

# Research Article

# **Experimental Study on Physical and Dynamic Mechanical Properties of Temperature-Water Coupled Sandstone**

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In order to study the influence characteristics of water bath at different temperatures on rock physical and dynamic mechanical properties, a total of 15 groups of temperature-water bath treatment were carried out on coal mine roadway sandstone at  $25^{\circ}C-95^{\circ}C$ , and the basic physical parameters were tested. The impact compression test was carried out using the split Hopkinson pressure bar (SHPB) device. The results show that, with the increase of water bath temperature, the particle gap on the specimen surface increases. The volume, mass, and density of the specimens all increased with the increase of water bath temperature, and the increase was closely related to the water bath temperature. The dynamic compressive strength increases as a quadratic function of the water bath temperature, and the rate of increase is different before and after  $45^{\circ}C$ . The dynamic peak strain and average strain rate showed a quadratic function with the water bath temperature. The dynamic peak strain before  $45^{\circ}C$  decreased with the temperature increasing, and the dynamic peak strain after  $45^{\circ}C$  increased with the temperature increasing. The dynamic elastic modulus increased first and then decreased with the increase of water bath temperature and reached the maximum at  $45^{\circ}C$ . The failure pattern of sandstone is spalling. With the increase of water bath temperature, the fracture degree of the specimen gradually decreases.

#### 1. Introduction

In recent years, with increasing excavation depth of underground space, the ground temperature is also getting higher [1]. Deep rock mass excavation is often in a special environment full of water [2]. Blasting excavation is one of the main excavation methods of deep rock mass engineering. Deep rock mass is subjected to impact load during excavation. Underground rock mass is mostly in the state of immersion, and different depth corresponding to the water temperature is different. Therefore, it is of great engineering value to carry out the experimental study on the dynamic mechanical properties of sandstone under the coupled action of temperature and water.

Many scholars have used TAW-2000 or RMT-150B rock mechanics test system to carry out static load test research on

rocks under or after high-temperature treatment. Qin et al. [3] carried out uniaxial compression tests on sandstone specimens treated at 200°C to 800°C and analyzed its stressstrain curve characteristics. Yu et al. [4] studied the variation characteristics of mass and longitudinal wave velocity with temperature after limestone was subjected to a high temperature of 20°C to 650°C and carried out uniaxial compression tests under static load. Jin et al. [5] compared two ways of natural cooling and water cooling after sandstone was subjected to a high temperature of 100°C to 800°C. Wu and Wang [6] carried out uniaxial compression and Brazil splitting tests on granites subjected to a high temperature of 250°C to 600°C, to analyze the stress-strain curve and loadradial displacement curve of granites. Rohan et al. [7] studied the effects of pretreatment on UPV and rock microstructure after treated at 100°C to 600°C. Yu et al. [8]

conducted uniaxial compression tests on sandstone after high-temperature treatment at 100°C to 600°C and under a high-temperature condition and analyzed the uniaxial compressive strength of sandstone after high-temperature cooling and under high-temperature condition. Su et al. [9] used the RMT-150B testing machine to analyze the deformation characteristics, strength characteristics, and acoustic emission characteristics of hard coal samples treated at 100°C to 500°C. Wei et al. [10] carried out static uniaxial compression on anthracite samples after hightemperature treatment at 20°C to 500°C and analyzed the change of coal sample density and porosity with temperature. Chen et al. [11] carried out uniaxial compression tests on granite specimens under a high temperature of 25°C to 1000°C at five loading rates. Split Hopkinson pressure bar (SHPB) device is the most commonly used loading device in the study of rock dynamic physical and mechanical properties. Ping et al. [12-15] analyzed the variation rule of the dynamic stress-strain curve of sandstone under a high temperature of 25°C to 1000°C. In addition, the effects of temperature on dynamic compressive strength, dynamic peak strain and strain rate, dynamic elastic modulus, and failure mode were investigated. Xu et al. [16] carried out dynamic uniaxial compression tests at three loading rates on sandstone subjected to a high temperature ranging from 25°C to 700°C. Zhang [17] analyzed the variation of dynamic stress, strain, strain rate, fractal dimension, failure mode, and damage degree with a temperature of sandstone subjected from -15°C to 800°C. Chen et al. [18] carried out a dynamic uniaxial compression test on sandstone subjected to a high temperature of 100°C to 1000°C. Liu and Xu [19] carried out dynamic compression tests on granite under a high-temperature action of 25°C to 1000°C and analyzed the variation law of peak stress and strain of granite with temperature. Yang et al. [20] conducted triaxial compression tests on granites subjected to a high temperature of 200°C~800°C and found that thermal cracks were generated and the cohesion between crystals was reduced.

