text{ and } f_1' \longrightarrow A, f_1'' \longrightarrow 0 \text{ as } \eta \longrightarrow 0. \quad (7)$$

Here, $\alpha = 1/R\sqrt{\nu l/U_0}$ is the curvature factor, $\beta_1 = \lambda_1 U_0/l$ is the relaxation time parameter, $\beta_2 = \lambda_2 (U_0/l)^2$

is Burgers' fluid parameter, $\beta_3 = \lambda_3 U_0/l$ is the fluid relaxation time parameter, the magnetic force parameter is represented as $M = (\sigma B_0^2 / \rho_f U_0)^{1/2}$, and the velocity ratio parameter is represented as $A = w_e/w_s$.

2.2. *Thermal Features of Burgers' Fluid.* In the present case, the heat transport equation is given as shown in the following:

$$(\rho c_p) \left(u \frac{\partial T}{\partial r_1} + w \frac{\partial T}{\partial z_1} \right) = k \left(\frac{\partial^2 T}{\partial r_1^2} + \frac{1}{r_1} \frac{\partial T}{\partial r_1} \right) + q'''. \quad (8)$$

The following shows the boundary conditions which are related with each other:

$$-k \frac{\partial T}{\partial r_1} = h_f (T_f - T) \text{ at } r_1 = R \text{ and } T \longrightarrow T_\infty \text{ as } r_1 \longrightarrow \infty, \quad (9)$$

where k is the thermal conductivity, ρ is the density, T is the temperature, T_f is the convective surface temperature with heat transfer coefficient h_f , and c_p is the specific heat at constant pressure.

q''' is the space- and temperature-related internal heat generation/absorption which can be conveyed in the simplest form as (Song et al. [44])

$$q''' = \frac{k w_s}{z_1 \nu} \left[A^* (T_f - T_\infty) f_1' + B^* (T - T_\infty) \right]. \quad (10)$$

Here, space and temperature parameters depend on the internal heat generation/absorption, and these are represented as A^* and B^* . $A^* > 0$ and $B^* > 0$ show that values are corresponded to the internal heat generation, and $A^* < 0$ and $B^* < 0$ show that values are corresponded to the internal heat absorption.

The following shows Burgers' fluid which is based on the dimensionless temperature:

$$\theta(\eta) = \frac{T - T_\infty}{T_f - T_\infty}. \quad (11)$$

By making use of equations (10) and (11) into equations (8) and (9), we get

$$(1 + 2\alpha\eta)\theta'' + 2\alpha\theta' + \text{Pr}f_1\theta' + A^*f_1' + B^*\theta = 0, \quad (12)$$

$$\theta' = -\text{Bi}(1 - \theta) \text{ at } \eta = 0 \text{ } \theta \longrightarrow 0 \text{ as } \eta \longrightarrow \infty. \quad (13)$$

Here, the Prandtl number is represented as $\text{Pr} = \mu c_p/k$, and the Biot number is represented as $\text{Bi}h_f/k$.

2.3. Relation for Chemical Species. Hence, chemical reactants have (a_1, a_2) as concentrations with (k_c, k_s) as rate constants by assuming the (G, H) values. Cubic autocatalysis is assumed by maintaining the response of homogeneous, and it is shown from the following equation:

$$A + 2B \longrightarrow 3B, \text{ rate} = k_c a_1 a_2^2. \quad (14)$$

The following shows the representation of isothermal response which is at the first order by maintaining the surface of the catalyst as heterogeneous:

$$A \longrightarrow B, \text{ rate} = k_s a_1. \quad (15)$$

Isothermal reactants are utilized, and it is assumed that the ambient fluid is taken far away from the surface; uniform concentration of reactant A is represented using a_0 when the autocatalyst is not existed. Hence, the species will govern the equations based on the limitations which are given in the following:

$$u \frac{\partial a_1}{\partial r_1} + w \frac{\partial a_2}{\partial z_1} = D_G \left(\frac{1}{r_1} \frac{\partial a_1}{\partial r_1} + \frac{\partial^2 a_1}{\partial r_1^2} \right) - k_c a_1 a_2^2, \quad (16)$$

$$u \frac{\partial a_2}{\partial r_1} + w \frac{\partial a_2}{\partial z_1} = D_H \left(\frac{1}{r_1} \frac{\partial a_2}{\partial r_1} + \frac{\partial^2 a_2}{\partial r_1^2} \right) + k_c a_1 a_2^2, \quad (17)$$

with associated boundary conditions as

$$D_G \frac{1}{r_1} \frac{\partial a_1}{\partial r_1} = k_s a_1, \quad (18)$$

$$D_H \frac{1}{r_1} \frac{\partial a_2}{\partial r_1} = -k_s a_1, \text{ at } r_1 = R.$$

$$a_1 \longrightarrow a_0, a_2 \longrightarrow 0 \text{ as } r_1 \longrightarrow \infty. \quad (19)$$

Here, the coefficient of diffusion for the species G is represented using D_G , whereas diffusion coefficient for species H is represented using D_H .

The following shows the transformations which are in use:

$$\begin{aligned} a_1 &= a_0 \phi(\eta), \\ a_2 &= b_0 \psi(\eta). \end{aligned} \quad (20)$$

Equations (14)–(18) show the transformations:

$$B((1 + 2\alpha\eta)\phi'' + 2\alpha\phi') \frac{1}{\text{Sc}} + f_1\phi' - k_1\phi\psi^2 = 0,$$

$$((1 + 2\alpha\eta)\psi'' + 2\alpha\psi') \frac{\lambda^*}{\text{Sc}} + f_1\psi' + k_1\phi\psi^2 = 0,$$

$$\phi'(0) = k_2\phi(0),$$

$$\lambda^* \psi'(0) = -k_2\phi(0),$$

$$\phi \longrightarrow 1, \psi \longrightarrow 0, \text{ as } \eta \longrightarrow \infty.$$

Here, diffusion coefficient is represented as $\lambda^* = D_H/D_G$, homogeneous reaction constant is represented as k_1 , heterogeneous reaction constant is represented as k_2 , and Schmidt number is represented as $\text{Sc} = \nu/D_a$.

