

## Research Article

# Time Period Analysis of Orthotropic Skew Plate with 2-D Circular Thickness and 1-D Circular Density

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In the present study, the time period of vibration of an orthotropic parallelogram plate with 2-D (two-dimensional) circular thickness under the effect of 2-D parabolic temperature is investigated for the first time. The different edge conditions are *CCCC*, *CCCF*, *CFCF*, *CSCF*, and *SFSF* boundary conditions, where C, S, and F stands for clamped, simply supported, and free edges of the plate, respectively. The variation in density of plate material is considered to be 1-D (one-dimensional) circular. The Rayleigh–Ritz technique is used to solve the differential equation and evaluate the time period for the first two modes of vibration. A convergence study of an orthotropic parallelogram, rectangle plate, and square plate for modes of frequency at various edge conditions is also carried out. The authors performed a comparative analysis of the time period and modes of frequency of orthotropic parallelogram, rectangle plate, and isotropic square plate with the available published results at various edge conditions. The main conclusion which we made from this study is that by choosing the above-mentioned plate parameters, we obtained fewer modes of frequency in comparison to other variations mentioned in the literature. Also, the study suggests that the variation in modes of frequency is less in comparison to other variations.

## 1. Introduction

In engineering, machines and structures vibrate, so we cannot proceed without considering vibration. Modern technology requires knowing the vibration characteristics of plates with different plate parameters. Tapered plates with uniform and nonuniform thickness under a temperature environment are generally utilized in the aeronautical field, construction industry, and submarine structures. Different analysts/researchers investigated the vibration characteristics of various plates (homogeneous or nonhomogeneous) having variable thickness with or without consideration of temperature effect. A significant work about the vibrational characteristics of plates has been reported in the literature.

The quasi-green function method (QGFM) [1] is applied to solve the free vibration of clamped orthotropic thin plates (parallelogram shape) on the Winkler foundation. In this study, a quasi-green function is established by using the fundamental solution and a principal differential equation

has been solved with the help of the variable separable method. Vibration of the viscoelastic orthotropic parallelogram plate with parabolic [2] and linear thickness [3] at clamped boundary conditions was studied by using the Rayleigh–Ritz technique to determine the frequency equation. The frequency equation is derived by using the Rayleigh–Ritz technique, and two-term deflection function is used to find the modes of frequency for various values of taper constants, aspect ratios, and skew angle. Rayleigh–Ritz technique is employed to study the natural vibration of the nonhomogeneous tapered parallelogram plate with two-dimensional varying thickness [4] and one-dimensional circular variation in density parameter [5] at clamped boundary conditions under temperature field. The time period of natural transverse vibration of a nonhomogeneous skew (parallelogram) plate [6] with variable thickness and temperature field has been investigated on clamped and combination of clamped and simply supported edge conditions. The effect of sinusoidal varying thickness [7] on the

vibrations of nonhomogeneous parallelogram plates is computed at clamped edges. Here, the frequency equation is solved by using the Rayleigh–Ritz method and we analyze the vibrational behavior of frequencies of a parallelogram plate for both modes. The effect of two-dimensional circular variations in thickness [8] on a nonhomogeneous parallelogram plate under thermal effect was computed, and differential equations of motions are solved by using the Rayleigh–Ritz technique and we evaluate the vibrational frequencies at various plate parameters. A fast-converging semi-analytical method [9] was developed for assessing the vibration effect on thin orthotropic skew plates. An experimental and finite element [10] was proposed to study the free vibration of isotropic and laminated composite skew plates. A method to unify the solutions for plates with different shapes [11] (circular plate, annular plate, circular sector plate, and annular sector plate) subjected to general boundary conditions was adapted to study vibration characteristics. The time period of a rectangular plate [12] with variable thickness and temperature effect was analyzed. Two-dimensional circular thickness effects on time period of the nonhomogeneous skew plate [13] for variable temperature environments are computed at various combinations of clamped, simply supported, and free edge conditions. Free vibration of an orthotropic parallelogram plate [14] with a simply supported boundary condition under the effect of biparabolic thickness variation and linear temperature distribution in both directions is carried out at simply supported edges. The effect of parabolically thick variation on vibration of a viscoelastic orthotropic parallelogram plate [15] having clamped boundary conditions on all four edges was studied by using the separation of variables method. Vibration and modes of nanocomposite plates, functionally graded sandwich plates, sector plates, sandwich panels, l-shaped graphene sheet, skew plate, cylindrical skew plates, functionally graded rectangle plates, spherical shell, and annular sector plates [16–37] have been analyzed.

In the literature till date, researchers have studied the 1–D (one-dimensional) circular tapering impact on vibrational modes of frequency for different isotropic plate structures. But in the case of orthotropic material, none of the researchers have tackled 1–D (one-dimensional) circular tapering as well as 2–D (two-dimensional) circular tapering impact on the mode of frequency. In this work, we aim to fill up this research gap. Also, none of the researchers have aimed to tackle the 2–D circular tapering impact on the mode of frequency in the case of orthotropic parallelogram plate. We will also address this issue.

In this paper, the authors studied the impact of 2–D (two-dimensional) circular tapering on the time period of vibrational modes of frequency of the nonhomogeneous orthotropic parallelogram plate on *CCCC*, *CCCF*, *CFCF*, *CSCF*, and *SFSF* boundary conditions. The authors also evaluated 1–D (one-dimensional) circular density and 2–D (two-dimensional) parabolic temperature impacts on the time period of vibrational modes of frequency. All the results displayed in the tabular form (refer Tables 1–3). In order to authenticate our findings, authors performed comparatively

analysis of time period and modes of frequency of the orthotropic parallelogram plate (*SSSS* and *CCCC* edge condition), rectangle plate (*CCCC* edge condition), and square plate (*CCCC*, *SCSC*, *FCCF*, and *SFSF* edge conditions) with the available published results (refer Tables 4–10).

## 2. Analysis

The orthotropic parallelogram plates made with nonhomogeneous material properties with variable thickness  $l$  having skew angle  $\theta$ , length  $a$ , breadth  $b$ , density  $\rho$ , and Poisson's ratio  $\nu$  referred to the skew coordinates  $\zeta = x - y \tan \theta$  and  $\psi = y \sec \theta$  (refer Figure 1).

The thickness  $l$  of the skew plate is assumed to be circular in both dimensions (refer Figure 2), and density  $\rho$  is assumed to be circular in one dimension as

$$\begin{aligned} l &= l_0 \left[ 1 + \beta_1 \left( 1 - \sqrt{1 - \frac{\zeta^2}{a^2}} \right) \right] \left[ 1 + \beta_2 \left( 1 - \sqrt{1 - \frac{\psi^2}{b^2}} \right) \right], \\ \rho &= \rho_0 \left[ 1 - m \left( 1 - \sqrt{1 - \frac{\zeta^2}{a^2}} \right) \right], \end{aligned} \quad (1)$$

where  $l_0$  and  $\rho_0$  are the thickness and density of the plate, respectively, at the origin. Also,  $\beta_1, \beta_2$  ( $0 \leq \beta_1, \beta_2 \leq 1$ ) and  $m$  ( $0 \leq m < 1$ ) are taper parameters and nonhomogeneity parameter, respectively.

Two-dimensional steady state temperature variations on the plate are considered to be parabolic as taken in [13]

$$\tau = \tau_0 \left( 1 - \frac{\zeta^2}{a^2} \right) \left( 1 - \frac{\psi^2}{b^2} \right), \quad (2)$$

where  $\tau$  and  $\tau_0$  denotes the temperature excess above the reference temperature on the plate at any point and at the origin, respectively.

The temperature-dependent modulus of elasticity for engineering structures is taken as in [14]

$$\begin{aligned} E_\zeta(\tau) &= E_1 (1 - \gamma\tau), \quad E_\psi(\tau) = E_2 (1 - \gamma\tau), \\ G_{\zeta\psi}(\tau) &= G_0 (1 - \gamma\tau), \end{aligned} \quad (3)$$

where  $E_\zeta$  and  $E_\psi$  are Young's moduli in  $\zeta$  and  $\psi$  directions, respectively,  $G_{\zeta\psi}$  is shear modulus, and  $\gamma$  is taken as the slope variation of moduli with temperature.

Substituting (2) in (3), we get the following expressions:

$$\begin{aligned} E_\zeta(\tau) &= E_1 \left[ 1 - \alpha \left( 1 - \frac{\zeta^2}{a^2} \right) \left( 1 - \frac{\psi^2}{b^2} \right) \right], \\ E_\psi(\tau) &= E_2 \left[ 1 - \alpha \left( 1 - \frac{\zeta^2}{a^2} \right) \left( 1 - \frac{\psi^2}{b^2} \right) \right], \\ G_{\zeta\psi}(\tau) &= G_0 \left[ 1 - \alpha \left( 1 - \frac{\zeta^2}{a^2} \right) \left( 1 - \frac{\psi^2}{b^2} \right) \right], \end{aligned} \quad (4)$$

where  $\alpha = \gamma\tau_0$ , ( $0 \leq \alpha < 1$ ) is called the temperature gradient.