Scholars at home and abroad mainly focus on the static and dynamic physical and mechanical properties of rocks in water. Xie et al. [21] used MTS815 testing machine to conduct uniaxial and triaxial compression tests on red-bed soft rocks under natural and saturated conditions and analyzed its strength and deformation characteristics. Liu et al. [22] used Rock-600-50 triaxial rheometer to analyze the mechanical behavior and energy evolution rule of yellow sandstone under the action of pore water. Duan and Ren [23] carried out static uniaxial compression tests on five kinds of sandstone with different water contents and analyzed the law of various physical parameters changing with water content. Zhang et al. [24] carried out a uniaxial compression acoustic emission test on saturated granite. Fang et al. [25] conducted uniaxial compression tests on four kinds of argillaceous siltstones and discussed the strength damage evolution characteristics of argillaceous siltstones under the influence of water content. Teng et al. [26] carried out uniaxial compression tests on four kinds of layered shales with water content and analyzed that the damage of water to shale was mainly due to adsorption of water and

capillary pressure. Su et al. [27] carried out uniaxial compression tests on natural and saturated sandstone and analyzed the deformation, strength, and energy characteristics of the specimens. Zhang [28] analyzed the water-rock interaction of shale and obtained the microscopic nature of the deterioration of water-rock interaction of shale. Fu et al. [29] carried out uniaxial compression tests on rock samples under natural state, saturated water action, and dry-wet cycle, to analyze the uniaxial compressive strength and elastic modulus of sandstone. Yang et al. [30] carried out uniaxial compression tests on siltstone samples soaked in water at 50°C and 100°C and discussed the infrared radiation characteristics of siltstone in the rupture process soaked at different water temperatures. Gao et al. [31] carried out uniaxial dynamic compression loading tests on marble under four damage gradients and dry and saturated states, to analyze the relationship between dynamic compressive strength and water content. Wang et al. [32] carried out a uniaxial dynamic compression test and dynamic splitting test on fine sandstone in a natural and saturated state and analyzed the effects of water and loading rate on dynamic tensile and compressive strength of fine sandstone and their differences. Zhao et al. [33] carried out dynamic tensile tests on sandstone specimens with different water contents and studied the variation rule of dynamic tensile strength of sandstone specimens with different water content under different loading rates. Zhou et al. [34] carried out dynamic compression, splitting, and fracture tests on dry and saturated sandstone and analyzed the relationship between rock strength and fracture toughness with water and loading rate. Chu et al. [35] carried out uniaxial dynamic compression tests on sandstone samples with three different waterbearing states and analyzed the stress-strain curves of the rock samples. Wang et al. [36] conducted uniaxial dynamic compression tests on four kinds of red sandstone with different water-bearing states and analyzed the rock failure micromechanism. Guo et al. [37] conducted an experimental study on the thermal conductivity of sandstone at different temperatures and water content and found that the thermal conductivity of sandstone in a saturated state decreased with the increase of temperature. Yu et al. [38] conducted uniaxial compression mechanical tests on granite after hydrothermal cycling and analyzed its appearance morphology and stressstrain curve. Hashiba and Fukui [39] carried out tensile tests on five kinds of rocks and found that the strength of rocks decreases after being saturated with water. Wong and Jong [40] studied the effect of water on the tensile strength of gypsum and found that water can reduce the tensile strength of gypsum. Karakul and Ulusay [41] conducted tensile tests on rock and found that the tensile strength of rocks decreased with the increase of water saturation. An et al. [42] carried out experimental research on rocks under the coupling action of high temperature and dynamic load, carried out dynamic and static tests on rocks, and obtained the relationship curves among loading rate, strain, temperature, compressive strength, and tensile strength. Wen et al. [43] conducted a dynamic compressive test study on sandstone under the coupling action of low temperature and dynamic load, analyzed the fracture morphology

characteristics, and obtained the dynamic failure law of sandstone. Wang et al. [44] conducted dynamic compression tests on Huashan granite to study the effects of treatment temperature and strain rate on the mechanical behavior of granite.