When $D_H = D_G$, coefficients of diffusion quality are assumed based on the quality. $\lambda^* = 1$ shows the implication of this quality. $\phi(\eta) + \psi(\eta) = 1$ shows the coefficients of diffusion quality.

Hence, the following shows the proof:

$$((1 + 2\alpha\eta)\phi'' + 2\alpha\phi') \frac{1}{\text{Sc}} + f_1\phi' - k_1\phi(1 - \phi)^2 = 0. \quad (22)$$

$$\phi'(0) = k_2\phi(0) \text{ and } \phi \longrightarrow 1 \text{ as } \eta \longrightarrow \infty. \quad (23)$$

2.4. Heat Transfer Performance. Local Nusselt number Nu_z is estimated by the performance of convective heat transfer over the cylindrical surface. The Nusselt number is utilized using Nu_z . The following shows the quality of mathematical expression:

$$\text{Nu}_z = \frac{z_1 q_w}{k(T_f - T_\infty)}, \quad (24)$$

with $q_w = -k(\partial T/\partial r_1)_{r_1=R}$.

The following equation shows the nondimensional form:

$$\text{Re}^{1/2} \text{Nu}_z = -\theta'(0), \quad (25)$$

where $\text{Re} = z_1 w_s/\nu$ is the local Reynolds number.

3. Method of the Solution

The nonlinear equations (6), (12), and (23) under conditions (7), (13), and (23) are solved via the shooting technique along with the Runge–Kutta–Fehlberg fourth and fifth order method. Computation is performed with the aid of MATLAB. Equations (6), (12), and (23) are written as

$$f_1^{iv} = \frac{1}{\begin{bmatrix} (1+2\alpha\eta)^3 f_1 \beta_3 \\ -(1+2\alpha\eta)^2 \beta_2 f_1^3 \end{bmatrix}} \begin{bmatrix} (1+2\alpha\eta)^2 \beta_1 [2f_1 f_1' f_1'' - f_1^2 f_1'''] \\ -(1+2\alpha\eta) \alpha \beta_1 f_1^2 f_1'' + (1+2\alpha\eta)^3 f_1''' \\ -4\alpha^2 \beta_2 f_1 f_1'' - 4\alpha \beta_3 (1+2\alpha\eta)^2 f_1 f_1'' \\ -(1+2\alpha\eta)^2 \beta_2 [3f_1^2 f_1''^2 + 2f_1 f_1'^2 f_1'''] \\ +(1+2\alpha\eta) \alpha \beta_2 [3f_1^2 f_1' f_1'' + f_1^3 f_1'''] \\ +(1+2\alpha\eta)^2 [2\alpha f_1'' + f_1 f_1' - f_1'^2] \\ +(1+2\alpha\eta)^3 \beta_3 [f_1''^2] \\ -(1+2\alpha\eta)^2 M^2 \begin{bmatrix} \beta_2 f_1 f_1'' - \beta_1 f_1 f_1''' \\ + f_1' - A \end{bmatrix} \\ +(1+2\alpha\eta)^2 A^2 = 0, \end{bmatrix}, \quad (26)$$

$$\theta'' = -\frac{1}{(1+2\alpha\eta)} [2\alpha\theta' + \text{Pr} f_1 \theta' + A^* f_1' + B^* \theta],$$

$$\phi'' = -\frac{1}{(1+2\alpha\eta)} [2\alpha\phi' + \text{Sc} f_1 \phi' - \text{Sc} k_1 \phi (1-\phi)^2].$$

The first-order corresponding scheme in terms of variables

$(\Psi_1, \Psi_2, \Psi_3, \Psi_4, \Psi_5, \Psi_6, \Psi_7, \Psi_8) = (f_1, f_1', f_1'', f_1''', \theta, \theta', \phi, \phi')$ is

$$\begin{aligned} \Psi_1' &= \Psi_2, \\ \Psi_2' &= \Psi_3, \\ \Psi_3' &= \Psi_4, \end{aligned}$$

$$\Psi_4' = \frac{1}{\begin{bmatrix} (1+2\alpha\eta)^3 \Psi_1 \beta_3 \\ -(1+2\alpha\eta)^2 \beta_2 \Psi_1^3 \end{bmatrix}} \begin{bmatrix} (1+2\alpha\eta)^2 \beta_1 [2\Psi_1 \Psi_2 \Psi_3 - \Psi_1^2 \Psi_4] \\ -(1+2\alpha\eta) \alpha \beta_1 \Psi_1^2 \Psi_3 + (1+2\alpha\eta)^3 \Psi_4 \\ -4\alpha^2 \beta_2 \Psi_4 \Psi_3 - 4\alpha \beta_3 (1+2\alpha\eta)^2 \Psi_1 \Psi_4 \\ -(1+2\alpha\eta)^2 \beta_2 [3\Psi_1^2 \Psi_3^2 + 2\Psi_1 \Psi_2^2 \Psi_3] \\ +(1+2\alpha\eta) \alpha \beta_2 [3\Psi_1^2 \Psi_2 \Psi_3 + \Psi_1^3 \Psi_4] \\ +(1+2\alpha\eta)^2 [2\alpha \Psi_3 + \Psi_1 \Psi_3 - \Psi_2^2] \\ +(1+2\alpha\eta)^3 \beta_3 [\Psi_3^2] \\ -(1+2\alpha\eta)^2 M^2 \begin{bmatrix} \beta_2 \Psi_1 \Psi_4 - \beta_1 \Psi_1 \Psi_3 \\ + \Psi_2 - A \end{bmatrix} \\ +(1+2\alpha\eta)^2 A^2 = 0, \end{bmatrix}, \quad (27)$$