TABLE 1: Time period of the orthotropic parallelogram plate at *CCCC*, *CCCF*, *CFCF*, *CSCF*, and *SFSF* edge conditions corresponding to both tapering parameters  $\beta_1$  and  $\beta_2$ .

		$m = 0.2, \alpha = 0.4$											
		$\beta_2 = 0.0$		$\beta_2 = 0.2$		$\beta_2 = 0.4$		$\beta_2 = 0.6$		$\beta_2 = 0.8$		$\beta_2 = 1.0$	
$\beta_1$		$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$
CCCC	0.0	0.16309	0.62562	0.15807	0.60548	0.15315	0.58591	0.14831	0.56693	0.14362	0.54865	0.13905	0.53102
	0.2	0.15367	0.59097	0.14909	0.57262	0.14457	0.55471	0.14013	0.53734	0.13581	0.52059	0.13160	0.50445
	0.4	0.14441	0.55792	0.14022	0.54114	0.13608	0.52474	0.13201	0.50884	0.12803	0.49345	0.12416	0.47862
	0.6	0.13551	0.52688	0.13167	0.51155	0.12788	0.49650	0.12415	0.48192	0.12049	0.46778	0.11692	0.45412
	0.8	0.12710	0.49816	0.12358	0.48403	0.12010	0.47020	0.11667	0.45676	0.11330	0.44372	0.11001	0.43109
	1.0	0.11926	0.47168	0.11603	0.45864	0.11282	0.44586	0.10965	0.43345	0.10654	0.42135	0.10351	0.40966
CCCF	0.0	0.18375	0.59876	0.17094	0.56505	0.15918	0.53461	0.14848	0.50709	0.13883	0.48205	0.13011	0.45921
	0.2	0.17587	0.56935	0.16385	0.53834	0.15277	0.51026	0.14266	0.48465	0.13350	0.46128	0.12522	0.43992
	0.4	0.16788	0.54054	0.15665	0.51218	0.14625	0.48629	0.13673	0.46254	0.12808	0.44083	0.12024	0.42085
	0.6	0.15993	0.51293	0.14948	0.48695	0.13976	0.46310	0.13082	0.44114	0.12267	0.42094	0.11527	0.40228
	0.8	0.15215	0.48676	0.14245	0.46295	0.13338	0.44095	0.12501	0.42063	0.11735	0.40181	0.11036	0.38441
	1.0	0.14465	0.46219	0.13564	0.44033	0.12719	0.42000	0.11936	0.40115	0.11216	0.38365	0.10559	0.36741
CFCF	0.0	0.36163	0.78754	0.34906	0.74915	0.33628	0.71107	0.32349	0.67419	0.31091	0.63900	0.29866	0.60589
	0.2	0.34291	0.72835	0.33134	0.69379	0.31947	0.65955	0.30755	0.62625	0.29574	0.59442	0.28419	0.56439
	0.4	0.32421	0.67356	0.31352	0.64252	0.30249	0.61164	0.29132	0.58157	0.28022	0.55286	0.26933	0.52565
	0.6	0.30590	0.62420	0.29599	0.59612	0.28567	0.56819	0.27519	0.54111	0.26474	0.51507	0.25444	0.49040
	0.8	0.28826	0.58016	0.27902	0.55474	0.26934	0.52945	0.25948	0.50489	0.24959	0.48129	0.23985	0.45892
	1.0	0.27148	0.54123	0.26282	0.51811	0.25372	0.49512	0.24440	0.47275	0.23504	0.45129	0.22581	0.43090
CSCF	0.0	0.37061	0.76699	0.35126	0.70598	0.33276	0.65188	0.31529	0.60416	0.29896	0.56194	0.28379	0.52462
	0.2	0.35541	0.70202	0.33697	0.64698	0.31925	0.59800	0.30253	0.55471	0.28689	0.51638	0.27234	0.48242
	0.4	0.33964	0.64252	0.32201	0.59291	0.30508	0.54871	0.28907	0.50950	0.27409	0.47473	0.26014	0.44391
	0.6	0.32358	0.58971	0.30674	0.54491	0.29051	0.50501	0.27515	0.46948	0.26079	0.43800	0.24743	0.41001
	0.8	0.30755	0.54353	0.29139	0.50310	0.27581	0.46694	0.26106	0.43480	0.24726	0.40621	0.23445	0.38070
	1.0	0.29174	0.50354	0.27620	0.46694	0.26121	0.43417	0.24703	0.40492	0.23379	0.37888	0.22149	0.35560
SFSF	0.0	0.29229	1.6282	0.28379	1.5506	0.27512	1.4737	0.26640	1.3990	0.25774	1.3275	0.24924	1.2597
	0.2	0.27132	1.5574	0.26415	1.4821	0.25676	1.4077	0.24927	1.3356	0.24179	1.2666	0.23439	1.2013
	0.4	0.25116	1.4899	0.24510	1.4165	0.23879	1.3442	0.23236	1.2744	0.22589	1.2078	0.21944	1.1449
	0.6	0.23233	1.4263	0.22716	1.3545	0.22175	1.2840	0.21619	1.2162	0.21056	1.1517	0.20492	1.0910
	0.8	0.21506	1.3666	0.21059	1.2962	0.20590	1.2274	0.20106	1.1614	0.19612	1.0989	0.19117	1.0401
	1.0	0.19938	1.3107	0.19549	1.2416	0.19137	1.1744	0.18711	1.1101	0.18275	1.0493	0.17836	0.99243

TABLE 2: Time period of the orthotropic parallelogram plate at *CCCC*, *CCCF*, *CFCF*, *CSCF*, and *SFSF* edge conditions corresponding to thermal gradient  $\alpha$ .

		$m = 0.2$											
$\alpha$		$\beta_1 = \beta_2 = 0.0$		$\beta_1 = \beta_2 = 0.2$		$\beta_1 = \beta_2 = 0.4$		$\beta_1 = \beta_2 = 0.6$		$\beta_1 = \beta_2 = 0.8$		$\beta_1 = \beta_2 = 1.0$	
		$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$
CCCC	0.0	0.14745	0.56414	0.13598	0.51987	0.12512	0.47909	0.11500	0.44190	0.10566	0.40825	0.09710	0.37800
	0.2	0.15468	0.59241	0.14208	0.54428	0.13026	0.50027	0.11931	0.46046	0.10928	0.42474	0.10015	0.39276
	0.4	0.16309	0.62562	0.14909	0.57262	0.13608	0.52474	0.12415	0.48192	0.11330	0.44372	0.10351	0.40966
	0.6	0.17303	0.66527	0.15724	0.60627	0.14275	0.55368	0.12961	0.50712	0.11779	0.46593	0.10722	0.42949
	0.8	0.18503	0.71396	0.16688	0.64711	0.15050	0.58858	0.13586	0.53740	0.12286	0.49257	0.11135	0.45311
CCCF	0.0	0.17190	0.55465	0.15450	0.50036	0.13884	0.45314	0.12490	0.41196	0.11258	0.37596	0.10171	0.34432
	0.2	0.17753	0.57532	0.15898	0.51821	0.14241	0.46870	0.12776	0.42569	0.11489	0.38814	0.10360	0.35519
	0.4	0.18375	0.59876	0.16385	0.53834	0.14625	0.48629	0.13082	0.44114	0.11735	0.40181	0.10559	0.36741
	0.6	0.19066	0.62574	0.16920	0.56150	0.15043	0.50633	0.13411	0.45874	0.11997	0.41736	0.10770	0.38117
	0.8	0.19839	0.65747	0.17508	0.58855	0.15496	0.52971	0.13764	0.47909	0.12275	0.43517	0.10993	0.39694
CFCF	0.0	0.32761	0.72420	0.30262	0.64629	0.27855	0.57498	0.25551	0.51170	0.23363	0.45676	0.21303	0.40960
	0.2	0.34338	0.75380	0.31601	0.66866	0.28980	0.59219	0.26484	0.52553	0.24126	0.46826	0.21918	0.41959
	0.4	0.36163	0.78754	0.33134	0.69379	0.30249	0.61164	0.27519	0.54111	0.24959	0.48129	0.22581	0.43090
	0.6	0.38312	0.82668	0.34906	0.72263	0.31689	0.63372	0.28676	0.55886	0.25875	0.49628	0.23298	0.44388
	0.8	0.40888	0.87292	0.36986	0.75625	0.33348	0.65948	0.29977	0.57963	0.26885	0.51375	0.24073	0.45918

TABLE 2: Continued.