It can be seen that there are many researches on the static and dynamic physical and mechanical properties of sandstone under the action of high temperature and water rock. The researches on the physical and mechanical properties of sandstone under the action of temperature-water coupling mainly focus on the static load test, while the dynamic load test needs to be further studied. For studying physical and dynamic mechanical properties of sandstone is influenced by temperature and water coupling rules, the basic physical parameters of sandstone specimens after water bath at 25°C, 30°C, 35°C, 40°C, 45°C, 50°C, 55°C, 60°C, 65°C, 70°C, 75°C, 80°C, 85°C, 90°C, and 95°C were measured, and the color, mass, volume, and density of the specimens were compared and analyzed. The impact compression tests of sandstone specimens subjected to different water bath temperatures were carried out under similar loading conditions by using SHPB equipment. The correlation between dynamic characteristics of the specimens, such as peak stress strength, dynamic elastic modulus, average strain rate, and failure mode, and the change of water bath temperature was studied.

### 2. Sample Preparation and SHPB Test Device after Water Bath

2.1. Processing of Sandstone Specimen. Rock specimens used in this test are all taken from the deep roadway sandstone of Gubei Coal Mine of Huainan Mining Group in Anhui Province. In order to increase the contrast between the test specimens, the test specimens are all selected from the same rock block. According to the relevant provisions of "Methods for Determination of Physical and Mechanical Properties of Coal and Rock" [45], rock coring machine, cutting machine, and end grinding machine were used to grind the specimen into a cylinder specimen with a diameter of 50 mm and a length-diameter ratio of about 0.5.

2.2. Preparation of Specimens after Water Bath. The box-type water bath box is used to heat the sandstone specimen in the water bath, as shown in Figure 1. The size of the box is  $420 \text{ mm} \times 200 \text{ mm} \times 105 \text{ mm}$ , and the maximum heating temperature is 99°C.

First of all, the sandstone test pieces are evenly placed in the water bath box, with a certain gap between the test pieces and the door of the box closed. After heating to the corresponding temperature, keep the temperature with a constant value and water bath for 48 h [46]. Finally, turn off the water bath heating system, open the box cover, remove the specimen from the water bath box, wipe the moisture on the surface of the specimen with a dry towel, and measure the mass, diameter, thickness, and longitudinal wave velocity of the specimen.



FIGURE 1: Water bath.

2.3. SHPB Test Device. The test equipment in this paper is the SHPB test device of the State Key Laboratory of Mining Response and Disaster Prevention and Control in Deep Coal Mine, as shown in Figure 2. The impact compression test is carried out on sandstone specimens subjected to different water bath temperatures.

The SHPB test device shown in Figure 2 is mainly composed of an impact bar, an incident bar, a transmission bar, an absorbing bar, an oscilloscope, and a CS dynamic resistance strain gauge. The diameter of the incident bar, transmission bar, and absorption bar is 50 mm, bar length is 2000 mm, 1500 mm, and 1000 mm, respectively, with a material density of 7636 kg/m<sup>3</sup>, Poisson ratio is 0.28, elastic longitudinal wave velocity is 5190 m/s, and the impact rod adopts spindle shape. Before installation, a thin layer of Vaseline is evenly applied to the contact area between the pressure bar and the end face of the specimen as a lubricant to reduce the friction between the sandstone specimen and the end face of the pressure bar. In order to compare the influence law of water bath action at different temperatures on the dynamic characteristics of sandstone specimens, it is necessary to ensure the same impact loading conditions for each impact compression test in SHPB; that is, the same impact pressure is used to load specimens. The experimental principle is to measure the incident wave and reflected wave in the incident bar and the transmitted pulse in the transmission bar by using a strain gauge and obtain the stress-strain relationship according to the stress wave theory [47].

## 3. Physical Properties of Sandstone before and after Water Bath

3.1. Color and Apparent Morphology of Specimens after Water Bath. The color and apparent morphological changes of sandstone specimens subjected to different water bath temperatures are shown in Figure 3.

As can be seen from Figure 3, the surface color of sandstone specimens after water bath at  $25^{\circ}C \sim 95^{\circ}C$  did not change significantly and was mainly grayish-white. After water bath at  $25^{\circ}C \sim 45^{\circ}C$ , the particles on the surface of sandstone are dense. After water bath at  $45^{\circ}C \sim 95^{\circ}C$ , the particle gap on the surface of the specimen increases. It can be inferred that, with the increase of temperature, water gradually enters the specimen through the cracks on the surface, and water molecules weaken the binding effect between mineral particles and promote the particles to fall off, thus increasing the pores of sandstone. This indicates



FIGURE 2: SHPB test device.