$$\begin{aligned} \Psi_5' &= \Psi_6, \\ \Psi_6' &= -\frac{1}{(1+2\alpha\eta)} [2\alpha\Psi_6 + \text{Pr}\Psi_1\Psi_6 + A^*\Psi_2 + B^*\Psi_5], \\ \Psi_7' &= \Psi_8, \\ \Psi_8' &= -\frac{1}{(1+2\alpha\eta)} [2\alpha\Psi_8 + \text{Sc}\Psi_1\Psi_8 - \text{Sc}k_1\Psi_7(1-\Psi_7)^2], \end{aligned}$$

with

$$\begin{aligned}
 \Psi_1(0) &= 0, \\
 \Psi_2(0) &= 1, \\
 \Psi_3(0) &= s_1, \\
 \Psi_6(0) + \text{Bi}(1 - \Psi_5(0)) &= 0, \\
 \Psi_6(\infty) &= s_2, \\
 \Psi_7(0) &= 1, \\
 \Psi_8(0) &= s_3, \\
 \Psi_2(\infty) &= A, \\
 \Psi_3(\infty) &= 0, \\
 \Psi_5(\infty) &= 0, \\
 \Psi_7(\infty) &= 0.
 \end{aligned} \tag{28}$$

RKF-45 method will solve the unknown initial conditions (s_1, s_2, s_3) based on the IVP which is an appropriate choice. Benchmarks $(\max\{\Psi_1, \Psi_2, \Psi_5, \Psi_7\} < \varepsilon)$ are improved by assuring Newton's method. Any positive number is signified based on $(\varepsilon > 0)$. $\varepsilon = 10^{-6}$ will be obtained from the analysis of numerical results.

3.1. Validation of Results. Irfan et al. [33], Waqas et al. [11], and Subhas Abel et al. [10] validated the results by comparing the parameters after execution. Extra parameters are nullified by comparing the present results of skin friction coefficient against the pertinent parameter β , and this is shown in Table 1 with [10, 11, 33]. From Table 2, it can be observed that Shehzad et al. [18], Hayat et al. [16], and Khan et al. [17] compared the skin friction coefficient against the significant parameter M . Present results are validated by observing the comparisons of appropriate resemblance.

4. Results and Discussion

By using the mathematical formulation section, the ODEs are characterized and planned based on the physical constraints. The investigation of physical behavior is done for various parameters in the RKF-45 method. From equations (6), (13), and (23), the ODEs are depicted and mentioned in equations (7), (14), and (25). From Figures 2–8, the distributions of solutal, temperature, and flow are impacted and depicted. For numerical simulation, the leading parameters are allocated for fixed values; they are $\alpha = 0.1, \beta_1 = 0.7, \beta_2 = 0.25, \beta_3 = 0.5, M = 2, \text{Pr} = 6.2, k_1 = 0.4, A = 0.2, k_2 = 0.5, \text{Bi} = 0.5, A^* = 0.01, B^* = 0.1, \text{and Sc} = 6.0$, and from graphs, few are mentioned. Behaviors of involved parameters are introduced by physical interpretation and deliberation. Figure 2 shows the hydromagnetic flow situation and hydrodynamic flow patterns. Stagnation $z_1 = 0$ of the hydrodynamic flow situation in hydromagnetic flow streamlines is closed.

From Figures 3(a)–3(c), the distributions of velocity, temperature, and solutal are provided against the magnetic force parameter (M) and curvature parameter (α) which are an impact of combined characteristics. Large curvature parameter will become high when the flow of concentration curves of the fluid enhances and accesses the curves. In limiting sense, the radius of cylinder shrinks with curvature. The fluid will be build up when the resistance is produced with exterior diminution. The values of the curvature parameter are intensified using the thermal curves of Burgers' fluid in the upsurge. From these figures, it can be observed that the thermal boundary conditions are analyzed and satisfied due to the flow of patterns. The magnetic force parameter (M) is affected by using Burgers' fluid, and this will escalate the data using parameters.

A drag force is generated based on the effect of the magnetic force parameter. This force consists of intensifying nature which will oppose the motion of liquid flow, and the liquid deteriorates of velocity. A higher extent of the magnetic parameter is declined using the thermal energy transport perception which is a basic flow. Stronger Lorentz force is utilized based on the large magnetic parameter. Thermal profile of Burgers' fluid is developed by using the force parameters ultimately. Hence, larger values are assigned to the magnetic force parameter which is declined by the concentration rate. Hydromagnetic flow situation is corresponded to $M \neq 0$ when it is classified by the hydrodynamic flow pattern. 0.0 to 1.5 is the range that is analyzed by M .

From Figures 4(a)–4(c), the material parameter for Burgers' fluid (β_2) against flow, temperature, concentration curves, and fluid relaxation time (β_1) impact are shown in a detailed manner. Momentum boundary layer of Burgers' fluid is diminished based on the thickness. Large values of β_1 are scrutinized which will lead to the profile. Fluid relaxation time parameter is utilized by Burgers' fluid buildup technique which will escalate the data in a very effective way. Based on the relaxation time λ_1 , the value of β_1 is dependent. Various effects are opposed by escalating the Deborah number β_1 and fluid motion which is augmented based on the fluid relaxation time. In this, victim diminution will depend on Burgers' fluid flow curves which are mainly improving the strength. Deborah number (β_1) is escalated by intensifying the fluid elements' improvement, and this will mainly increase the interface flows. Burgers' fluid will improve the flow by raising the thermal energy transport. Deborah number β_1 large values are obtained by associating the thickness of the boundary layer and concentration curves. 0.5 to 3.5 range is obtained for the β_1 values after analyzing. Magnitude of β_2 is enlarged by enlarging the thickness of the velocity boundary layer, and this is shown from Figures 4(a)–4(c) which will attenuate the flow of curves. Scales are varied based on Burgers' fluid parameter by augmenting the thermal profile. Higher magnitude of β_2 is obtained by decreasing