		$m = 0.2$											
$\alpha$	$\beta_1 = \beta_2 = 0.0$		$\beta_1 = \beta_2 = 0.2$		$\beta_1 = \beta_2 = 0.4$		$\beta_1 = \beta_2 = 0.6$		$\beta_1 = \beta_2 = 0.8$		$\beta_1 = \beta_2 = 1.0$		
	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	
CSCF	0.0	0.34199	0.73689	0.31288	0.62662	0.28512	0.53401	0.25890	0.45792	0.23429	0.39622	0.21136	0.34639
	0.2	0.35544	0.75147	0.32424	0.63649	0.29461	0.54111	0.26668	0.46351	0.24055	0.40096	0.21629	0.35073
	0.4	0.37061	0.76699	0.33697	0.64698	0.30508	0.54871	0.27515	0.46948	0.24726	0.40621	0.22149	0.35560
	0.6	0.38789	0.78358	0.35123	0.65817	0.31670	0.55688	0.28443	0.47611	0.25449	0.41205	0.22699	0.36110
	0.8	0.40784	0.80142	0.36747	0.67017	0.32971	0.56574	0.29460	0.48343	0.26225	0.41865	0.23277	0.36735
SFSF	0.0	0.26839	1.4686	0.24490	1.3499	0.22325	1.2354	0.20355	1.1270	0.18578	1.0257	0.16983	0.93243
	0.2	0.27958	1.5420	0.25398	1.4111	0.23062	1.2862	0.20959	1.1689	0.19075	1.0602	0.17394	0.96089
	0.4	0.29229	1.6282	0.26415	1.4821	0.23879	1.3442	0.21619	1.2162	0.19612	1.0989	0.17836	0.99243
	0.6	0.30692	1.7316	0.27564	1.5656	0.24788	1.4115	0.22345	1.2703	0.20198	1.1424	0.18314	1.0276
	0.8	0.32396	1.8591	0.28876	1.6665	0.25810	1.4910	0.23149	1.3331	0.20839	1.1921	0.18832	1.0671

TABLE 3: Time period of the orthotropic parallelogram plate at CCCC, CCCF, CFCF, CSCF, and SFSF edge conditions corresponding to nonhomogeneity  $m$ .

		$\alpha = 0.4$											
$m$	$\beta_1 = \beta_2 = 0.0$		$\beta_1 = \beta_2 = 0.2$		$\beta_1 = \beta_2 = 0.4$		$\beta_1 = \beta_2 = 0.6$		$\beta_1 = \beta_2 = 0.8$		$\beta_1 = \beta_2 = 1.0$		
	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	$K_1$	$K_2$	
CCCC	0.0	0.16035	0.61629	0.14653	0.56401	0.13369	0.51682	0.12193	0.47460	0.11124	0.43693	0.10159	0.40338
	0.2	0.16309	0.62562	0.14909	0.57262	0.13608	0.52474	0.12415	0.48192	0.11330	0.44372	0.10351	0.40966
	0.4	0.16578	0.63479	0.15160	0.58107	0.13843	0.53256	0.12632	0.48912	0.11533	0.45041	0.10539	0.41589
	0.6	0.16842	0.64384	0.15408	0.58943	0.14072	0.54026	0.12847	0.49622	0.11732	0.45701	0.10724	0.42198
	0.8	0.17102	0.65276	0.15651	0.59766	0.14299	0.54783	0.13057	0.50325	0.11927	0.46348	0.10906	0.42801
CCCF	0.0	0.18087	0.58993	0.16124	0.53036	0.14389	0.47897	0.12868	0.43448	0.11539	0.39575	0.10381	0.36182
	0.2	0.18375	0.59876	0.16385	0.53834	0.14625	0.48629	0.13082	0.44114	0.11735	0.40181	0.10559	0.10559
	0.4	0.18659	0.60749	0.16642	0.54623	0.14859	0.49342	0.13293	0.44768	0.11927	0.40781	0.10734	0.37288
	0.6	0.18938	0.61607	0.16896	0.55402	0.15088	0.50049	0.13501	0.45412	0.12115	0.41372	0.10906	0.37831
	0.8	0.19213	0.62452	0.17145	0.56166	0.15313	0.50743	0.13706	0.46046	0.12301	0.41956	0.11075	0.38368
CFCF	0.0	0.35632	0.77579	0.32644	0.68336	0.29794	0.60231	0.27100	0.53278	0.24575	0.47391	0.22229	0.42424
	0.2	0.36163	0.78754	0.33134	0.69379	0.30249	0.61164	0.27519	0.54111	0.24959	0.48129	0.22581	0.43090
	0.4	0.36684	0.79916	0.33618	0.70416	0.30695	0.62075	0.27930	0.54925	0.25338	0.48858	0.22927	0.43744
	0.6	0.37200	0.81060	0.34093	0.71427	0.31136	0.62977	0.28336	0.55726	0.25710	0.49574	0.23269	0.44385
	0.8	0.37705	0.82184	0.34564	0.72433	0.31570	0.63869	0.28736	0.56517	0.26077	0.50281	0.23605	0.45022
CSCF	0.0	0.36524	0.75543	0.33204	0.63718	0.30056	0.54029	0.27104	0.46229	0.24352	0.39993	0.21809	0.35010
	0.2	0.37061	0.76699	0.33697	0.64698	0.30508	0.54871	0.27515	0.46948	0.24726	0.40621	0.22149	0.35560
	0.4	0.37589	0.77830	0.34181	0.65666	0.30954	0.55697	0.27922	0.47661	0.25096	0.41237	0.22484	0.36103
	0.6	0.38114	0.78948	0.34661	0.66614	0.31393	0.56508	0.28322	0.48362	0.25461	0.41846	0.22815	0.36634
	0.8	0.38629	0.80054	0.35133	0.67557	0.31824	0.57312	0.28717	0.49053	0.25820	0.42446	0.23140	0.37162
SFSF	0.0	0.28765	1.6025	0.25987	1.4583	0.23487	1.3223	0.21258	1.1961	0.19281	1.0805	0.17531	0.97559
	0.2	0.29229	1.6282	0.26415	1.4821	0.23879	1.3442	0.21619	1.2162	0.19612	1.0989	0.17836	0.99243
	0.4	0.29688	1.6536	0.26835	1.5055	0.24265	1.3658	0.21973	1.2360	0.19938	1.1170	0.18136	1.0090
	0.6	0.30138	1.6786	0.27250	1.5286	0.24646	1.3871	0.22322	1.2554	0.20258	1.1347	0.18431	1.0252
	0.8	0.30581	1.7032	0.27656	1.5514	0.25020	1.4079	0.22665	1.2746	0.20574	1.1523	0.18721	1.0413

TABLE 4: Comparison of modes of frequency of the present study (orthotropic parallelogram plate) and obtained in [14] corresponding to tapering parameter  $\beta_1$  for a fixed value of aspect ratio  $a/b = 1.5$ .

BC	$\beta_1$	$\alpha = \beta_2 = m = 0.0, \theta = 30^\circ$		$\alpha = \beta_2 = m = 0.4, \theta = 45^\circ$		$\alpha = \beta_2 = m = 0.8, \theta = 60^\circ$	
		$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$
SSSS	0.0	06.71	42.63	05.74	36.23	04.81	30.75
		<b>11.18</b>	<b>101.84</b>	<b>11.03</b>	<b>101.40</b>	<b>09.83</b>	<b>88.88</b>
	0.2	06.96	45.46	06.02	38.95	05.11	33.26
		<b>12.33</b>	<b>113.01</b>	<b>12.38</b>	<b>114.77</b>	<b>11.29</b>	<b>103.40</b>
	0.4	07.22	48.66	06.30	41.99	05.41	36.00
		<b>13.52</b>	<b>125.78</b>	<b>13.78</b>	<b>129.71</b>	<b>12.77</b>	<b>119.22</b>
0.6	07.50	52.17	06.59	45.28	05.72	38.95	
	<b>14.73</b>	<b>139.73</b>	<b>15.20</b>	<b>145.76</b>	<b>14.28</b>	<b>135.97</b>	
0.8	07.78	55.95	06.90	48.80	06.04	42.08	
	<b>15.98</b>	<b>154.53</b>	<b>16.64</b>	<b>162.61</b>	<b>15.79</b>	<b>153.39</b>	

Bold values are obtained from [14].

TABLE 5: Comparison of modes of frequency of the present study (orthotropic parallelogram plate) and obtained in [14] corresponding to tapering parameter  $\beta_2$  for a fixed value of aspect ratio  $a/b = 1.5$ .