FIGURE 3: Apparent morphology of sandstone specimens after water bath at different temperatures. (a)  $25^{\circ}$ C. (b)  $30^{\circ}$ C. (c)  $35^{\circ}$ C. (d)  $40^{\circ}$ C. (e)  $45^{\circ}$ C. (f)  $50^{\circ}$ C. (g)  $55^{\circ}$ C. (h)  $60^{\circ}$ C. (j)  $70^{\circ}$ C. (k)  $75^{\circ}$ C. (l)  $80^{\circ}$ C. (m)  $85^{\circ}$ C. (n)  $90^{\circ}$ C. (o)  $95^{\circ}$ C.

that when the temperature is between 25°C and 45°C, a small amount of water enters the interior of the sandstone, and the internal structure of the sandstone specimen is mainly the combination between particles. After 45°C, more water enters the sandstone, and the internal structure of sandstone specimen is mainly composed of a water-particle combination.

3.2. Measurement and Results of Basic Physical Parameters. After the specimen taken out of the water bath box is wiped clean with a dry towel, the size and mass of the sandstone specimen are measured one by one, and the volume and density are calculated. The C61 nonmetallic ultrasonic detector was used to measure the elastic wave propagation time between the two end faces of the specimen, and longitudinal wave velocity was calculated. The basic physical parameters of sandstone specimens before and after water bath are shown in Table 1. 3.3. Changes in Volume, Mass, and Density of Specimens. After water bath at different temperatures, the sandstone specimens showed volume expansion and mass increase, and the volume expansion rate increased with the increase of water bath temperature, as shown in Figure 4.

As can be seen from Figure 4, the volume expansion rate of sandstone specimen was not affected by the change of water bath temperature in the range of  $25^{\circ}$ C~ $45^{\circ}$ C, and the increased value varied from 0.39% to 0.45%. The volume expansion rate showed a slight increase, and the volume expansion rate was the smallest at  $25^{\circ}$ C, only 0.39%. This may be because the water bath caused the volume expansion of the mineral particles composed of sandstone, which first occupied the original micropores and microcracks in the specimen, so the volume expansion of the specimen was relatively small. When the water bath temperature rose to  $45^{\circ}$ C, new microcracks sprouted inside the sandstone specimen, leading to the appearance volume expansion of the specimen, and the volume expansion rate increased