TABLE 1: For various values of β_1 , $\alpha = \beta_2 = \beta_3 = M = 0$ against $-f''(0)$ comparison table.

| β_1 | Subhas Abel et al. [10] | Irfan et al. [33] | Waqas et al. [11] | Present results |
|-----------|-------------------------|-------------------|-------------------|-----------------|
| 0.0 | 1.000000 | 1.000000 | 1.000000 | 1.0000000 |
| 0.2 | 1.051948 | 1.051889 | 1.051889 | 1.0518898 |
| 0.4 | 1.101850 | 1.101903 | 1.101903 | 1.10190328 |
| 0.6 | 1.150163 | 1.1501374 | 1.150137 | 1.15013735 |
| 0.8 | 1.196692 | 1.1967114 | 1.196711 | 1.19671127 |
| 1.0 | — | 1.2417477 | — | 1.24174749 |
| 1.2 | 1.285257 | 1.2853630 | 1.285363 | 1.28536328 |
| 1.4 | — | 1.3276675 | — | 1.32766723 |
| 1.6 | 1.368641 | 1.3687582 | 1.368758 | 1.36875824 |
| 1.8 | — | 1.4087264 | — | 1.40872641 |
| 2.0 | 1.447617 | 1.4476526 | 1.447651 | 1.44765068 |

TABLE 2: Comparative study of the present results for $-f''(0)$ against $\alpha = \beta_1 = \beta_2 = \beta_3 = 0$.

| M | Shehzad et al. [18] | Hayat et al. [16] | Khan et al. [17] | Present results |
|-----|---------------------|-------------------|------------------|-----------------|
| 0.0 | 1.00000 | 1.00000 | 1.000000 | 1.0000000 |
| 0.2 | 1.01980 | 1.01980 | 1.019801 | 1.01980390 |
| 0.5 | 1.11803 | 1.11803 | 1.118029 | 1.11803399 |
| 0.8 | 1.28063 | 1.28063 | 1.280633 | 1.28062485 |
| 1.0 | 1.41421 | 1.41421 | 1.414221 | 1.41421356 |
| 1.2 | 1.56205 | 1.56205 | 1.562048 | 1.56204994 |
| 1.5 | 1.80303 | 1.80303 | 1.803044 | 1.80277564 |

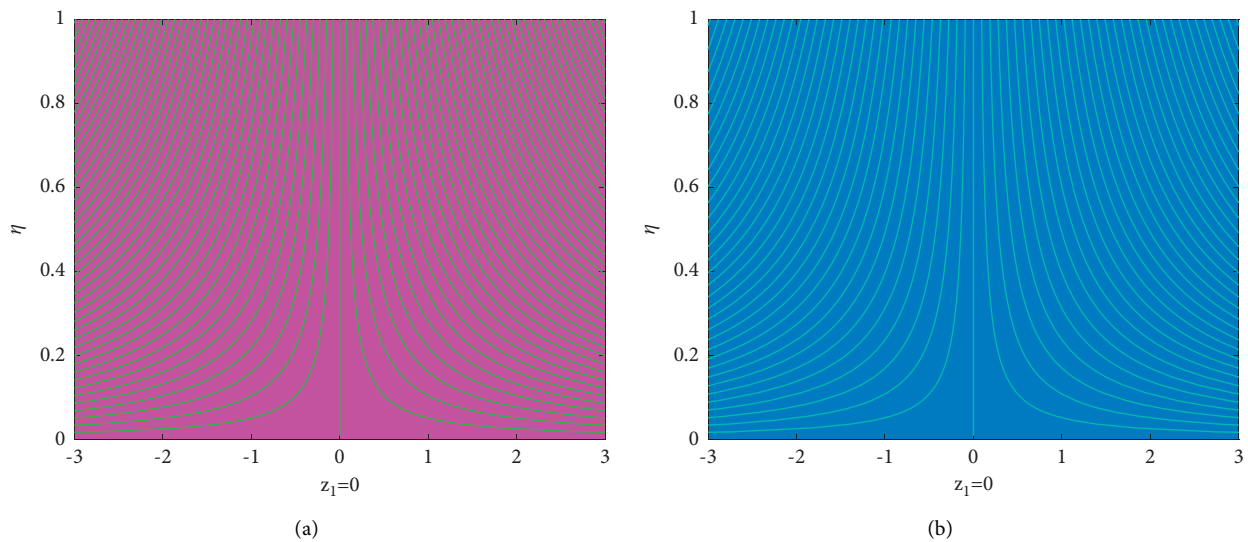


FIGURE 2: (a) $M = 0$ streamlines. (b) $M = 2$ streamlines.

the thickness of boundary layers which depend on the concentration curves. 2.5 to 5.5 range is taken for the value of β_2 by scrutinizing.

From Figures 5(a)–5(c), the solutal, temperature, and retardation time parameter (β_3) against flow distributions are characterized. By concentrating the profiles of

Burgers’ fluid rise, the flow is detected. Deborah number β_3 will diminish the values of thermal energy transport. Retardation time λ_3 is enlarged physically. Non-Newtonian viscoelastic fluid model will use the two situations to reduce the viscous fluid model by detecting it. They are given as (1) $\lambda_1 = \lambda_2 = \lambda_3$, (2) $\lambda_2 = 0$, and (3) $\lambda_1 = \lambda_3$. Fluid