BC	$\beta_2$	$\alpha = \beta_1 = m = 0.0, \theta = 30^\circ$		$\alpha = \beta_1 = m = 0.4, \theta = 45^\circ$		$\alpha = \beta_1 = m = 0.8, \theta = 60^\circ$	
		$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$
SSSS	0.0	06.71	42.63	05.74	38.89	04.79	34.79
		<b>11.18</b>	<b>101.84</b>	<b>11.06</b>	<b>107.11</b>	<b>09.95</b>	<b>106.48</b>
	0.2	06.96	44.05	06.01	40.38	05.10	36.44
		<b>12.32</b>	<b>112.17</b>	<b>12.41</b>	<b>118.28</b>	<b>11.38</b>	<b>117.87</b>
	0.4	07.22	45.56	06.30	41.99	05.41	38.21
		<b>13.51</b>	<b>122.74</b>	<b>13.78</b>	<b>129.71</b>	<b>12.84</b>	<b>129.53</b>
0.6	07.50	47.17	06.60	43.69	05.72	40.09	
	<b>14.73</b>	<b>133.49</b>	<b>15.18</b>	<b>141.33</b>	<b>14.31</b>	<b>141.39</b>	
0.8	07.79	48.86	06.90	45.48	06.04	42.08	
	<b>15.97</b>	<b>144.39</b>	<b>16.62</b>	<b>153.11</b>	<b>15.80</b>	<b>153.40</b>	

Bold values are obtained from [14].

TABLE 6: Comparison of modes of frequency of the present study (orthotropic parallelogram plate) and obtained in [14] corresponding to nonhomogeneity  $m$  for a fixed value of aspect ratio  $a/b = 1.5$ .

BC	$m$	$\alpha = \beta_1 = \beta_2 = 0.0, \theta = 30^\circ$		$\alpha = \beta_1 = \beta_2 = 0.4, \theta = 45^\circ$		$\alpha = \beta_1 = \beta_2 = 0.8, \theta = 60^\circ$	
		$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$
SSSS	0.0	06.71	42.63	06.50	43.62	06.43	45.45
		<b>11.18</b>	<b>101.84</b>	<b>12.29</b>	<b>115.39</b>	<b>12.08</b>	<b>115.82</b>
	0.2	06.61	41.85	06.40	42.78	06.33	44.53
		<b>11.78</b>	<b>107.35</b>	<b>12.97</b>	<b>121.93</b>	<b>12.76</b>	<b>122.59</b>
	0.4	06.51	41.12	06.30	41.99	06.23	43.66
		<b>12.50</b>	<b>113.86</b>	<b>13.78</b>	<b>129.71</b>	<b>13.57</b>	<b>130.72</b>
0.6	06.41	40.42	06.20	41.24	06.13	42.85	
	<b>13.36</b>	<b>121.72</b>	<b>14.76</b>	<b>139.21</b>	<b>14.56</b>	<b>140.70</b>	
0.8	06.32	39.76	06.11	40.53	06.04	42.08	
	<b>14.43</b>	<b>131.47</b>	<b>15.98</b>	<b>151.15</b>	<b>15.79</b>	<b>153.39</b>	

Bold values are obtained from [14].

TABLE 7: Comparison of time period of the present study (orthotropic parallelogram plate) and obtained in [15] corresponding to tapering parameter  $\beta_1$  for the fixed value of aspect ratio  $a/b = 1.5$ .

BC	$\beta_1$	$\theta = 0^\circ$		$\theta = 45^\circ$	
		$K_1$	$K_2$	$K_1$	$K_2$
CCCC	0.0	0.13285	0.51082	0.16123	0.61588
		<b>0.03735</b>	<b>0.14364</b>	<b>0.02407</b>	<b>0.09130</b>
	0.2	0.12599	0.48513	0.15323	0.58578
		<b>0.03446</b>	<b>0.13278</b>	<b>0.02229</b>	<b>0.08463</b>
	0.4	0.11912	0.45999	0.14520	0.55628
		<b>0.03166</b>	<b>0.12252</b>	<b>0.02229</b>	<b>0.07832</b>
	0.6	0.11240	0.43599	0.13733	0.52804
<b>0.02906</b>		<b>0.11315</b>	<b>0.01896</b>	<b>0.07254</b>	
0.8	0.10595	0.41343	0.12974	0.50137	
		<b>0.02669</b>	<b>0.10476</b>	<b>0.01749</b>	<b>0.06734</b>

Bold values are obtained from [15].

TABLE 8: Comparison of the time period of the orthotropic rectangle plate and obtained in [38] corresponding to nonhomogeneity  $m$  for a fixed value of aspect ratio  $a/b = 1.5$ .

BC	$m$	$\beta_1 = 0.0$		$\beta_1 = 0.4$	
		$K_1$	$K_2$	$K_1$	$K_2$
CCCC	0.0	0.13285	0.51082	0.11912	0.45999
		<b>0.02978</b>	<b>0.14981</b>	<b>0.02554</b>	<b>0.12964</b>
	0.2	0.13511	0.51855	0.12124	0.46709
		<b>0.02980</b>	<b>0.15016</b>	<b>0.02535</b>	<b>0.12919</b>
	0.4	0.13733	0.52619	0.12333	0.47407
		<b>0.02982</b>	<b>0.15045</b>	<b>0.02519</b>	<b>0.12883</b>
	0.6	0.13952	0.53370	0.12538	0.48092
<b>0.02983</b>		<b>0.15070</b>	<b>0.02506</b>	<b>0.12853</b>	
0.8	0.14168	0.5411	0.12740	0.48770	
		<b>0.02984</b>	<b>0.15091</b>	<b>0.02491</b>	<b>0.12827</b>

Bold values are obtained from [38].

TABLE 9: Comparison of the time period of the orthotropic rectangle plate and obtained in [38] corresponding to tapering parameter  $\beta_1$  for aspect ratio  $a/b = 1.5$ .

BC	$\beta_1$	$m = 0.0$		$m = 0.4$	
		$K_1$	$K_2$	$K_1$	$K_2$
CCCC	0.0	0.13285	0.51082	0.13733	0.52619
		<b>0.02978</b>	<b>0.14981</b>	<b>0.02982</b>	<b>0.15045</b>
	0.2	0.12599	0.48513	0.13035	0.49983
		<b>0.02755</b>	<b>0.13908</b>	<b>0.02736</b>	<b>0.13886</b>
	0.4	0.11912	0.45999	0.12333	0.47407
		<b>0.02554</b>	<b>0.12964</b>	<b>0.02519</b>	<b>0.12883</b>
	0.6	0.11240	0.43599	0.11645	0.44941
<b>0.02374</b>		<b>0.12132</b>	<b>0.02328</b>	<b>0.12009</b>	
0.8	0.10595	0.41343	0.10984	0.42625	
		<b>0.02214</b>	<b>0.11396</b>	<b>0.02160</b>	<b>0.11243</b>

Bold values are obtained from [38].

TABLE 10: Comparison of modes of frequency of the isotropic square plate and obtained in [39–50] at CCCC, SCSC, FCFC, and FSFS edge conditions.

Boundary conditions	Ref	$\lambda_1$
CCCC	[39]	35.98
	[40]	35.99
	[41]	35.98
	[42]	35.98
	[43]	35.99
	[44]	35.99
	[45]	35.99
	[46]	35.99
	Present	<b>33.33</b>
SCSC	[39]	28.950
	[40]	28.951
	[47]	28.955
	[48]	29.951
	Present	<b>28.911</b>
FCFC	[39]	22.19
	[40]	22.27
	[49]	22.03
	Present	<b>22.43</b>
FSFS	[39]	9.631
	[40]	9.631
	[49]	9.631
	[50]	9.631
	Present	<b>10.574</b>

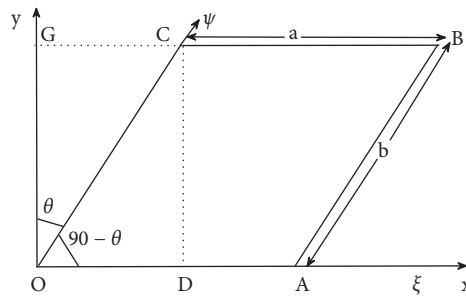


FIGURE 1: Orthotropic parallelogram plate with a skew angle  $\theta$ .

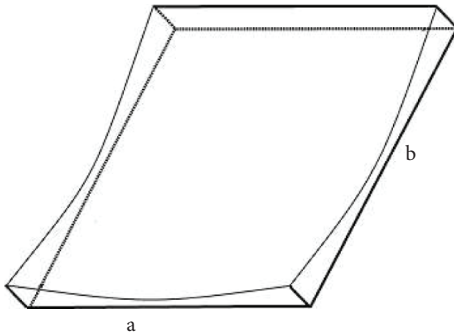


FIGURE 2: Orthotropic parallelogram plate having a two-dimensional circular thickness.