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Snecimen			Without	the water i	bath				After	the water	bath		
number	Diameter (mm)	Thickness (mm)	Mass (g)	Volume (cm <sup>3</sup> )	Density (g·cm <sup>-3</sup> )	Longitudinal wave velocity (m·s <sup>-1</sup> )	Temperature (°C)	Diameter (mm)	Thickness (mm)	Mass (g)	Volume (cm <sup>3</sup> )	$\frac{\text{Density}}{\text{(g-cm}^{-3})}$	Longitudinal wave velocity (m·s <sup>-1</sup> )
GB22-03	49.68	24.96	121.09	48.4	2.502	2600		49.69	25.05	122.78	48.6	2.527	2319
GB22-04	49.69	25.17	122.86	48.8	2.517	2860	25	49.84	25.19	124.34	49.1	2.530	2422
GB22-05	49.72	25.24	123.51	49.0	2.521	2868		49.71	25.34	125.21	49.3	2.540	2437
GB22-07	49.73	25.00	122.81	48.5	2.530	2976		49.70	25.11	124.26	48.7	2.551	2511
GB22-08	49.72	25.01	121.57	48.5	2.504	2718	30	49.71	25.05	123.10	48.6	2.532	2319
GB22-09	49.73	25.06	121.78	48.7	2.502	2610		49.76	25.06	123.26	48.7	2.529	2321
GB22-13	49.72	25.09	123.05	48.7	2.526	2987		49.81	25.15	124.25	49.0	2.535	2418
GB22-14	49.71	24.94	122.12	48.4	2.524	2834	35	49.71	24.97	123.45	48.5	2.547	2401
GB22-15	49.58	24.83	119.63	47.9	2.496	2821		49.62	24.79	121.14	47.9	2.528	2430
GB22-16	49.70	25.08	121.37	48.6	2.495	2612		49.80	25.17	123.09	49.0	2.511	2247
GB22-17	49.65	25.01	121.87	48.4	2.518	2718	40	49.74	25.19	123.25	48.9	2.518	2209
GB22-18	49.76	25.10	123.85	48.8	2.537	2988		49.81	25.19	124.99	49.1	2.546	2377
GB22-21	49.71	25.19	123.23	48.9	2.521	2863		49.76	25.30	124.85	49.2	2.538	2433
GB22-22	49.72	24.90	121.83	48.4	2.520	2394	45	49.80	25.02	123.32	48.7	2.531	2120
GB22-23	49.74	25.07	121.93	48.7	2.504	2507		49.67	25.14	123.14	48.7	2.528	2095
GB22-26	49.69	25.07	121.63	48.6	2.502	2725		49.77	25.18	123.44	49.0	2.520	2421
GB22-27	49.73	25.08	122.16	48.7	2.507	2986	50	49.88	25.21	123.30	49.2	2.504	2424
GB22-28	49.68	25.06	122.16	48.6	2.515	2848		49.74	25.12	123.50	48.8	2.530	2416
GB22-31	49.71	24.83	121.56	48.2	2.523	2956		49.74	24.97	123.23	48.5	2.540	2400
GB22-32	49.69	24.96	121.20	48.4	2.505	2713	55	49.68	25.05	122.45	48.5	2.522	2456
GB22-33	49.74	24.93	122.40	48.4	2.527	2968		49.79	25.01	123.57	48.7	2.538	2452
GB22-36	49.63	24.77	118.90	47.9	2.482	2477		49.65	24.87	120.64	48.1	2.506	2220
GB22-37	49.77	25.04	124.03	48.7	2.547	2981	60	49.80	25.18	125.17	49.0	2.553	2518
GB22-38	49.69	24.88	120.38	48.2	2.495	2704		49.72	25.01	121.76	48.6	2.507	2233
GB22-41	49.64	24.80	119.69	48.0	2.494	2696		49.66	24.96	121.38	48.3	2.511	2311
GB22-42	49.77	25.09	123.94	48.8	2.539	2987	65	49.79	25.22	125.17	49.1	2.550	2425
GB22-43	49.59	25.06	122.01	48.4	2.522	2847		49.64	25.11	123.18	48.6	2.535	2415
GB22-46	49.70	25.13	122.05	48.7	2.504	2991		49.83	25.19	124.73	49.1	2.539	2519
GB22-47	49.70	24.86	120.31	48.2	2.495	2390	70	49.73	24.99	121.59	48.5	2.505	2231
GB22-48	49.61	25.11	122.46	48.5	2.523	2854		49.70	25.14	123.55	48.8	2.534	2514
GB22-51	49.73	24.84	121.11	48.2	2.511	2957		49.78	24.90	124.80	48.5	2.576	2490
GB22-52	49.73	24.95	121.49	48.5	2.507	2712	75	49.75	25.04	122.69	48.7	2.521	2608
GB22-53	49.59	25.04	121.30	48.4	2.509	2722		49.66	25.18	122.65	48.8	2.515	2569
GB22-56	49.71	25.09	122.11	48.7	2.508	2727		49.85	25.13	124.82	49.0	2.546	2416
GB22-57	49.72	24.99	122.46	48.5	2.524	2717	80	49.76	25.12	123.81	48.8	2.535	2415
GB22-58	59.65	25.00	120.73	69.8	1.729	2404		49.80	25.04	122.13	48.8	2.504	2236
GB22-62	49.66	25.09	123.40	48.6	2.540	2851		49.68	25.24	124.51	48.9	2.545	2629
GB22-63	49.63	24.93	121.44	48.2	2.518	2493	85	49.70	25.10	122.93	48.7	2.524	2510
GB22-64	49.74	25.03	123.48	48.6	2.539	2979		49.87	25.08	126.21	49.0	2.576	2508
GB22-66	49.64	25.06	121.39	48.5	2.504	2983		49.58	25.21	124.37	48.7	2.556	2626
GB22-67	49.74	24.96	120.76	48.5	2.491	2496	90	49.79	25.12	122.02	48.9	2.495	2325
GB22-68	49.71	24.99	122.63	48.5	2.529	2716		49.80	25.09	124.11	48.9	2.540	2412
GB22-70	49.73	25.03	122.06	48.6	2.511	2317		49.75	25.15	125.80	48.9	2.573	2372
GB22-71	49.69	25.04	122.57	48.5	2.525	2721	95	49.77	25.15	123.63	48.9	2.527	2418
GB22-72	49.65	24.98	121.20	48.4	2.506	2402		49.77	25.03	122.25	48.7	2.511	2318

rapidly. When the water bath temperature was increased to 95°C, the volume expansion rate of the specimen reached the maximum of 0.94%.

The volume expansion rate of the sandstone specimen increases with the water bath temperature in a quadratic function relationship, as shown in equation (1), and the fitting curve is shown in Figure 4:

$$\begin{cases} V_{T1}' = 9 \times 10^{-5} T^2 - 0.003T + 0.4117, \ 25^{\circ} C \sim 45^{\circ} C, \quad R^2 = 0.9975, \\ V_{T1}' = 9 \times 10^{-5} T^2 - 0.003T + 0.4117, \ 45^{\circ} C \sim 95^{\circ} C, \quad R^2 = 0.9843, \end{cases}$$
(1)

where  $V_{T1}'$  and  $V_{T2}'$  are the volume expansion rate of sandstone specimen after water bath action, %.