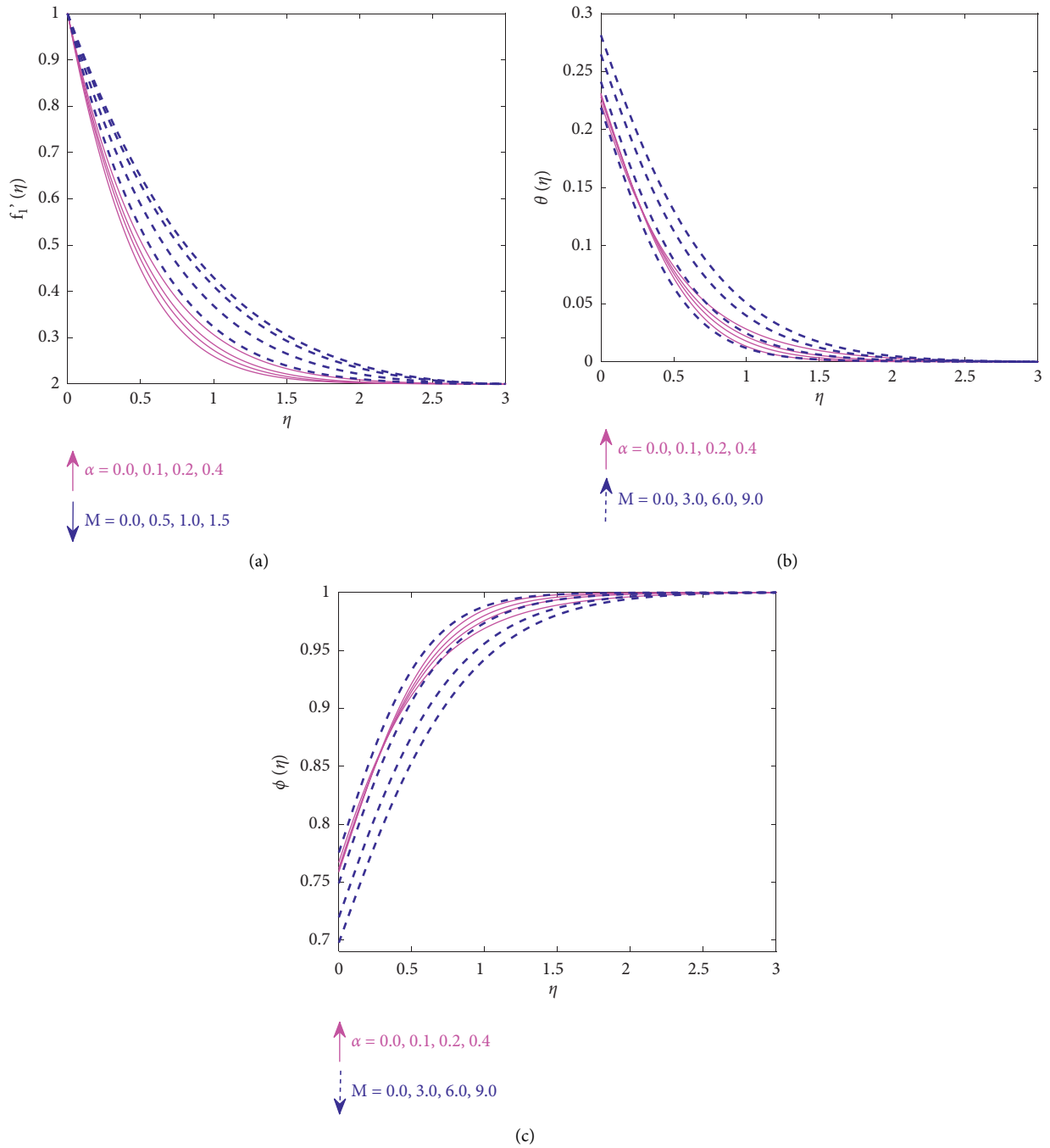


FIGURE 3: (a) Variation of $f_1'(\eta)$ versus α and M . (b) Variation of $\theta(\eta)$ versus α and M . (c) Variation of $\phi(\eta)$ versus α and M .

retardation time will become equal when the parameters of Burgers' fluid are utilized, and this is the first case in fluid relaxation time.

Vanished Burgers' fluid parameter is elaborated by maintaining the retardation time. Maxwell viscoelastic fluid model will describe this position based on the $\lambda_2 = \lambda_3 = 0$

description. Relaxation time β_1 will control the distribution by maintaining the value of fluid relaxation time β_3 .

By using the hydrodynamic and hydromagnetic flow situations, Burgers' liquid flow distributions will utilize the velocity ratio parameter (A), and this is shown from Figure 6(a). The phenomenon of flow is detected from this