The flexural rigidities  $D_\zeta, D_\psi$  and torsional rigidity  $D_{\zeta\psi}$  of the plate are taken as in [14]

$$D_\zeta = \frac{E_\zeta l^3}{12(1 - \nu_\zeta \nu_\psi)}, D_\psi = \frac{E_\psi l^3}{12(1 - \nu_\zeta \nu_\psi)}, \tag{5}$$

$$D_{\zeta\psi} = \frac{G_{\zeta\psi} l^3}{12}, D_1 = \nu_\zeta D_\psi = \nu_\psi D_\zeta,$$

where  $\nu_\zeta$  and  $\nu_\psi$  are Poisson's ratios.

Using (3) and (4) in (5), we get

$$\begin{aligned}
D_\zeta &= \frac{E_1 h_0^3}{12(1-\nu_\zeta \nu_\psi)} \left[ \begin{array}{c} \left\{ 1 - \alpha \left( 1 - \frac{\zeta^2}{a^2} \right) \left( 1 - \frac{\psi^2}{b^2} \right) \right\} \\ \left\{ \left( 1 + \beta_1 \left( 1 - \sqrt{1 - \frac{\zeta^2}{a^2}} \right) \right) \left( 1 + \beta_2 \left( 1 - \sqrt{1 - \frac{\psi^2}{b^2}} \right) \right) \right\}^3 \end{array} \right], \\
D_\psi &= \frac{E_2 h_0^3}{12(1-\nu_\zeta \nu_\psi)} \left[ \begin{array}{c} \left\{ 1 - \alpha \left( 1 - \frac{\zeta^2}{a^2} \right) \left( 1 - \frac{\psi^2}{b^2} \right) \right\} \\ \left\{ \left( 1 + \beta_1 \left( 1 - \sqrt{1 - \frac{\zeta^2}{a^2}} \right) \right) \left( 1 + \beta_2 \left( 1 - \sqrt{1 - \frac{\psi^2}{b^2}} \right) \right) \right\}^3 \end{array} \right], \\
D_{\zeta\psi} &= \frac{G_0 h_0^3}{12} \left[ \begin{array}{c} \left\{ 1 - \alpha \left( 1 - \frac{\zeta^2}{a^2} \right) \left( 1 - \frac{\psi^2}{b^2} \right) \right\} \\ \left\{ \left( 1 + \beta_1 \left( 1 - \sqrt{1 - \frac{\zeta^2}{a^2}} \right) \right) \left( 1 + \beta_2 \left( 1 - \sqrt{1 - \frac{\psi^2}{b^2}} \right) \right) \right\}^3 \end{array} \right], \\
D_1 &= \frac{E_1 h_0^3 \nu_\psi}{12(1-\nu_\zeta \nu_\psi)} \left[ \begin{array}{c} \left\{ 1 - \alpha \left( 1 - \frac{\zeta^2}{a^2} \right) \left( 1 - \frac{\psi^2}{b^2} \right) \right\} \\ \left\{ \left( 1 + \beta_1 \left( 1 - \sqrt{1 - \frac{\zeta^2}{a^2}} \right) \right) \left( 1 + \beta_2 \left( 1 - \sqrt{1 - \frac{\psi^2}{b^2}} \right) \right) \right\}^3 \end{array} \right].
\end{aligned} \tag{6}$$

Now, introducing nondimensional variable as

$$E_1^* = \frac{E_1}{1-\nu_\zeta \nu_\psi}, E_2^* = \frac{E_2}{1-\nu_\zeta \nu_\psi}, E^* = \nu_\zeta E_2^* = \nu_\psi E_1^*, \tag{7}$$

and components of  $E_1^*$ ,  $E_2^*$ ,  $E^*$  and  $G_0$  are  $E_1^*$ ,  $E_2^* \sec \theta$ ,  $E^* \sec \theta$ , and  $G_0 \sec \theta$ , respectively, in  $\zeta$  and  $\psi$  directions.

The equation for kinetic energy  $T_s$  and strain energy  $V_s$  for natural transverse vibration of a nonuniform orthotropic parallelogram is taken as in [15]

$$T_s = \frac{1}{2} \omega^2 \int_0^a \int_0^b \rho l \Phi^2 \cos \theta d\zeta d\psi, \tag{8}$$

$$\begin{aligned}
V_s &= \frac{1}{2} \int_0^a \int_0^b \left[ D_\zeta \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \right)^2 + D_\psi \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \tan^2 \theta - 2 \frac{\partial^2 \Phi}{\partial \zeta \partial \psi} \tan \theta \sec \theta + \frac{\partial^2 \Phi}{\partial \psi^2} \sec^2 \theta \right)^2 \right. \\
&\quad \left. + 2D_1 \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \right) \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \tan^2 \theta + 2 \frac{\partial^2 \Phi}{\partial \zeta \partial \psi} \tan \theta \sec \theta + \frac{\partial^2 \Phi}{\partial \psi^2} \sec^2 \theta \right) + 4D_{\zeta\psi} \left( -\frac{\partial^2 \Phi}{\partial \zeta^2} \tan \theta + \frac{\partial^2 \Phi}{\partial \zeta \partial \psi} \sec \theta \right)^2 \right] \cos \theta d\zeta d\psi.
\end{aligned} \tag{9}$$

$$J = \delta(V_s - T_s) = 0. \tag{10}$$

The Rayleigh-Ritz method requires that maximum strain energy must be equal to maximum kinetic energy, i.e.,

Substituting (8) and (9) in (10), we obtained

$$\begin{aligned}
J &= \frac{1}{2} \int_0^a \int_0^b \left[ D_\zeta \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \right)^2 + D_\psi \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \tan^2 \theta - 2 \frac{\partial^2 \Phi}{\partial \zeta \partial \psi} \tan \theta \sec \theta + \frac{\partial^2 \Phi}{\partial \psi^2} \sec^2 \theta \right)^2 \right. \\
&\quad \left. + 2D_1 \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \right) \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \tan^2 \theta + 2 \frac{\partial^2 \Phi}{\partial \zeta \partial \psi} \tan \theta \sec \theta + \frac{\partial^2 \Phi}{\partial \psi^2} \sec^2 \theta \right) + 4D_{\zeta\psi} \left( -\frac{\partial^2 \Phi}{\partial \zeta^2} \tan \theta + \frac{\partial^2 \Phi}{\partial \zeta \partial \psi} \sec \theta \right)^2 \right] \cos \theta d\zeta d\psi \\
&\quad - \frac{1}{2} \omega^2 \int_0^a \int_0^b \rho l \Phi^2 \cos \theta d\zeta d\psi.
\end{aligned} \tag{11}$$



Using Eqs. (1), (6) and (7), (11) becomes

$$\begin{aligned}
 J = \int_0^a \int_0^b & \left[ \left\{ 1 - \alpha \left( 1 - \frac{\zeta^2}{a^2} \right) \left( 1 - \frac{\psi^2}{b^2} \right) \right\} \{ (1 + \beta_1 \Upsilon_1)(1 + \beta_2 \Upsilon_2) \}^3 \right. \\
 & \left[ \left\{ \cos^4 \theta + \frac{E_2^*}{E_1^*} \sin^4 \theta + 2 \frac{E_2^*}{E_1^*} \sin^2 \theta \cos^2 \theta + 4 \frac{G_0}{E_1^*} \sin^2 \theta \cos^2 \theta \right\} \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \right)^2 + \frac{E_2^*}{E_1^*} \left( \frac{\partial^2 \Phi}{\partial \psi^2} \right)^2 \right. \\
 & + 4 \left\{ \frac{E_2^*}{E_1^*} \sin^2 \theta + \frac{G_0}{E_1^*} \cos^2 \theta \right\} \left( \frac{\partial^2 \Phi}{\partial \zeta \partial \psi} \right)^2 + 2 \left\{ \frac{E_2^*}{E_1^*} \sin^2 \theta + \frac{E_2^*}{E_1^*} \cos^2 \theta \right\} \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \right) \left( \frac{\partial^2 \Phi}{\partial \psi^2} \right) \\
 & - 4 \left\{ \frac{E_2^*}{E_1^*} \sin^3 \theta + 2 \frac{E_2^*}{E_1^*} \sin \theta \cos^2 \theta + 2 \frac{G_0}{E_1^*} \sin \theta \cos^2 \theta \right\} \left( \frac{\partial^2 \Phi}{\partial \zeta^2} \right) \left( \frac{\partial^2 \Phi}{\partial \zeta \partial \psi} \right) \\
 & \left. \left. - 4 \left\{ \frac{E_2^*}{E_1^*} \sin \theta \right\} \left( \frac{\partial^2 \Phi}{\partial \psi^2} \right) \left( \frac{\partial^2 \Phi}{\partial \zeta \partial \psi} \right) \right] d\zeta d\psi, \right. \\
 & \left. - \lambda^2 \int_0^a \int_0^b [(1 - m \Upsilon_1)(1 + \beta_1 \Upsilon_1)(1 + \beta_2 \Upsilon_2)] \Phi^2 d\zeta d\psi, \right.
 \end{aligned} \tag{12}$$

where  $\lambda^2 = 12\rho_0 a^2 \cos^5 \theta / E_1^* h_0^2$ ,  $\Upsilon_1 = (1 - \sqrt{1 - \zeta^2/a^2})$ , and  $\Upsilon_2 = (1 - \sqrt{1 - \psi^2/b^2})$ .