The variation of the water absorption rate of sandstone specimens with the rise of water bath temperature after water bath action is shown in Figure 5.

As can be seen from Figure 5, the water absorption rate of specimens with different water bath temperatures increased with the increase of water bath temperature. With the increase of water bath temperature, the water absorption capacity of sandstone becomes stronger. Sandstone is mainly cemented by sand grains, which have more sand content, thus showing a temperature effect. The higher the temperature is, the easier the water will enter the interior of the sandstone. The relationship between water absorption of sandstone specimens and water temperature increases with a strong quadratic function after different water bath temperatures. As shown in equation (2), the fitting curve is shown in Figure 5:

$$\begin{cases} M_{T1} = 4 \times 10^{-4} T^2 - 0.0224T + 1.514, \ 25^{\circ} \text{C} \sim 45^{\circ} \text{C}, \quad R^2 = 0.9830, \\ M_{T2} = 5 \times 10^{-5} T^2 + 0.0176T + 0.4376, \ 45^{\circ} \text{C} \sim 95^{\circ} \text{C}, \quad R^2 = 0.9820, \end{cases}$$
(2)

where  $M_{T1}$  and  $M_{T2}$  are the water absorption rate of sandstone specimen after water bath action, %.

After the water bath, the density of sandstone specimen changes with the rise of water bath temperature, as shown in Figure 6.

It can be seen from Figure 6 that the density of the specimen increases with the increase of water bath temperature after the action of different water bath temperatures. When the water bath temperature was in the range of  $25^{\circ}$ C~ $45^{\circ}$ C, the increase rate of the specimen density was less affected by the change of the water bath temperature, and the amplitude of the increase rate of the specimen density was

0.51%~0.68%. When the water bath temperature was in the range of 45°C to 95°C, the density of the specimen was greatly affected by the water bath temperature. The density increase rate at 45°C was 0.68%, and the density increase rate at 95°C was the largest (2.47%), which was about 3.6 times that at 45°C. The basic reason for the increase of density of sandstone specimen is that the volume expansion and mass increase of sandstone specimen after water bath.

The density increase rate of sandstone specimen increases in a quadratic function between 25°C and 95°C, and the growth rate is different before and after 45°C, as shown in equation (3). The fitting curve is shown in Figure 6:

$$\begin{cases} \rho_{T1} = -6 \times 10^{-5} T^2 + 0.012T + 0.2489, \ 25^{\circ} \text{C} \sim 45^{\circ} \text{C}, \quad R^2 = 0.9703, \\ \rho_{T2} = 4 \times 10^{-4} T^2 - 0.0288T + 1.0747, \ 45^{\circ} \text{C} \sim 95^{\circ} \text{C}, \quad R^2 = 0.9693, \end{cases}$$
(3)

where  $\rho_{T1}$  and  $\rho_{T1}$  are the density increase rate of sandstone specimen after water bath action, %.

#### 4. Test Results and Analysis of Sandstone with Different Water Bath Temperatures

4.1. Analysis of the Relationship between Different Water Bath Temperatures and Peak Stress Strength. The variation of peak stress strength of sandstone specimens after water bath is shown in Figure 7.

It can be seen from Figure 7 that the dynamic peak stresses of sandstone specimen quadratic increase with the increase of water bath temperature between 25°C and 45°C.

The absorb water ratio of sandstone specimen increases with increasing bath temperature, which resists the extension of cracks. Therefore, the peak stress increases accordingly. The peak stress strength increases rapidly between 45°C and 95°C. It can be inferred that, with the increase of temperature, a certain amount of moisture and thermal stress accumulates inside the sandstone, and under the action of temperature-water coupling, the internal pores of the sandstone are filled, thus improving the compressive strength of the sandstone.

The peak stress strength of sandstone specimens increases as a quadratic function with the water bath temperature, as shown in equation (4), and the fitting curve is shown in Figure 7:



FIGURE 4: Volume changes with water bath temperature.



FIGURE 5: Relationship between water absorption of sandstone and water bath temperature.



FIGURE 6: Density changes with water bath temperature.