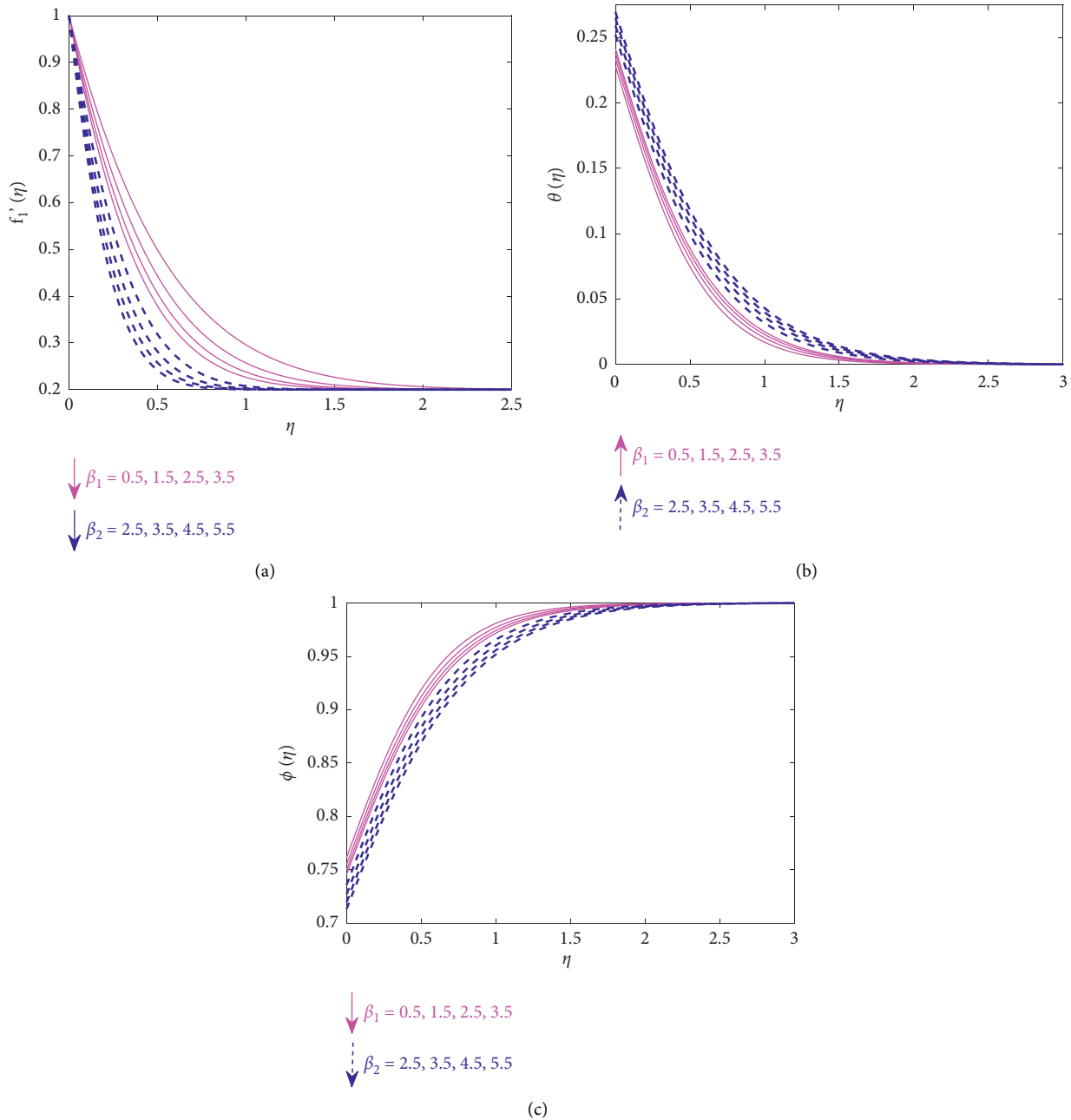


FIGURE 4: (a) Variation of $f_1'(\eta)$ versus β_1 and β_2 . (b) Variation of $\theta(\eta)$ versus β_1 and β_2 . (c) Variation of $\phi(\eta)$ versus β_1 and β_2 .

plot. In Burgers' liquid, boundary layer thickness will improve the magnitude velocity of ratio constant ($A < 1$).

Figure 6(b) is to feature the actual impact of the temperature profile inside the heat source (A^* and B^*) against temperature of Burgers' liquid. From this diagram, it is related that the temperature of the liquid is essentially influenced by the boundaries (A^* and B^*). An unmistakable upsurge is distinguished in the temperature profile of Burgers' liquid because of acceleration in the improvement of the heat source (A^* and B^*). By taking assumptions in the framework expansion will improve the heating rise eventually. This heat rising condition of the fluid is highlighted by bringing the assumptions of heightening. These outcomes are like those of Song et al. [44].

From Figure 6(c), it is shown that Prandtl number (Pr) and Biot number (Bi) are against the Burgers' fluid temperature features. Prandtl number is varied by extending magneto-Burgers' liquid which is inspected from the thermal counters. Based on the thermal diffusivity function, the Prandtl number Pr is utilized. Temperature distribution coefficient is analyzed by accessing the Prandtl number in a higher form. Thermal profiles decline for higher Pr and thickness of temperature from the boundary using Burgers' liquid. 3.0 to 6.0 is the range of the Prandtl number for realization.

From Figure 7, it shows that the heterogeneous and homogeneous response parameters (k_1 and k_2) are impacted