The two-term deflection function, which satisfies all the edge conditions, can be taken as in [6]

$$\begin{aligned}
 \Phi(\zeta, \psi) = & \left[ \left( \frac{\zeta}{a} \right)^e \left( \frac{\psi}{b} \right)^f \left( 1 - \frac{\zeta}{a} \right)^g \left( 1 - \frac{\psi}{b} \right)^h \right] \\
 & \times \left[ \sum_{i=0}^N \Omega_i \left\{ \left( \frac{\zeta}{a} \right) \left( \frac{\psi}{b} \right) \left( 1 - \frac{\zeta}{a} \right) \left( 1 - \frac{\psi}{b} \right) \right\}^i \right],
 \end{aligned} \tag{13}$$

which is the product of two functions. Here, the first function represents the boundary conditions depending on the value of  $e, f, g$ , and  $h$ , which can take different values depending upon the support edge condition. Values 0, 1, 2 are assigned for free edge, simply supported, and clamped edge, respectively. The second function represents the number of modes of frequencies and  $\Omega_i, i = 0, 1, 2, \dots, N$ , represents arbitrary constants.

In order to minimize the functional given in (12), we require the following condition:

$$\frac{\delta J}{\delta \Omega_i} = 0, i = 0, 1, 2, 3 \dots N. \tag{14}$$

After simplifying (14), we get a homogeneous system of equations in  $\Omega_i$  whose nonzero solution gives an equation of frequency as

$$|P - \lambda^2 Q| = 0, \tag{15}$$

where  $P = [p_{ij}]_{N+1}$  and  $Q = [q_{ij}]_{N+1}$  are the square matrix of order  $(n + 1), i = 0, 1, 2 \dots N$  and  $j = 0, 1, 2 \dots N$ .

The following expression is used for calculating the time period:

$$K = \frac{2\pi}{\lambda}, \tag{16}$$

where  $\lambda$  is a frequency obtained from (15).

### 3. Numerical Results and Discussion

For a fixed value of aspect ratio  $a/b = 1.5$  and skew angle  $\theta = 30^\circ$ , the time period  $K$  for the first two modes of vibration of an orthotropic parallelogram plate with 2-D circular thickness and 1-D circular density under 2-D parabolic temperature is computed at *CCCC*, *CCCF*, *CFCF*, *CSCF* and *SFSF* edge conditions (refer Figure 3) corresponding to different plate parameters (tapering parameters  $\beta_1, \beta_2$ , thermal gradient  $\alpha$ , and non-homogeneity  $m$ ). In this study, the authors examined the impact of plate parameters on the behavior of time period of vibrational modes. During the calculation, the values of the following orthotropic material parameters are taken as in [15]:

$$\frac{E_2^*}{E_1^*} = 0.01, \frac{E^*}{E_1^*} = 0.3, \frac{G_0}{E_1^*} = 0.0333, \tag{17}$$

$$\frac{E_1^*}{\rho_0} = 3.0 \times 10^5 \text{ and } \nu_0 = 0.345.$$

All the results are conferred within Tables 1–3.

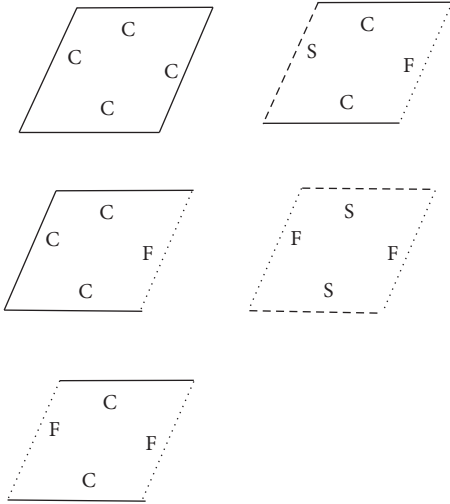


FIGURE 3: Orthotropic parallelogram plate with different edge conditions.

Table 1 represents the time period  $K$  of orthotropic parallelogram plate at  $CCCC$ ,  $CCCF$ ,  $CFCF$ ,  $CSCF$ , and  $SFSF$  edge conditions for the fixed value of thermal gradient  $\alpha = 0.4$  and nonhomogeneity  $m = 0.2$  corresponding to both tapering parameters  $\beta_1$  and  $\beta_2$ . The following observations can be drawn from Table 1:

- (i) Time period  $K$  decreases corresponding to both increasing value of the tapering parameters  $\beta_1$  and  $\beta_2$  at all the edge conditions.
- (ii) Under  $CSCF$  edge condition, the time periods  $K$  of vibrational modes are higher and less on  $CCCC$  edge condition. For different edge conditions, the time period  $K$  of vibrational modes in increasing order, corresponding to tapering parameters  $\beta_1$  and  $\beta_2$ , is  $CCCC < CCCF < SFSF < CFCF < CSCF$ .
- (iii) The rate of decrement in the time period  $K$  corresponding to the tapering parameter  $\beta_1$  is higher at  $CCCC$ ,  $CFCF$ , and  $SFSF$  in comparison to the rate of decrement in the time period  $K$  corresponding to the tapering parameter  $\beta_2$ , while the rate of decrement corresponding to the tapering parameter  $\beta_2$  is higher at  $CCCF$  and  $CSCF$  corresponding to tapering parameter  $\beta_2$  in comparison to the rate of decrement in the time period  $K$  corresponding to the tapering parameter  $\beta_1$ .
- (iv) For different edge conditions, the rate of decrement in time period  $K$  of vibrational modes in ascending order corresponding to tapering parameter  $\beta_1$  is  $CCCF < CSCF < CFCF < CCCC < SFSF$ , while for different edge conditions, the rate of decrement in time period  $K$  of vibrational modes in ascending order corresponding to tapering parameter  $\beta_2$  is  $SFSF < CCCC < CFCF < CSCF < CCCF$ .

Table 2 displays the time period  $K$  of the orthotropic parallelogram plate having variation in tapering parameters  $\beta_1$  and  $\beta_2$  from 0.0 to 0.8 and for fixed value of

nonhomogeneity  $m = 0.2$  corresponding to thermal gradient  $\alpha$  at  $CCCC$ ,  $CCCF$ ,  $CFCF$ ,  $CSCF$ , and  $SFSF$  edge conditions. The subsequent observations can be drawn from Table 2:

- (i) As the value of thermal gradient  $\alpha$  increases, the time period  $K$  of vibrational modes also increases but the time period  $K$  of vibrational modes decreases with the increasing value of tapering parameters  $\beta_1$  and  $\beta_2$  at all edge conditions.
- (ii) Like in Table 1, the time period  $K$  of vibrational modes is higher on  $CSCF$  edge condition and less on  $CCCC$  edge condition. For different edge conditions, the time period  $K$  of vibrational modes in increasing order corresponding to thermal gradients  $\alpha$  is  $CCCC < CCCF < SFSF < CFCF < CSCF$ .
- (iii) At  $CCCC$  edge condition, the rate of increment in time period  $K$  is higher corresponding to thermal gradient  $\alpha$  in comparison to the rate of decrement corresponding to tapering parameters  $\beta_1$  and  $\beta_2$ , while on the rest of the edge conditions, i.e.,  $CCCF$ ,  $CFCF$ ,  $CSCF$ , and  $SFSF$ , the rate of increment in time period  $K$  is smaller corresponding to thermal gradient  $\alpha$  in comparison to the rate of decrement corresponding to tapering parameters  $\beta_1$  and  $\beta_2$ .
- (iv) The rate of increment in time period  $K$  of vibrational modes is higher on  $CCCC$  edge condition and less in  $CCCF$  edge condition corresponding to thermal gradient  $\alpha$ , while the rate of decrement in time period  $K$  of vibrational modes is higher on  $CCCF$  edge condition and less in  $CCCC$  edge condition corresponding to tapering parameters  $\beta_1$  and  $\beta_2$ . For different edge conditions, the rate of increment in time period  $K$  of vibrational modes in ascending order corresponding to thermal gradient  $\alpha$  is  $CCCF < CSCF < SFSF < CFCF < CCCC$ . But the rate of decrement in time period  $K$  of vibrational modes in ascending order corresponding to tapering parameters  $\beta_1$  and  $\beta_2$  is  $CCCC < CFCF < SFSF < CSCF < CCCF$ .