FIGURE 7: Fitting curve between water bath temperature and peak stress strength.

$$\begin{cases} \sigma_{T1} = -0.0301T^2 + 2.961T + 7.3591, 25^{\circ}C \sim 45^{\circ}C, \quad R^2 = 0.9963, \\ \sigma_{T2} = 0.0115T^2 - 0.9774T + 99.166, 45^{\circ}C \sim 95^{\circ}C, \quad R^2 = 0.9928, \end{cases}$$
(4)

where  $\sigma_{T1}$  and  $\sigma_{T2}$  are the peak stress strength of sandstone specimen after water bath action, MPa.

4.2. Analysis of the Relationship between Different Water Bath Temperatures and Peak Strain. The variation of peak strain of sandstone specimen with water bath temperature after water bath is shown in Figure 8.

It can be seen from the Figure 8, The peak strain of sandstone specimen decreases at, 25°C~45°C. The sandstone

specimen move the peak strain decreases with water bath temperature, and can be speculated that with the increase of bath temperature, sandstone specimens gathered a certain amount of internal thermal stress and water, and water under the action of thermal stress in these, the internal microcracks, filled with rock to produce thermal damage, the sandstone specimen of peak strain showed a trend of decrease. In the temperature range of 45°C water bath, the dynamic peak strain has little change, and the strain amplitude is  $1.35 \times 10^{-3} \sim 2.27 \times 10^{-3}$ . When the water bath

temperature exceeds 45°C, the dynamic peak strain obviously increases with the increase of the water bath temperature. When the temperature of the water bath reaches 95°C, the dynamic peak strain is  $5.23 \times 10^{-3}$ , which is about 3.9 times compared with that at 45°C.

The relationship between the dynamic peak strain of sandstone specimen and the water bath temperature is a quadratic function, as shown in equation (5), and the fitting curve is shown in Figure 8:

$$\begin{cases} \varepsilon_{T1} = 0.0026T^2 - 0.2238T + 6.198, 25^{\circ}C \sim 45^{\circ}C, & R^2 = 0.9657, \\ \varepsilon_{T2} = 0.0015T^2 - 0.1445T + 4.9419, 45^{\circ}C \sim 95^{\circ}C, & R^2 = 0.9803, \end{cases}$$
(5)

where  $\varepsilon_{T1}$  and  $\varepsilon_{T2}$  are the dynamic peak strain of sandstone specimen after water bath action.

4.3. Analysis of the Relationship between Different Water Bath Temperatures and Dynamic Elastic Modulus. After the water bath, the dynamic elastic modulus of sandstone specimen changes with water bath temperature, as shown in Figure 9.

It can be seen from Figure 9 that the dynamic modulus of elasticity increases with the increase of water bath temperature between 25°C and 45°C. The dynamic modulus of elasticity is 27.61 GPa at 25°C and 79.36 GPa at 45°C, which is 187% higher than that at 25°C. It reaches the peak value at 45°C and then decreases with the increase of water bath temperature. This is because when the water bath temperature is lower than 45°C, the damage of sandstone is mainly affected by water. Due to the Stefan effect of water [48], water exerts resistance to rock cracks, impedes the expansion of cracks, and thus improves rock strength. After reaching the peak value, with the increase of water bath temperature, the failure of sandstone is mainly affected by the temperature, and the microcracks in sandstone specimens gradually expand, which leads to the decrease of deformation resistance and elastic modulus of the specimens. The elastic modulus of the specimen has a quadratic function relationship with the water bath temperature, as shown in equation (6), and the fitting curve is shown in Figure 9:

$$\begin{cases} E_{T1} = -0.0397T^2 + 4.284T - 54.141, \ 25^{\circ}C \sim 45^{\circ}C, \quad R^2 = 0.9938, \\ E_{T2} = 0.0025T^2 - 1.0393T + 99.292, \ 45^{\circ}C \sim 95^{\circ}C, \quad R^2 = 0.9869, \end{cases}$$
(6)

where  $E_{T1}$  and  $E_{T2}$  are the dynamic elastic modulus (GPa) of sandstone specimen after water bath.

4.4. Analysis of the Relationship between Different Water Bath Temperatures and Average Strain Rates. After the water bath, the average strain rate of sandstone varies with water bath temperature, as shown in Figure 10. As can be seen from Figure 10, the average strain rate decreases in a quadratic parabola with the temperature increasing from  $25^{\circ}$ C to  $45^{\circ}$ C. From  $45^{\circ}$ C to  $95^{\circ}$ C, the average strain rate increases in a quadratic parabola with the increase of temperature. As shown in equation (7), the fitting curve is shown in Figure 10:

$$\begin{cases} \dot{\varepsilon}_{T1} = 0.0233T^2 - 2.1702T + 74.905, 25^{\circ}C \sim 45^{\circ}C, \quad R^2 = 0.9959, \\ \dot{\varepsilon}_{T2} = -0.0004T^2 + 0.5051T + 3.5677, 45^{\circ}C \sim 95^{\circ}C, \quad R^2 = 0.9935, \end{cases}$$
(7)

where  $\dot{\varepsilon}_{T1}$  and  $\dot{\varepsilon}_{T2}$  are the mean strain rate of sandstone specimen after water bath action, s-1.