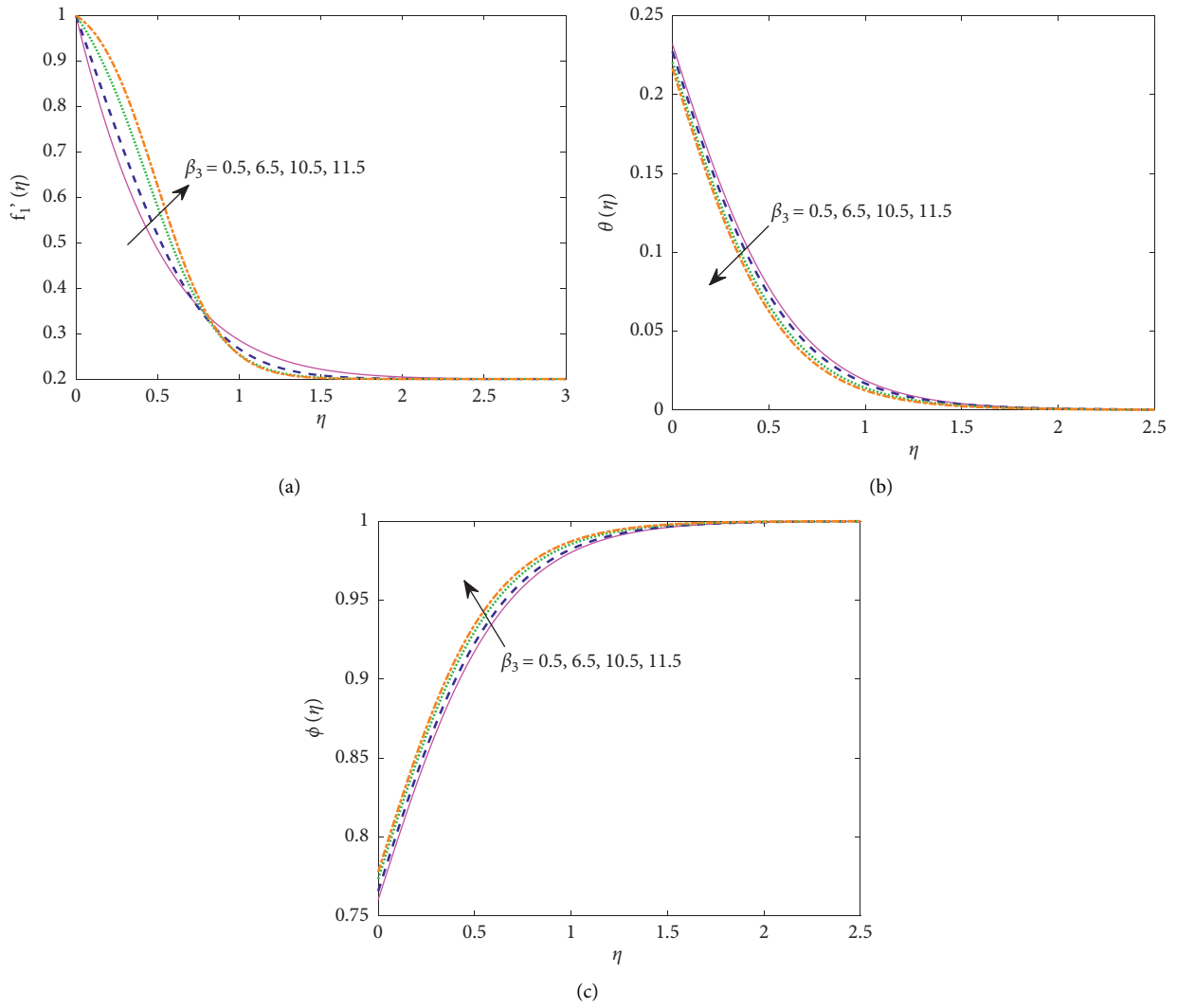


FIGURE 5: (a) Variation of $f_1'(\eta)$ versus β_3 . (b) Variation of $\theta(\eta)$ versus β_3 . (c) Variation of $\phi(\eta)$ versus β_3 .

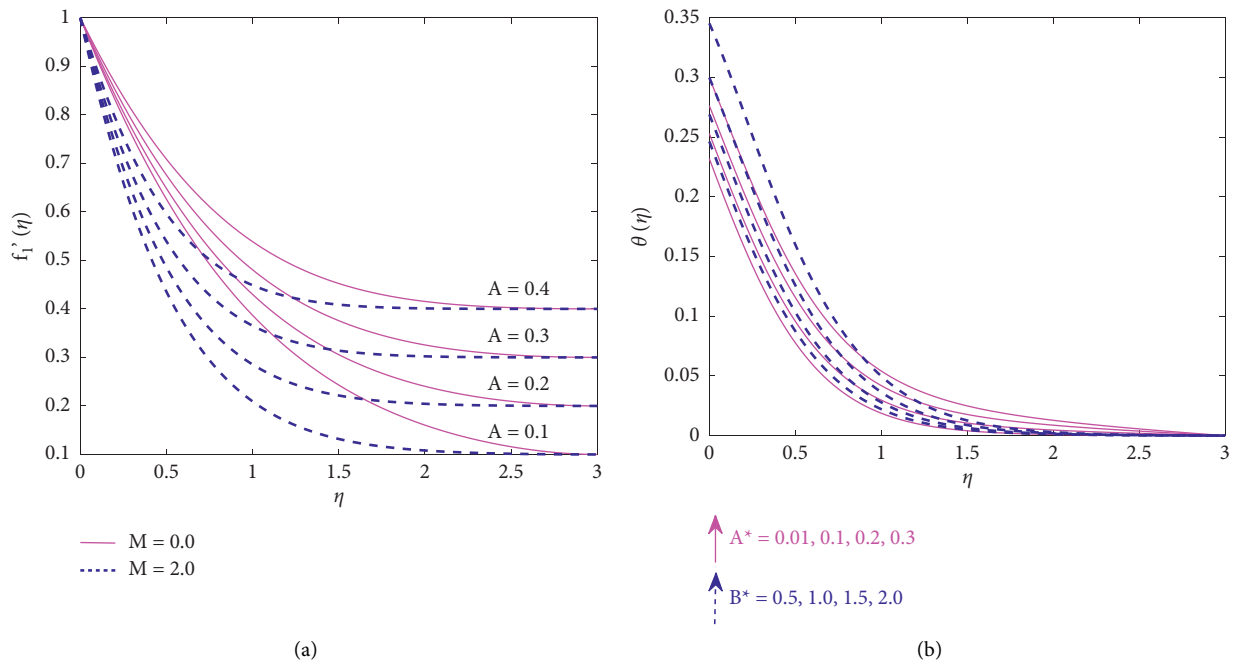


FIGURE 6: Continued.

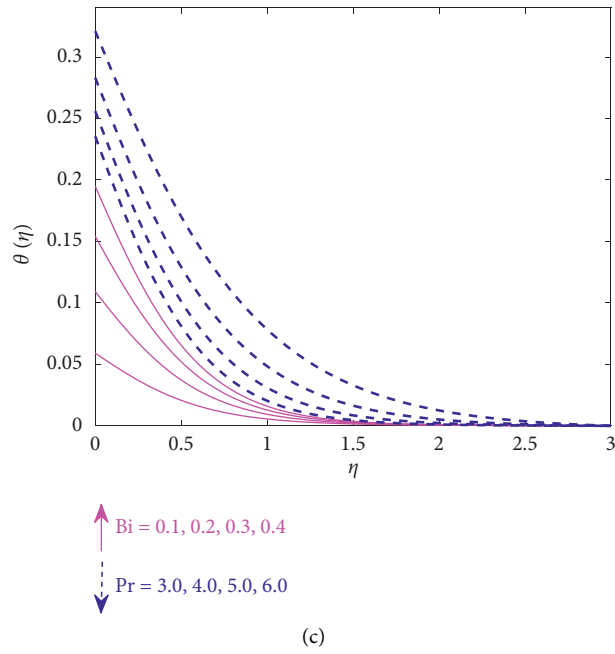
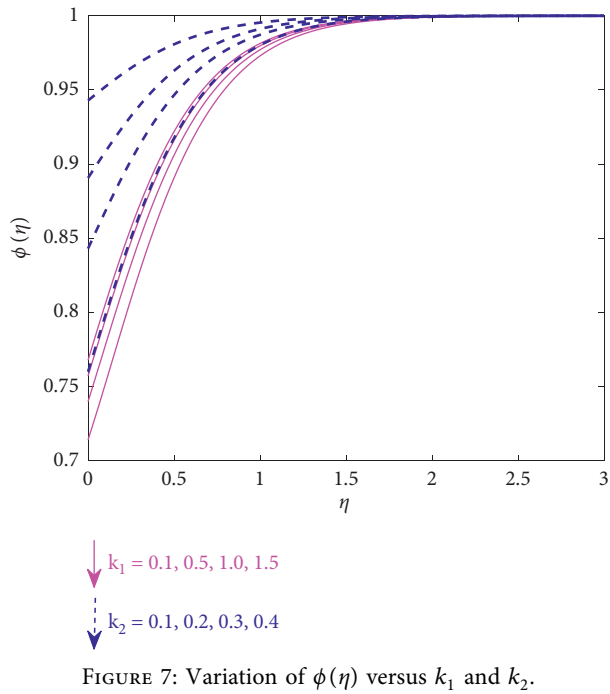