Table 3 provides the time period  $K$  of the orthotropic parallelogram plate at  $CCCC$ ,  $CCCF$ ,  $CFCF$ ,  $CSCF$ , and  $SFSF$  edge conditions corresponding to nonhomogeneity  $m$  for a fixed value of thermal gradient  $\alpha = 0.4$  and variable values of tapering parameters  $\beta_1$  and  $\beta_2$  from 0.0 to 0.8. From Table 3, the following facts can be interpreted:

- (i) As the value of nonhomogeneity  $m$  increases, the time period  $K$  of vibrational modes also increases, but time period  $K$  of vibrational modes decreases with the increasing value of tapering parameters  $\beta_1$  and  $\beta_2$ ,  $\beta_1$ ,  $\beta_2$  at all edge conditions.
- (ii) Like in Tables 1 and 2, here also the time period  $K$  of vibrational modes is higher on  $CSCF$  edge condition and less on  $CCCC$  edge condition. For different edge conditions, the time period  $K$  of vibrational modes in increasing order corresponding to nonhomogeneity  $m$  is  $CCCC < CCCF < SFSF < CFCF < CSCF$ .

- (iii) At all edge conditions, i.e., *CCCC*, *CCCF*, *CFCF*, *CSCF*, and *SFSF*, the rate of increment in time period  $K$  is less corresponding to nonhomogeneity  $m$  in comparison to the rate of decrement corresponding to tapering parameters  $\beta_1$  and  $\beta_2$ .
- (iv) The rate of increment in time period  $K$  of vibrational modes is higher on *CCCC* edge condition and less in *CSCF* edge condition corresponding to nonhomogeneity  $m$ , while the rate of decrement in time period  $K$  of vibrational modes is higher on *CCCF* edge condition and less in *CCCC* edge condition corresponding to tapering parameters  $\beta_1$  and  $\beta_2$ . For different edge conditions, the rate of increment in time period  $K$  of vibrational modes in ascending order corresponding to nonhomogeneity  $m$  is *CSCF* < *CFCF* < *CCCF* < *SFSF* < *CCCC*. But the rate of decrement in time period  $K$  of vibrational modes in ascending order corresponding to tapering parameters  $\beta_1$  and  $\beta_2$  is *CCCC* < *CFCF* < *SFSF* < *CSCF* < *CCCF*.

#### 4. Convergence of Results

In this section, the authors report a convergence study on modes of frequency  $\lambda$  for the following:

- (i) Orthotropic parallelogram plate (by taking  $\theta = 30^\circ, a/b = 1.5$  in the present study) at *CCCC*, *CCCF*, and *SFSF* edge conditions (refer Table 11)
- (ii) Orthotropic rectangle plate (by taking  $\theta = 0^\circ, a/b = 1.5$  in the present study) at *CCCC*, *CCCF*, *CFCF*, and *SFSF* edge conditions (refer Table 12)
- (iii) Orthotropic square plate (by taking  $\theta = 0^\circ, a/b = 1.0$  in the present study) at *CCCC*, *CCCF*, *CFCF*, *SFSF*, and *CSCF* edge conditions (refer Table 13)

When the order of approximation increased for all values of plate parameters in the ranges specified, i.e.,  $\beta_1 = \beta_2 = m = \alpha = 0, E_2^*/E_1^* = 0.01, E^*/E_1^* = 0.3, G_0/E_1^* = 0.0333$ , and  $\nu_0 = 0.345$ . All the results are presented in tabular form.

From Tables 11 and 12, the authors conclude that the first two modes of frequency  $\lambda$  of the orthotropic parallelogram plate at *CCCC*, *CCCF*, and *SFSF* edge conditions and orthotropic rectangle plate at *CCCC*, *CCCF*, *CFCF*, and *SFSF* edge conditions converge up to four decimal places in the fifth approximation, while Table 13 shows that the first two modes of frequency  $\lambda$  of orthotropic square plate at *CCCC*, *CCCF*, *CFCF*, *SFSF*, and *CSCF* edge conditions converge up to four decimal places in the sixth approximation.

#### 5. Result Comparison

A comparative analysis of modes of frequency  $\lambda$  and time period  $K$  obtained in the present study was done with the following available published results:

- (i) Modes of frequency  $\lambda$  of the orthotropic parallelogram plate obtained in [14] at *SSSS* edge condition

corresponding to tapering parameters  $\beta_1$  and  $\beta_2$  and nonhomogeneity  $m$  (refer Tables 4–6)

- (ii) Time period  $K$  of the orthotropic parallelogram plate obtained in [15] at *CCCC* edge condition corresponding to tapering parameter  $\beta_1$  (refer Table 7)
- (iii) Time period  $K$  of the orthotropic rectangular plate obtained in [38] at *CCCC* edge condition corresponding to nonhomogeneity  $m$  and tapering parameter  $\beta_1$  (refer Tables 8 and 9)
- (iv) Modes of frequency  $\lambda$  of isotropic square plate obtained in [39–50] at *CCCC*, *SCSC*, *FCFC*, and *SFSF* edge conditions (refer Table 10)

Tables 4 and 5 present the comparison of modes of frequency  $\lambda$  obtained in the present study (orthotropic parallelogram plate) and obtained in [14] corresponding to tapering parameters  $\beta_1$  and  $\beta_2$ , respectively, for a fixed value of aspect ratio  $a/b = 1.5$  and for the varying values of tapering parameters  $\beta_2$  and  $\beta_1$ , nonhomogeneity  $m$ , thermal gradient  $\alpha$ , and skew angle  $\theta$ , i.e.,  $\beta_2 = m = \alpha = 0.0, 0.4, 0.8, \theta = 30^\circ, 45^\circ, 60^\circ$  (refer Table 4) and  $\beta_1 = m = \alpha = 0.0, 0.4, 0.8, \theta = 30^\circ, 45^\circ, 60^\circ$  (refer Table 5) at *SSSS* edge condition. From Tables 4 and 5, the authors conclude that modes of frequency  $\lambda$  obtained in the present study (orthotropic parallelogram plate) is less in comparison to modes of frequency  $\lambda$  obtained in [14] with the increasing value of the tapering parameters  $\beta_1$  as well as  $\beta_2$  at *SSSS* edge condition.

The comparison of modes of frequency  $\lambda$  obtained in the present study (orthotropic parallelogram plate) and obtained in [14] corresponding to nonhomogeneity  $m$  for a fixed value of aspect ratio  $a/b = 1.5$  and for the varying values of tapering parameters  $\beta_1$  and  $\beta_2$ , thermal gradient  $\alpha$ , and skew angle  $\theta$ , i.e.,  $\beta_1 = \beta_2 = \alpha = 0.0, 0.4, 0.8, \theta = 30^\circ, 45^\circ, 60^\circ$  at *SSSS* edge condition, are displayed in Table 6. From Table 6, one can conclude that modes of frequency  $\lambda$  obtained in the present study (orthotropic parallelogram plate) is less in comparison to modes of frequency  $\lambda$  obtained in [14] with the increasing value of nonhomogeneity  $m$  at *SSSS* edge condition.

Table 7 shows the comparison of the time period  $K$  of the present study (orthotropic parallelogram plate) and obtained in [15] corresponding to tapering parameter  $\beta_1$  for two different sets of values of skew angle  $\theta$ , i.e.,  $\theta = 0^\circ, 45^\circ$ , at *CCCC* edge condition for a fixed value of aspect ratio  $a/b = 1.5$ . Here, the authors exclude nonhomogeneity  $m$ , thermal gradient  $\alpha$ , and tapering parameter  $\beta_2$  because these plate parameters are not considered in [15]. Table 7 enlightens the fact that the time period  $K$  obtained in the present study is higher in comparison to the time period obtained in [15] for increasing value of tapering parameter  $\beta_1$ . But the rate of decrement in the time period  $K$  obtained in the present study is less in comparison to the rate of decrement obtained in [15].