4.5. Failure Mode Analysis of Specimens. After experiencing different water bath temperatures, the failure modes of sandstone specimens SHPB under impact compression are shown in Figure 11.

As can be seen from Figure 11, under the same impact pressure, with the increase of water bath temperature, the damage degree of the specimen gradually decreases. When the temperature of the water bath was 25°C~45°C, the failure modes of specimens were large-scale flaking failure and axial splitting failure. When the water bath temperature was between 50°C and 95°C, the failure mode of the specimen was side spalling failure. When the temperature reaches 95°C, the damage degree of the specimen is small, and only a crack is formed on the side. To analyze the reasons, before the water bath temperature was 45°C, the specimen expanded slightly under the joint action of temperature and water. Under the action of the specimen were closed, thus



FIGURE 8: Fitting curve between water bath temperature and dynamic peak strain.



FIGURE 9: Fitting curve of water bath temperature and dynamic elastic modulus change law.



FIGURE 10: Fitting curve of change law between peak stress and average strain rate.



FIGURE 11: Dynamic compression failure modes of sandstone specimens with different water bath temperatures. (a)  $25^{\circ}$ C. (b)  $30^{\circ}$ C. (c)  $35^{\circ}$ C. (d)  $40^{\circ}$ C. (e)  $45^{\circ}$ C. (f)  $50^{\circ}$ C. (g)  $55^{\circ}$ C. (h)  $60^{\circ}$ C. (i)  $65^{\circ}$ C. (j)  $70^{\circ}$ C. (k)  $75^{\circ}$ C. (l)  $80^{\circ}$ C. (m)  $85^{\circ}$ C. (n)  $90^{\circ}$ C. (o)  $95^{\circ}$ C.

making the specimen compact, the compressive strength of the specimen also increased, and the damage degree of the specimen gradually decreased. When the bath temperature was larger than 45°C, more water was absorbed by sandstone specimen with the increase of temperature, resulting in the increase of Stefan effects. Therefore, it was more different for crack propagation of specimen under dynamic loading, and the specimen damage decreased gradually. In summary, the dynamic failure characteristics of water bath sandstone correspond to the strength characteristics.

#### 5. Conclusion

- (1) The sandstone at 25°C~95°C is basically grayishwhite, and the surface particles of the specimen at 25°C~45°C are compact. After 45°C, the surface particle gap of the specimen is obvious, and the water absorption rate of the sandstone also gradually increases. The volumetric expansion rate, water absorption rate, and density increase rate of the specimens increased in a quadratic function relationship with the water bath temperature and increased slowly from 25°C to 45°C, but rapidly from 45°C to 95°C. After a 95°C water bath, the maximum increase rates of specimen volume and density were 0.94% and 2.47%, respectively.
- (2) The peak stress strength of the specimen increases in a quadratic function with the increase of water bath temperature. The rate of increase is small from 25°C to 45°C but large from 45°C to 95°C. The dynamic peak strain of the specimen decreases first and then increases with the increase of water bath temperature,

which is a quadratic function with the water bath temperature. The dynamic peak strain of the specimen is the minimum when the water bath temperature is 45°C. The dynamic modulus of the specimen first increased and then decreased with the increase of the water bath temperature, which showed a quadratic function relationship with the water bath temperature. When the water bath temperature was 45°C, the dynamic modulus reached the maximum. The average strain rate of the specimen decreases first and then increases with the increase of water bath temperature.

(3) The change of dynamic failure characteristics of the specimen corresponds to its strength characteristics. The fracture degree of the specimen under impact compression gradually decreases with the increase of water bath temperature. Because of the Stefan effect of water, the crack propagation of sandstone is hindered and the dynamic mechanical properties of sandstone are changed. When the temperature is 95°C, the fracture degree of the specimen is the least, which appears as a crack on the side.

#### **Data Availability**

The data used to support the findings of this study are available from the corresponding author upon request.

#### **Conflicts of Interest**

The authors declare that there are no conflicts of interest regarding the publication of this paper.

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