FIGURE 6: (a) Variation of $f_1'(\eta)$ versus A and M . (b) Variation of $\theta(\eta)$ versus A^* and B^* . (c) Variation of $\phi(\eta)$ versus Bi and Pr .



by envying the solutal distribution. Stronger strength of homogeneous response (k_1) and strength of heterogeneous reaction constant are depicted. During the homogeneous process, the reactants will be utilized, and concentration

deteriorates the viscosity. Strength of homogeneous reactions will be increased by the solutal profile. Khan et al. [27] and Ahmed et al. [28] described the profile of obtained results.

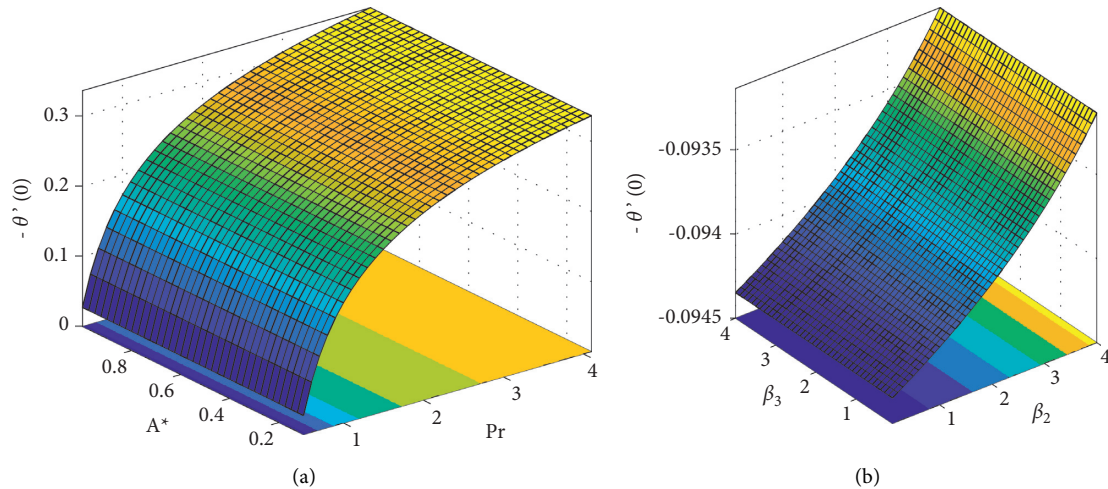


FIGURE 8: (a) Variation of $-\theta'(0)$ versus A^* and Pr . (b) Variation of $-\theta'(0)$ versus β_2 and β_3 .

The stimulus of space-related heat source parameter (A^*) and the Prandtl number (Pr) against the heat transfer rate of Burgers' liquid is delineated in Figure 8(a). Prandtl number is used for heat transfer rate, and this is dependent on Burgers' fluid. β_2 on heat transfer rate versus β_3 is influenced from Figure 8(b). Heat transfer rate is enhanced by reducing the parameter of Burgers' fluid which consists of higher estimation and a rise in values of β_3 .

5. Concluding Remarks

A theoretical analysis for incompressible two-dimensional magnetized Burgers' fluid in accordance with the space- and temperature-dependent heat generation phenomenon induced by a convectively heated stretching cylinder is performed. RKF-45 method is employed by the ODEs disclosed by the physical outcomes. In these investigations, the main findings are given in the following:

- (1) Magnetic force parameter, time relaxation parameter, and parameter of material for Burgers' fluid will be intensified by identifying the motion of Burgers' fluid. Here, the curvature parameter and velocity ratio parameter scale are detected by the escalation.
- (2) To improve the retardation time constant and Prandtl number the of Burgers magneto fluid is studied based on the thermal thickness of the layers and diminution behavior of thermal contours.
- (3) Biot number, space, and temperature will be enhanced by Burgers' liquid of temperature distribution. This will depend on the time constant of relaxation, fluid parameter of Burgers, and source parameter of heat dependence.
- (4) Curvature parameter and retardation time constant are varied by boosting Burgers' fluid in the boundary layer. This is the combination of solutal thickness and concentration rate of the boundary layer.

- (5) Higher Prandtl numbers are predicted with stronger magnitude based on the solutal profile.
- (6) Biot number will reduce the higher values of Burgers' liquid by depicting the heat transfer rate. Similarly, higher Prandtl numbers are obtained to increase the trend.

The current study clearly demonstrated the potential significance of rheological models. Nanofluid model study is ignored in the present generation. By using porous materials, this work can be extended in future [62].

Data Availability

No data were used to support this study.

Conflicts of Interest

The authors declare that they have no conflicts of interest.

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