For comparison of time period  $K$  of the orthotropic rectangle plate (by considering skew angle  $\theta = 0^\circ$  in the present study) and obtained in [38], the authors exclude thermal gradient  $\alpha$  and tapering parameter  $\beta_2$  because both plates parameters are not considered in [38] (refer Tables 8 and 9). Table 8 incorporates the comparison of time period  $K$  of the orthotropic rectangle plate and obtained in [38]

TABLE 11: Convergence study of modes of frequency of the orthotropic parallelogram plate at *CCCC*, *CCCF*, and *SFSF* edge conditions.

$N$	<i>CCCC</i>		<i>CCCF</i>		<i>SFSF</i>	
	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$
2	11.3063	43.3389	11.4976	37.1324	04.8196	26.2159
3	11.3061	42.7072	11.4948	35.5899	04.6538	24.0062
4	11.3061	42.7061	11.4936	35.5099	04.4441	23.9076
5	11.3061	42.7061	11.4936	35.5099	04.2815	23.7995

TABLE 12: Convergence study of modes of frequency of orthotropic rectangle plate at *CCCC*, *CCCF*, *CFCF*, and *SFSF* edge conditions.

$N$	<i>CCCC</i>		<i>CCCF</i>		<i>CFCF</i>		<i>SFSF</i>	
	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$
2	12.2999	47.2968	12.5143	39.6281	09.8217	21.2732	04.8196	26.2159
3	12.2997	46.5478	12.5123	38.4012	08.1298	19.6771	04.6538	24.0062
4	12.2997	46.5454	12.5111	38.3289	04.7723	18.7564	04.4441	23.9076
5	12.2997	46.5454	12.5111	38.3289	04.7723	18.7564	04.4441	23.9076

TABLE 13: Convergence study of modes of frequency of the orthotropic square plate under *CCCC*, *CCCF*, *CFCF*, *SFSF*, and *CSCF* edge conditions.

$N$	<i>CCCC</i>		<i>CCCF</i>		<i>CFCF</i>		<i>SFSF</i>		<i>CSCF</i>	
	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$	$\lambda_1$	$\lambda_2$
2	24.7880	98.0261	25.0290	75.9606	22.4259	44.6728	10.4990	56.9703	22.4249	41.5100
3	24.7880	95.3261	25.0287	75.1361	21.4911	41.3478	10.4247	49.7920	20.3751	38.6953
4	24.7880	95.3069	25.0282	75.1128	18.3431	38.1168	10.3099	49.7645	14.7061	36.6312
5	24.7880	95.1864	25.0279	75.0792	14.0662	36.4318	10.1751	49.7153	8.4351	35.7986
6	24.7880	95.1864	25.0279	75.0792	14.0662	36.4318	10.1751	49.7153	8.4351	35.7986

corresponding to nonhomogeneity  $m$  for two different sets of values of tapering parameter  $\beta_1$ , i.e.,  $\beta_1 = 0.0, 0.4$ , at *CCCC* edge condition for a fixed value of aspect ratio  $a/b = 1.5$ . In Table 8, it has been seen that time period  $K$  as well as the rate of increment in time period  $K$  obtained in orthotropic rectangle plate is higher as compared to time period  $K$  as well as the rate of increment in time period  $K$  obtained in [38] with the increase in value of nonhomogeneity  $m$ .

Comparison of time period  $K$  of the orthotropic rectangle plate and obtained in [38] corresponding to tapering parameter  $\beta_1$  for two different set of values of nonhomogeneity  $m$ , i.e.,  $m = 0.0, 0.4$ , at *CCCC* edge condition for fixed value of aspect ratio  $a/b = 1.5$  is incorporated in Table 9. Here, the authors observed that the behavior of time period  $K$  obtained for the orthotropic rectangle plate (refer Table 9) is the same as the behavior of the time period obtained for the orthotropic parallelogram plate (refer Table 7), i.e., the time period  $K$  obtained in the present study is higher in comparison to the time period obtained in [38] for increasing value of tapering parameter  $\beta_1$ . But the rate of decrement in the time period  $K$  obtained in the present study is less in comparison to the rate of decrement obtained in [38].

For comparison of the mode of frequency  $\lambda$  of an isotropic square plate (by considering skew angle  $\theta = 0^\circ$  and aspect ratio  $a/b = 1$  in the present study) with the mode of frequency  $\lambda$  obtained in [39–50], the authors take the value of the plate parameters as  $E_2^*/E_1^* = 1$ ,  $\alpha = \beta_1 = \beta_2 = m = 0.0$  (refer Table 10).

Table 10 incorporates the comparison of the mode of frequency  $\lambda$  (first mode) obtained for the square plate and obtained in [39–50] at *CCCC*, *SCSC*, *FCFC*, and *FSFS* edge conditions. From Table 10, the following facts can be drawn:

- (i) The mode of frequency  $\lambda$  (first mode) obtained for the square plate is less in comparison to the mode of frequency  $\lambda$  (first mode) obtained in [39–46] at *CCCC* and [39, 40, 47, 48] *SCSC* edge condition, respectively.
- (ii) The mode of frequency  $\lambda$  (first mode) obtained for the square plate is slightly higher in comparison to the mode of frequency  $\lambda$  (first mode) obtained in [39, 40, 49] at *FCFC* and [39, 40, 49, 50] *FSFS* edge condition, respectively.

## 6. Conclusions

The present study shows the effect of 2-D tapering parameters  $\beta_1, \beta_2$ , 2-D thermal gradient  $\alpha$ , and 1-D nonhomogeneity  $m$  on the time period  $K$  of the mode of vibration of an orthotropic parallelogram plate at *CCCC*, *CCCF*, *CFCF*, *CSCF*, and *SFSF* edge conditions. From the above discussion and results comparison, the authors would like to conclude the following facts:

- (i) In the case of two-dimensional circular variation in thickness, the modes of frequency  $\lambda$  obtained for orthotropic parallelogram plate (present study) are

less in comparison to modes of frequency  $\lambda$  obtained in [14] in the case of two-dimensional linear variation in thickness (refer Tables 4 and 5) at SSSS edge condition.

- (ii) In the case of one-dimensional circular variation in density, the modes of frequency  $\lambda$  obtained for orthotropic parallelogram plates (present study) are less in comparison to modes of frequency  $\lambda$  obtained in [14] in the case of one-dimensional linear variation in density (refer Table 6) at SSSS edge condition.
- (iii) In the case of one-dimensional circular variation in thickness, the time period  $K$  obtained for the orthotropic parallelogram plate (present study) is higher in comparison to time period  $K$  obtained in [15] in the case of one-dimensional parabolic variation in thickness (refer Table 7) at CCCC edge condition.
- (iv) In the case of one-dimensional circular variation in density, the time period  $K$  obtained for the orthotropic rectangle plate (present study) is higher in comparison to the time period  $K$  obtained in [38] in the case of one-dimensional linear variation in density (refer Table 8) at CCCC edge condition.
- (v) In the case of one-dimensional circular variation in thickness, the time period  $K$  obtained for the orthotropic rectangle plate (present study) is higher in comparison to the time period  $K$  obtained in [38] in the case of one-dimensional parabolic variation in thickness (refer Table 9) at CCCC edge condition.
- (vi) At CCCC, CFCF, and SFSF edge conditions, the tapering parameter  $\beta_1$  dominates the rate of change in time period  $K$  more than the tapering parameter  $\beta_2$ , while at CCCF and CFCF, the tapering parameter  $\beta_2$  dominates the rate of change in time period  $K$  more than the tapering parameter  $\beta_1$  (refer Table 1).
- (vii) At CCCC edge condition, the thermal gradient  $\alpha$  dominates the rate of change in time period  $K$  more than the tapering parameters  $\beta_1, \beta_2$ , while at CCCF, CFCF, CFCF, and SFSF, the tapering parameters  $\beta_1, \beta_2$  dominate the rate of change in time period  $K$  more than the thermal gradient  $\alpha$  (refer Table 2).
- (viii) At all edge conditions, i.e., CCCC, CCCF, CFCF, CSCF, and SFSF, the tapering parameters  $\beta_1, \beta_2$  dominate the time period  $K$  (rate of decrement) more than the nonhomogeneity  $m$  (refer Table 3).
- (ix) The time period  $K$  of modes of frequency decreases with the increasing value of tapering parameters  $\beta_1, \beta_2$  (refer Table 1), while the time period  $K$  of modes of frequency increases with the increasing value of thermal gradient  $\alpha$  and nonhomogeneity  $m$  (refer Tables 2 and 3).

From the abovementioned conclusions, we can say modes of frequency  $\lambda$ , time period  $K$ , and variation in time period  $K$  can be minimized and controlled by choosing the circular variation in the plate parameters.

## Data Availability

The research data used to support the findings of this study are currently under embargo, while the research findings are commercialized. Requests for data, 6 months after the publication of this article, will be considered by the corresponding authors.

## Conflicts of Interest

The authors declare that they have no conflicts of interest.

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